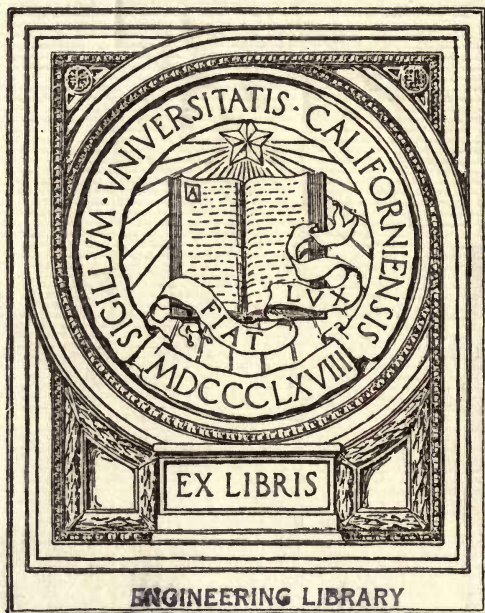


GIFT OF
Daughter of William
Stuart Smith, U.S. Navy



ENGINEERING LIBRARY



W. Stuart-Smith.

March 8th '97

San Francisco Calif.

THEORY AND CALCULATION

OF

ALTERNATING CURRENT
PHENOMENA

BY

CHARLES PROTEUS STEINMETZ

WITH THE ASSISTANCE OF

ERNST J. BERG

NEW YORK
THE W. J. JOHNSTON COMPANY
253 BROADWAY

1897

QC641
58

Engineering
Library

COPYRIGHT, 1897,

BY

THE W. J. JOHNSTON COMPANY.

Gift of
Daughter of William Stuart Smith, U.S. Navy,
to

ENGINEERING LIBRARY

LBC

DEDICATED
TO THE
MEMORY OF MY FATHER,
CARL HEINRICH STEINMETZ.

866778

PREFACE.

THE following volume is intended as an exposition of the methods which I have found useful in the theoretical investigation and calculation of the manifold phenomena taking place in alternating-current circuits, and of their application to alternating-current apparatus.

While the book is not intended as first instruction for a beginner, but presupposes some knowledge of electrical engineering, I have endeavored to make it as elementary as possible, and have therefore only used common algebra and trigonometry, practically excluding calculus, except in §§ 106 to 115 and Appendix II.; and even §§ 106 to 115 have been paralleled by the elementary approximation of the same phenomenon in §§ 102 to 105.

All the methods used in the book have been introduced and explicitly discussed, with instances of their application, the first part of the book being devoted to this. In the investigation of alternating-current phenomena and apparatus, one method only has usually been employed, though the other available methods are sufficiently explained to show their application.

A considerable part of the book is necessarily devoted to the application of complex imaginary quantities, as the method which I found most useful in dealing with alternating-current phenomena; and in this regard the book may be considered as an expansion and extension of my paper on the application of complex imaginary quantities to electrical engineering, read before the International Electrical Con-

gress at Chicago, 1893. The complex imaginary quantity is gradually introduced, with full explanations, the algebraic operations with complex quantities being discussed in Appendix I., so as not to require from the reader any previous knowledge of the algebra of the complex imaginary plane.

While those phenomena which are characteristic to polyphase systems, as the resultant action of the phases, the effects of unbalancing, the transformation of polyphase systems, etc., have been discussed separately in the last chapters, many of the investigations in the previous parts of the book apply to polyphase systems as well as single-phase circuits, as the chapters on induction motors, generators, synchronous motors, etc.

A part of the book is original investigation, either published here for the first time, or collected from previous publications and more fully explained. Other parts have been published before by other investigators, either in the same, or more frequently in a different form.

I have, however, omitted altogether literary references, for the reason that incomplete references would be worse than none, while complete references would entail the expenditure of much more time than is at my disposal, without offering sufficient compensation; since I believe that the reader who wants information on some phenomenon or apparatus is more interested in the information than in knowing who first investigated the phenomenon.

Special attention has been given to supply a complete and extensive index for easy reference, and to render the book as free from errors as possible. Nevertheless, it probably contains some errors, typographical and otherwise; and I will be obliged to any reader who on discovering an error or an apparent error will notify me.

I take pleasure here in expressing my thanks to Messrs. W. D. WEAVER, A. E. KENNELLY, and TOWNSEND WOLCOTT, for the interest they have taken in the book while in the course of publication, as well as for the valuable assist-

ance given by them in correcting and standardizing the notation to conform with the international system, and numerous valuable suggestions regarding desirable improvements.

Thanks are due also to the publishers, who have spared no effort or expense to make the book as creditable as possible mechanically.

CHARLES PROTEUS STEINMETZ.

January, 1897.

CONTENTS.

CHAP. I. Introduction. —

- § 1, p. 1. Fundamental laws of continuous current circuits.
- § 2, p. 2. Impedance, reactance, effective resistance.
- § 3, p. 3. Electro-magnetism as source of reactance.
- § 4, p. 5. Capacity as source of reactance.
- § 5, p. 6. Joule's law and power equation of alternating circuit.
- § 6, p. 6. Fundamental wave and higher harmonics, alternating waves with and without even harmonics.
- § 7, p. 9. Alternating waves as sine waves.

CHAP. II. Instantaneous Values and Integral Values. —

- § 8, p. 11. Integral values of wave.
- § 9, p. 13. Ratio of mean to maximum to effective value of wave.

CHAP. III. Law of Electro-magnetic Induction. —

- § 11, p. 16. Induced E.M.F. mean value.
- § 12, p. 17. Induced E.M.F. effective value.
- § 13, p. 18. Inductance and reactance.

CHAP. IV. Graphic Representation. —

- § 14, p. 19. Polar characteristic of alternating wave.
- § 15, p. 20. Polar characteristic of sine wave.
- § 16, p. 21. Parallelogram of sine waves, Kirchhoff's laws, and energy equation.
- § 17, p. 23. Non-inductive circuit fed over inductive line, instance.
- § 18, p. 24. Counter E.M.F. and component of impressed E.M.F.
- § 19, p. 26. Continued.
- § 20, p. 26. Inductive circuit and circuit with leading current fed over inductive line. Alternating-current generator.
- § 21, p. 28. Polar diagram of alternating-current transformer, instance.
- § 22, p. 30. Continued.

CHAP. V. Symbolic Method. —

- § 23, p. 33. Disadvantage of graphic method for numerical calculation.
- § 24, p. 34. Trigonometric calculation.
- § 25, p. 34. Rectangular components of vectors.
- § 26, p. 36. Introduction of j as distinguishing index.
- § 27, p. 36. Rotation of vector by 180° and 90° . $j = \sqrt{-1}$.

CHAP. V. Symbolic Method — Continued. —

- § 28, p. 37. Combination of sine waves in symbolic expression.
- § 29, p. 38. Resistance, reactance, impedance in symbolic expression.
- § 30, p. 40. Capacity reactance in symbolic representation.
- § 31, p. 40. Kirchhoff's laws in symbolic representation.
- § 32, p. 41. Circuit supplied over inductive line, instance.

CHAP. VI. Topographic Method. —

- § 33, p. 43. Ambiguity of vectors.
- § 34, p. 44. Instance of a three-phase system.
- § 35, p. 46. Three-phase generator on balanced load.
- § 36, p. 48. Three-phase generator on unbalanced load.
- § 37, p. 50. Quarter-phase system with common return.

CHAP. VII. Admittance, Conductance, Susceptance. —

- § 38, p. 52. Combination of resistances and conductances in series and in parallel.
- § 39, p. 53. Combination of impedances. Admittance, conductance, susceptance.
- § 40, p. 54. Relation between impedance, resistance, reactance, and admittance, conductance, susceptance.
- § 41, p. 56. Dependence of admittance, conductance, susceptance, upon resistance and reactance. Combination of impedances and admittances.

CHAP. VIII. Circuits containing Resistance, Inductance, and Capacity. —

- § 42, p. 58. Introduction.
- § 43, p. 58. Resistance in series with circuit.
- § 44, p. 60. Discussion of instances.
- § 45, p. 61. Reactance in series with circuit.
- § 46, p. 64. Discussion of instances.
- § 47, p. 66. Reactance in series with circuit.
- § 48, p. 68. Impedance in series with circuit.
- § 49, p. 69. Continued.
- § 50, p. 71. Instance.
- § 51, p. 72. Compensation for lagging currents by shunted condensation.
- § 52, p. 73. Complete balance by variation of shunted condensation.
- § 53, p. 75. Partial balance by constant shunted condensation.
- § 54, p. 76. Constant potential — constant current transformation.
- § 55, p. 79. Constant current — constant potential transformation.
- § 56, p. 81. Efficiency of constant potential — constant current transformation.

CHAP. IX. Resistance and Reactance of Transmission Lines. —

- § 57, p. 83. Introduction.
- § 58, p. 84. Non-inductive receiver circuit supplied over inductive line.
- § 59, p. 86. Instance.

CHAP. IX. Resistance and Reactance of Transmission Lines —

Continued. —

- § 60, p. 87. Maximum power supplied over inductive line.
- § 61, p. 88. Dependence of output upon the susceptance of the receiver circuit.
- § 62, p. 89. Dependence of output upon the conductance of the receiver circuit.
- § 63, p. 90. Summary.
- § 64, p. 92. Instance.
- § 65, p. 93. Condition of maximum efficiency.
- § 66, p. 96. Control of receiver voltage by shunted susceptance.
- § 67, p. 97. Compensation for line drop by shunted susceptance.
- § 68, p. 97. Maximum output and discussion.
- § 69, p. 98. Instances.
- § 70, p. 101. Maximum rise of potential in receiver circuit.
- § 71, p. 102. Summary and instances.

CHAP. X. Effective Resistance and Reactance. —

- § 72, p. 104. Effective resistance, reactance, conductance, and susceptance.
- § 73, p. 105. Sources of energy-losses in alternating-current circuits.
- § 74, p. 106. Magnetic hysteresis.
- § 75, p. 107. Hysteretic cycles and corresponding current waves.
- § 76, p. 111. Action of air-gap and of induced current on hysteretic distortion.
- § 77, p. 111. Equivalent sine wave and wattless higher harmonic.
- § 78, p. 113. True and apparent magnetic characteristic.
- § 79, p. 115. Angle of hysteretic advance of phase.
- § 80, p. 116. Loss of energy by molecular magnetic friction.
- § 81, p. 119. Effective conductance, due to magnetic hysteresis.
- § 82, p. 122. Absolute admittance of ironclad circuits and angle of hysteretic advance.
- § 83, p. 124. Magnetic circuit containing air-gap.
- § 84, p. 125. Electric constants of circuit containing iron.
- § 85, p. 127. Conclusion.

CHAP. XI. Foucault or Eddy Currents. —

- § 86, p. 129. Effective conductance of eddy currents.
- § 87, p. 130. Advance angle of eddy currents.
- § 88, p. 131. Loss of power by eddy currents, and coefficient of eddy currents.
- § 89, p. 131. Laminated iron.
- § 90, p. 133. Iron wire.
- § 91, p. 135. Comparison of sheet iron and iron wire.
- § 92, p. 136. Demagnetizing or screening effect of eddy currents.
- § 93, p. 138. Continued.
- § 94, p. 138. Large eddy currents.

CHAP. XI. Foucault or Eddy Currents — Continued. —

- § 95, p. 139. Eddy currents in conductor and unequal current distribution.
- § 96, p. 140. Continued.
- § 97, p. 142. Mutual inductance.
- § 98, p. 144. Dielectric and electrostatic phenomena.
- § 99, p. 145. Dielectric hysteretic admittance, impedance, lag, etc.
- § 100, p. 147. Electrostatic induction or influence.
- § 101, p. 148. Energy components and wattless components.

CHAP. XII. Distributed Capacity, Inductance, Resistance, and Leakage. —

- § 102, p. 150. Introduction.
- § 103, p. 151. Magnitude of charging current of transmission lines.
- § 104, p. 152. Line capacity represented by one condenser shunted across middle of line.
- § 105, p. 153. Line capacity represented by three condensers.
- § 106, p. 155. Complete investigation of distributed capacity, inductance, leakage, and resistance.
- § 107, p. 157. Continued.
- § 108, p. 158. Continued.
- § 109, p. 158. Continued.
- § 110, p. 159. Continued.
- § 111, p. 161. Continued.
- § 112, p. 161. Continued.
- § 113, p. 162. Difference of phase at any point of line.
- § 114, p. 163. Instance.
- § 115, p. 165. Particular cases, open circuit at end of line, line grounded at end, infinitely long conductor, generator feeding into closed circuit.

CHAP. XIII. The Alternating-Current Transformer. —

- § 116, p. 167. General.
- § 117, p. 167. Mutual inductance and self-inductance of transformer.
- § 118, p. 168. Magnetic circuit of transformer.
- § 119, p. 169. Continued.
- § 120, p. 170. Polar diagram of transformer.
- § 121, p. 172. Instance.
- § 122, p. 176. Diagram for varying load.
- § 123, p. 177. Instance.
- § 124, p. 178. Symbolic method, equations.
- § 125, p. 180. Continued.
- § 126, p. 182. Apparent impedance of transformer. Transformer equivalent to divided circuit.
- § 127, p. 183. Continued.
- § 128, p. 186. Transformer on non-inductive load.
- § 129, p. 188. Constants of transformer on non-inductive load.
- § 130, p. 191. Numerical instance.

CHAP. XIV. **General Alternating-Current Transformer.** —

- § 131, p. 194. Introduction.
- § 132, p. 194. Magnetic cross-flux or self-induction of transformer.
- § 133, p. 195. Mutual flux of transformer.
- § 134, p. 195. Difference of frequency between primary and secondary of general alternate-current transformer.
- § 135, p. 195. Equations of general alternate-current transformer.
- § 136, p. 201. Power, output and input, mechanical and electrical.
- § 137, p. 202. Continued.
- § 138, p. 203. Speed and output.
- § 139, p. 205. Numerical instance.

CHAP. XV. **Induction Motor.** —

- § 140, p. 207. Slip and secondary frequency.
- § 141, p. 208. Equations of induction motor.
- § 142, p. 209. Magnetic flux, admittance, and impedance.
- § 143, p. 211. E.M.F.
- § 144, p. 213. Graphic representation.
- § 145, p. 214. Continued.
- § 146, p. 216. Torque and power.
- § 147, p. 218. Power of induction motors.
- § 148, p. 219. Maximum torque.
- § 149, p. 221. Continued.
- § 150, p. 222. Maximum power.
- § 151, p. 224. Starting torque.
- § 152, p. 225. Continued.
- § 153, p. 227. Starting resistance.
- § 154, p. 228. Synchronism.
- § 155, p. 228. Near synchronism.
- § 156, p. 229. Induction generator.
- § 157, p. 229. Comparison of induction generator and synchronous generator.
- § 158, p. 230. Numerical instance of induction motor.

CHAP. XVI. **Alternate-Current Generator.** —

- § 159, p. 234. General.
- § 160, p. 235. Magnetic reaction of lag and lead.
- § 161, p. 237. Self-inductance of alternator.
- § 162, p. 238. Synchronous reactance.
- § 163, p. 238. Equations of alternator.
- § 164, p. 239. Numerical instance, field characteristic.
- § 165, p. 244. Dependence of terminal voltage on phase relation.
- § 166, p. 244. Constant potential regulation.
- § 167, p. 246. Constant current regulation, maximum output.

CHAP. XVII. **Synchronizing Alternators.** —

- § 168, p. 248. Introduction.
- § 169, p. 248. Rigid mechanical connection.

CHAP. XVII. **Synchronous Motor** — *Continued.* —

- § 170, p. 248. Uniformity of speed.
- § 171, p. 249. Synchronizing.
- § 172, p. 250. Running in synchronism.
- § 173, p. 250. Series operation of alternators.
- § 174, p. 251. Equations of synchronous running alternators, synchronizing power.
- § 175, p. 254. Special case of equal alternators at equal excitation.
- § 176, p. 257. Numerical instance.

CHAP. XVIII. **Synchronous Motor.** —

- § 177, p. 258. Graphic method.
- § 178, p. 260. Continued.
- § 179, p. 262. Instance.
- § 180, p. 263. Constant impressed E.M.F. and constant current.
- § 181, p. 266. Constant impressed and counter E.M.F.
- § 182, p. 269. Constant impressed E.M.F. and maximum efficiency.
- § 183, p. 271. Constant impressed E.M.F. and constant output.
- § 184, p. 275. Analytical method. Fundamental equations and power characteristic.
- § 185, p. 279. Maximum output.
- § 186, p. 280. No load.
- § 187, p. 282. Minimum current.
- § 188, p. 284. Maximum displacement of phase.
- § 189, p. 286. Constant counter E.M.F.
- § 190, p. 286. Numerical instance.
- § 191, p. 288. Discussion of results.

CHAP. XIX. **Commutator Motors.** —

- § 192, p. 291. Types of commutator motors.
- § 193, p. 291. Repulsion motor as induction motor.
- § 194, p. 293. Two types of repulsion motors.
- § 195, p. 295. Definition of repulsion motor.
- § 196, p. 296. Equations of repulsion motor.
- § 197, p. 297. Continued.
- § 198, p. 298. Power of repulsion motor. Instance.
- § 199, p. 300. Series motor, shunt motor.
- § 200, p. 303. Equations of series motor.
- § 201, p. 304. Numerical instance.
- § 202, p. 305. Shunt motor.
- § 203, p. 307. Power factor of series motor.

CHAP. XX. **Reaction Machines.** —

- § 204, p. 308. General discussion.
- § 205, p. 309. Energy component of reactance.
- § 206, p. 309. Hysteretic energy component of reactance.
- § 207, p. 310. Periodic variation of reactance.

CHAP. XX. **Reaction Machines — Continued.** —

- § 208, p. 312. Distortion of wave-shape.
- § 209, p. 314. Unsymmetrical distortion of wave-shape.
- § 210, p. 315. Equations of reaction machines.
- § 211, p. 317. Numerical instance.

CHAP. XXI. **Distortion of Wave-Shape and its Causes.** —

- § 212, p. 320. Equivalent sine wave.
- § 213, p. 320. Cause of distortion.
- § 214, p. 321. Lack of uniformity and pulsation of magnetic field.
- § 215, p. 324. Continued.
- § 216, p. 327. Pulsation of reactance.
- § 217, p. 327. Pulsation of reactance in reaction machine.
- § 218, p. 329. General discussion.
- § 219, p. 329. Pulsation of resistance, arc.
- § 220, p. 331. Instance.
- § 221, p. 332. Distortion of wave-shape by arc.
- § 222, p. 333. Discussion.

CHAP. XXII. **Effects of Higher Harmonics.** —

- § 223, p. 334. Distortion of wave-shape by triple and quintuple harmonics. Some characteristic wave-shapes.
- § 224, p. 337. Effect of self-induction and capacity on higher harmonics.
- § 225, p. 338. Resonance due to higher harmonics in transmission lines.
- § 226, p. 341. Power of complex harmonic waves.
- § 227, p. 341. Three-phase generator.
- § 228, p. 343. Decrease of hysteresis by distortion of wave-shape.
- § 229, p. 343. Increase of hysteresis by distortion of wave-shape.
- § 230, p. 344. Eddy currents.
- § 231, p. 344. Effect of distorted waves on insulation.

CHAP. XXIII. **General Polyphase Systems.** —

- § 232, p. 346. Definition of systems, symmetrical and unsymmetrical systems.
- § 233, p. 346. Flow of power. Balanced and unbalanced systems. Independent and interlinked systems. Star connection and ring connection.
- § 234, p. 348. Classification of polyphase systems.

CHAP. XXIV. **Symmetrical Polyphase Systems.** —

- § 235, p. 350. General equations of symmetrical system.
- § 236, p. 351. Particular systems.
- § 237, p. 352. Resultant M.M.F. of symmetrical system.
- § 238, p. 355. Particular systems.

CHAP. XXV. **Balanced and Unbalanced Polyphase Systems.** —

- § 239, p. 356. Flow of power in single-phase system.
- § 240, p. 357. Flow of power in polyphase systems, balance factor of system.

CHAP. XXV. Balanced and Unbalanced Polyphase Systems — *Continued.* —

- § 241, p. 358. Balance factor.
- § 242, p. 358. Three-phase system, quarter-phase system.
- § 243, p. 359. Inverted three-phase system.
- § 244, p. 360. Diagrams of flow of power.
- § 245, p. 363. Monocyclic and polycyclic systems.
- § 246, p. 363. Power characteristic of alternating-current system.
- § 247, p. 364. The same in rectangular coördinates.
- § 248, p. 366. Main power axes of alternating-current system.

CHAP. XXVI. Interlinked Polyphase Systems. —

- § 249, p. 368. Interlinked and independent systems.
- § 250, p. 368. Star connection and ring connection. Y connection and delta connection.
- § 251, p. 370. Continued.
- § 252, p. 371. Star potential and ring potential. Star current and ring current. Y potential and Y current, delta potential and delta current.
- § 253, p. 371. Equations of interlinked polyphase systems.
- § 254, p. 373. Continued.

CHAP. XXVII. Transformation of Polyphase Systems. —

- § 255, p. 376. Constancy of balance factor.
- § 256, p. 376. Equations of transformation of polyphase systems.
- § 257, p. 378. Three-phase, quarter-phase transformation.
- § 258, p. 379. Transformation with change of balance factor.

CHAP. XXVIII. Copper Efficiency of Systems. —

- § 259, p. 380. General discussion.
- § 260, p. 381. Comparison on the basis of equality of minimum difference of potential.
- § 261, p. 386. Comparison on the basis of equality of maximum difference of potential.
- § 262, p. 388. Continued.

CHAP. XXIX. Three-phase System. —

- § 263, p. 390. General equations.
- § 264, p. 393. Special cases: balanced system, one branch loaded, two branches loaded.

CHAP. XXX. Quarter-phase System. —

- § 265, p. 395. General equations.
- § 266, p. 396. Special cases: balanced system, one branch loaded.

APPENDIX I. Algebra of Complex Imaginary Quantities. —

- § 267, p. 401. Introduction.
- § 268, p. 401. Numeration, addition, multiplication, involution.

APPENDIX I. **Algebra of Complex Imaginary Quantities — Continued.**

- § 269, p. 402. Subtraction, negative number.
- § 270, p. 403. Division, fraction.
- § 271, p. 403. Evolution and logarithmation.
- § 272, p. 404. Imaginary units; complex imaginary number.
- § 273, p. 404. Review.
- § 274, p. 405. Algebraic operations with complex quantities.
- § 275, p. 406. Continued.
- § 276, p. 407. Roots of the unit.
- § 277, p. 407. Rotation.
- § 278, p. 408. Complex imaginary plane.

APPENDIX II. **Oscillating Currents. —**

- § 279, p. 409. Introduction.
- § 280, p. 410. General equations.
- § 281, p. 411. Polar coördinates.
- § 282, p. 412. Loxodromic spiral.
- § 283, p. 413. Impedance and admittance.
- § 284, p. 414. Inductance.
- § 285, p. 414. Capacity.
- § 286, p. 415. Impedance.
- § 287, p. 416. Admittance.
- § 288, p. 417. Conductance and susceptance.
- § 289, p. 418. Circuits of zero impedance.
- § 290, p. 418. Continued.
- § 291, p. 419. Origin of oscillating currents.
- § 292, p. 420. Oscillating discharge.
- § 293, p. 421. Oscillating discharge of condensers.
- § 294, p. 422. Oscillating current transformer.
- § 295, p. 424. Fundamental equations thereof.

THEORY AND CALCULATION
OF
ALTERNATING-CURRENT PHENOMENA.

CHAPTER I.

INTRODUCTION.

1. IN the practical applications of electrical energy, we meet with two different classes of phenomena, due respectively to the continuous current and to the alternating current.

The continuous-current phenomena have been brought within the realm of exact analytical calculation by a few fundamental laws:—

1.) Ohm's law: $i = e/r$, where r , the resistance, is a constant of the circuit.

2.) Joule's law: $P = i^2 r$, where P is the rate at which energy is expended by the current, i , in the resistance, r .

3.) The power equation: $P_o = ei$, where P_o is the power expended in the circuit of E.M.F., e , and current, i .

4.) Kirchhoff's laws:

a.) The sum of all the E.M.Fs. in a closed circuit = 0, if the E.M.F. consumed by the resistance, ir , is also considered as a counter E.M.F., and all the E.M.Fs. are taken in their proper direction.

b.) The sum of all the currents flowing towards a distributing point = 0.

In alternating-current circuits, that is, in circuits conveying currents which rapidly and periodically change their

direction, these laws cease to hold. Energy is expended, not only in the conductor through its ohmic resistance, but also outside of it; energy is stored up and returned, so that large currents may flow, impressed by high E.M.Fs., without representing any considerable amount of expended energy, but merely a surging to and fro of energy; the ohmic resistance ceases to be the determining factor of current strength; currents may divide into components, each of which is larger than the undivided current, etc.

2. In place of the above-mentioned fundamental laws of continuous currents, we find in alternating-current circuits the following :

Ohm's law assumes the form, $i = e/z$, where z , the apparent resistance, or *impedance*, is no longer a constant of the circuit, but depends upon the frequency of the currents; and in circuits containing iron, etc., also upon the E.M.F.

Impedance, z , is, in the system of absolute units, of the same dimensions as resistance (that is, of the dimension $LT^{-1} = \text{velocity}$), and is expressed in ohms.

It consists of two components, the resistance, r , and the reactance, x , or —

$$z = \sqrt{r^2 + x^2}.$$

The resistance, r , in circuits where energy is expended only in heating the conductor, is the same as the ohmic resistance of continuous-current circuits. In circuits, however, where energy is also expended outside of the conductor by magnetic hysteresis, mutual inductance, dielectric hysteresis, etc., r is larger than the true ohmic resistance of the conductor, since it refers to the total expenditure of energy. It may be called then the *effective resistance*. It is no longer a constant of the circuit.

The reactance, x , does not represent the expenditure of power, as does the effective resistance, r , but merely the surging to and fro of energy. It is not a constant of the

circuit, but depends upon the frequency, and frequently, as in circuits containing iron, or in electrolytic conductors, upon the E.M.F. also. Hence, while the effective resistance, r , refers to the energy component of E.M.F., or the E.M.F. in phase with the current, the reactance, x , refers to the wattless component of E.M.F., or the E.M.F. in quadrature with the current.

3. The principal sources of reactance are electro-magnetism and capacity.

ELECTRO-MAGNETISM.

An electric current, i , flowing through a circuit, produces a magnetic flux surrounding the conductor in lines of magnetic force (or more correctly, lines of magnetic induction), of closed, circular, or other form, which alternate with the alternations of the current, and thereby induce an E.M.F. in the conductor. Since the magnetic flux is in phase with the current, and the induced E.M.F. 90° , or a quarter period, behind the flux, this *E.M.F. of self-inductance* lags 90° , or a quarter period, behind the current; that is, is in quadrature therewith, and therefore wattless.

If now Φ = the magnetic flux produced by, and interlinked with, the current i (where those lines of magnetic force, which are interlinked n -fold, or pass around n turns of the conductor, are counted n times), the ratio, Φ/i , is denoted by L , and called *self-inductance*, or the *coefficient of self-induction* of the circuit. It is numerically equal, in absolute units, to the interlinkages of the circuit with the magnetic flux produced by unit current, and is, in the system of absolute units, of the dimension of length. Instead of the self-inductance, L , sometimes its ratio with the ohmic resistance, r , is used, and is called the *Time-Constant* of the circuit:

$$T = \frac{L}{r}.$$

If a conductor surrounds with n turns a magnetic circuit of reluctance, \mathcal{R} , the current, i , in the conductor represents the M.M.F. of ni ampere-turns, and hence produces a magnetic flux of ni/\mathcal{R} lines of magnetic force, surrounding each n turns of the conductor, and thereby giving $\Phi = n^2 i/\mathcal{R}$ interlinkages between the magnetic and electric circuits. Hence the inductance is $L = \Phi/i = n^2/\mathcal{R}$.

The fundamental law of electro-magnetic induction is, that the E.M.F. induced in a conductor by a varying magnetic field is the rate of cutting of the conductor through the magnetic field.

Hence, if i is the current, and L is the inductance of a circuit, the magnetic flux interlinked with a circuit of current, i , is Li , and $4NLi$ is consequently the average rate of cutting; that is, the number of lines of force cut by the conductor per second, where N = frequency, or number of complete periods (double reversals) of the current per second.

Since the maximum rate of cutting bears to the average rate the same ratio as the quadrant to the radius of a circle (a sinusoidal variation supposed), that is the ratio $\pi/2 \div 1$, the maximum rate of cutting is $2\pi N$, and, consequently, the maximum value of E.M.F. induced in a circuit of maximum current strength, i , and inductance, L , is,

$$e = 2\pi NLi.$$

Since the maximum values of sine waves are proportional (by factor $\sqrt{2}$) to the effective values (square root of mean squares), if i = effective value of alternating current, $e = 2\pi NLi$ is the effective value of E.M.F. of self-inductance, and the ratio, $e/i = 2\pi NL$, is the magnetic reactance:

$$x_m = 2\pi NL.$$

Thus, if r = resistance, x_m = reactance, z = impedance,—

the E.M.F. consumed by resistance is: $e_1 = ir$;

the E.M.F. consumed by reactance is: $e_2 = ix_m$;

and, since both E.M.F.s. are in quadrature to each other, the total E.M.F. is —

$$e = \sqrt{e_1^2 + e_2^2} = i \sqrt{r^2 + x_m^2} = iz;$$

that is, the impedance, z , takes in alternating-current circuits the place of the resistance, r , in continuous-current circuits.

CAPACITY.

4. If upon a condenser of capacity, C , an E.M.F., e , is impressed, the condenser receives the electrostatic charge, Ce .

If the E.M.F., e , alternates with the frequency, N , the average rate of charge and discharge is $4N$, and $2\pi N$ the maximum rate of charge and discharge, sinusoidal waves supposed, hence, $i = 2\pi NCe$ the current passing into the condenser, which is in quadrature to the E.M.F., and leading.

It is then :—
$$x_c = \frac{e}{i} = \frac{1}{2\pi NC},$$

the capacity reactance, or condensance.

Polarization in electrolytic conductors acts to a certain extent like capacity.

The capacity reactance is inversely proportional to the frequency, and represents the leading out-of-phase wave; the magnetic reactance is directly proportional to the frequency, and represents the lagging out-of-phase wave. Hence both are of opposite sign with regard to each other, and the total reactance of the circuit is their difference, $x = x_m - x_c$.

The total resistance of a circuit is equal to the sum of all the resistances connected in series; the total reactance of a circuit is equal to the algebraic sum of all the reactances connected in series; the total impedance of a circuit, however, is not equal to the sum of all the individual impedances, but in general less, and is the resultant of the total resistance and the total reactance. Hence it is not permissible directly to add impedances, as it is with resistances or reactances.

A further discussion of these quantities will be found in the later chapters.

5. In Joule's law, $P = i^2 r$, r is not the true ohmic resistance any more, but the "effective resistance;" that is, the ratio of the energy component of E.M.F. to the current. Since in alternating-current circuits, besides by the ohmic resistance of the conductor, energy is expended, partly outside, partly even inside, of the conductor, by magnetic hysteresis, mutual inductance, dielectric hysteresis, etc., the effective resistance, r , is in general larger than the true resistance of the conductor, sometimes many times larger, as in transformers at open secondary circuit, and is not a constant of the circuit any more. It is more fully discussed in Chapter VII.

In alternating-current circuits, the power equation contains a third term, which, in sine waves, is the cosine of the difference of phase between E.M.F. and current:—

$$P_o = ei \cos \phi.$$

Consequently, even if e and i are both large, P_o may be very small, if $\cos \phi$ is small, that is, ϕ near 90° .

Kirchhoff's laws become meaningless in their original form, since these laws consider the E.M.Fs. and currents as directional quantities, counted positive in the one, negative in the opposite direction, while the alternating current has no definite direction of its own.

6. The alternating waves may have widely different shapes; some of the more frequent ones are shown in a later chapter.

The simplest form, however, is the sine wave, shown in Fig. 1, or, at least, a wave very near sine shape, which may be represented analytically by:—

$$i = I \sin \frac{2\pi}{T} (t - t_1) = I \sin 2\pi N (t - t_1);$$

where I is the maximum value of the wave, or its *amplitude*; T is the time of one complete cyclic repetition, or the *period* of the wave, or $N = 1/T$ is the *frequency* or number of complete periods per second; and t_1 is the time, where the wave is zero, or the *epoch* of the wave, generally called the *phase*.*

Obviously, "phase" or "epoch" attains a practical meaning only when several waves of different phases are considered, as "difference of phase." When dealing with one wave only, we may count the time from the moment

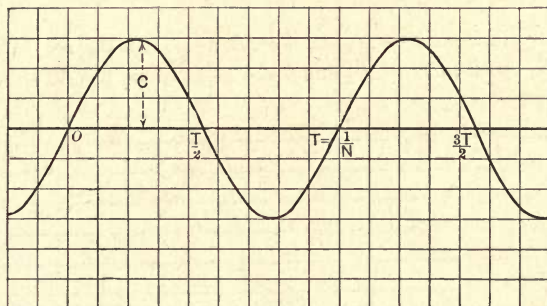


Fig. 1. Sine Wave.

where the wave is zero, or from the moment of its maximum, and then represent it by:—

$$i = I \sin 2 \pi Nt;$$

or,

$$i = I \cos 2 \pi Nt.$$

Since it is a univalent function of time, that is, can at a given instant have one value only, by Fourier's theorem, any alternating wave, no matter what its shape may be, can be represented by a series of sine functions of different frequencies and different phases, in the form:—

$$i = I_1 \sin 2 \pi N(t - t_1) + I_2 \sin 4 \pi N(t - t_2) \\ + I_3 \sin 6 \pi N(t - t_3) + \dots$$

* "Epoch" is the time where a periodic function reaches a certain value, for instance, zero; and "phase" is the angular position, with respect to a datum position, of a periodic function at a given time. Both are in alternate-current phenomena only different ways of expressing the same thing.

where I_1, I_2, I_3, \dots are the maximum values of the different components of the wave, t_1, t_2, t_3, \dots the times, where the respective components pass the zero value.

The first term, $I_1 \sin 2\pi N(t - t_1)$, is called the *fundamental wave*, or the *first harmonic*; the further terms are called the *higher harmonics*, or "overtones," in analogy to the overtones of sound waves. $I_n \sin 2n\pi N(t - t_n)$ is the n^{th} harmonic.

By resolving the sine functions of the time differences, $t - t_1, t - t_2, \dots$, we reduce the general expression of the wave to the form :

$$i = A_1 \sin 2\pi Nt + A_2 \sin 4\pi Nt + A_3 \sin 6\pi Nt + \dots \\ + B_1 \cos 2\pi Nt + B_2 \cos 4\pi Nt + B_3 \cos 6\pi Nt + \dots$$

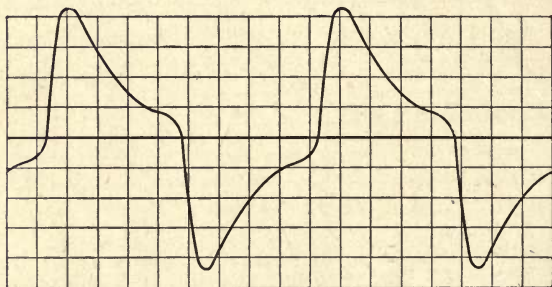


Fig. 2. Wave without Even Harmonics.

The two half-waves of each period, the *positive wave* and the *negative wave* (counting in a definite direction in the circuit), are almost always identical. Hence the even higher harmonics, which cause a difference in the shape of the two half-waves, disappear, and only the odd harmonics exist, except in very special cases.

Hence the general alternating current is expressed by :

$$i = I_1 \sin 2\pi N(t - t_1) + I_3 \sin 6\pi N(t - t_3) \\ + I_5 \sin 10\pi N(t - t_5) + \dots$$

or,

$$i = A'_1 \sin 2\pi Nt + A'_3 \sin 6\pi Nt + A'_5 \sin 10\pi Nt + \dots \\ + B_1 \cos 2\pi Nt + B_3 \cos 6\pi Nt + B_5 \cos 10\pi Nt + \dots$$

Such a wave is shown in Fig. 2, while Fig. 3 shows a wave whose half-waves are different. Figs. 2 and 3 represent the secondary currents of a Ruhmkorff coil, whose secondary coil is closed by a high external resistance: Fig. 3 is the coil operated in the usual way, by make and break of the primary battery current; Fig. 2 is the coil fed with reversed currents by a commutator from a battery.

7. Self-inductance, or electro-magnetic momentum, which is always present in alternating-current circuits, — to a large extent in generators, transformers, etc., — tends to

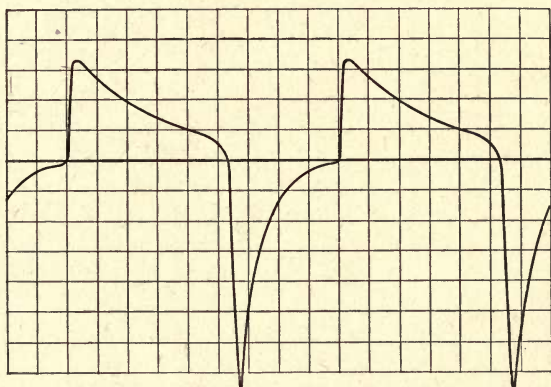


Fig. 3. Wave with Even Harmonics.

suppress the higher harmonics of a complex harmonic wave more than the fundamental harmonic, and thereby causes a general tendency towards simple sine shape, which has the effect, that, in general, the alternating currents in our light and power circuits are sufficiently near sine waves to make the assumption of sine shape permissible.

Hence, in the calculation of alternating-current phenomena, we can safely assume the alternating wave as a sine wave, without making any serious error; and it will be sufficient to keep the distortion from sine shape in mind as a possible, though improbable, disturbing factor, which

generally, however, is in practice negligible — perhaps with the only exception of low-resistance circuits containing large magnetic reactance, and large condensances in series with each other, so as to produce resonance effects of these higher harmonics.

CHAPTER II

INSTANTANEOUS VALUES AND INTEGRAL VALUES.

8. In a periodically varying function, as an alternating current, we have to distinguish between the *instantaneous value*, which varies constantly as function of the time, and the *integral value*, which characterizes the wave as a whole.

As such integral value, almost exclusively the *effective*

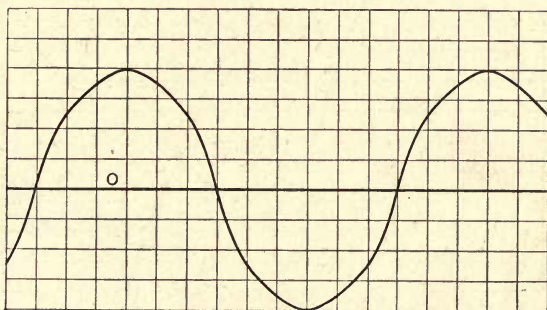


Fig. 4. Alternating Wave.

value is used, that is, the square root of the mean squares; and wherever the intensity of an electric wave is mentioned without further reference, the effective value is understood.

The *maximum value* of the wave is of practical interest only in few cases, and may, besides, be different for the two half-waves, as in Fig. 3.

As *arithmetic mean*, or *average value*, of a wave as in Figs. 4 and 5, the arithmetical average of all the instantaneous values during one complete period is understood.

This arithmetic mean is either $= 0$, as in Fig. 4, or it differs from 0, as in Fig. 5. In the first case, the wave is called an *alternating wave*, in the latter a *pulsating wave*.

Thus, an alternating wave is a wave whose positive values give the same sum total as the negative values ; that is, whose two half-waves have in rectangular coördinates the same area, as shown in Fig. 4.

A pulsating wave is a wave in which one of the half-waves preponderates, as in Fig. 5.

Pulsating waves are produced only by commutating machines, and by unipolar machines (or by the superposition of alternating waves upon continuous currents, etc.).

All inductive apparatus without commutation give exclusively alternating waves, because, no matter what con-

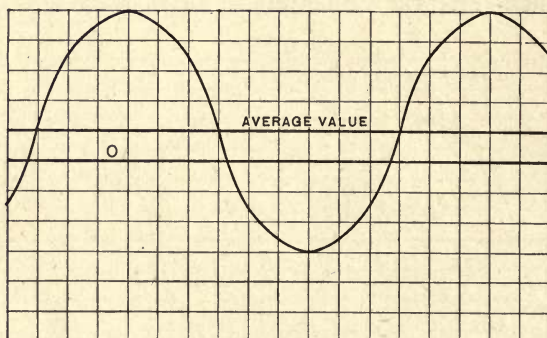


Fig. 5. Pulsating Wave.

ditions may exist in the circuit, any line of magnetic force, which during a complete period is cut by the circuit, and thereby induces an E.M.F., must during the same period be cut again in the opposite direction, and thereby induce the same total amount of E.M.F. (Obviously, this does not apply to circuits consisting of different parts movable with regard to each other, as in unipolar machines.)

In the following we shall almost exclusively consider the alternating wave, that is the wave whose true arithmetic mean value = 0.

Frequently, by mean value of an alternating wave, the average of one half-wave only is denoted, or rather the

average of all instantaneous values without regard to their sign. This *mean value* is of no practical importance, and is, besides, in many cases, indefinite.

9. In a sine wave, the relation of the mean to the maximum value is found in the following way:—

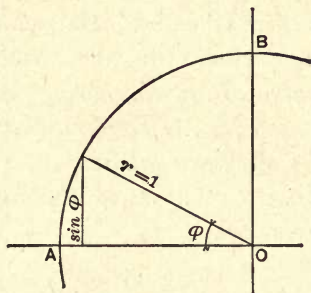


Fig. 6.

Let, in Fig. 6, AOB represent a quadrant of a circle with radius 1.

Then, while the angle ϕ traverses the arc $\pi/2$ from A to B , the sine varies from 0 to $OB = 1$. Hence the average variation of the sine bears to that of the corresponding arc the ratio $1 \div \pi/2$, or $2/\pi \div 1$. The maximum variation of the sine takes place about its zero value, where the sine is equal to the arc. Hence the maximum variation of the sine is equal to the variation of the corresponding arc, and consequently the maximum variation of the sine bears to its average variation the same ratio as the average variation of the arc to that of the sine; that is, $1 \div 2/\pi$, and since the variations of a sine-function are sinusoidal also, we have,

$$\begin{aligned} \text{Mean value of sine wave} \div \text{maximum value} &= \frac{2}{\pi} \div 1 \\ &= .63663. \end{aligned}$$

The quantities, "current," "E.M.F.," "magnetism," etc., are in reality mathematical fictions only, as the components

of the entities, "energy," "power," etc.; that is, they have no independent existence, but appear only as squares or products.

Consequently, the only integral value of an alternating wave which is of practical importance, as directly connected with the mechanical system of units, is that value which represents the same *power* or *effect* as the periodical wave. This is called the *effective value*. Its square is equal to the mean square of the periodic function, that is:—

The effective value of an alternating wave, or the value representing the same effect as the periodically varying wave, is the square root of the mean square.

In a sine wave, its relation to the maximum value is found in the following way:

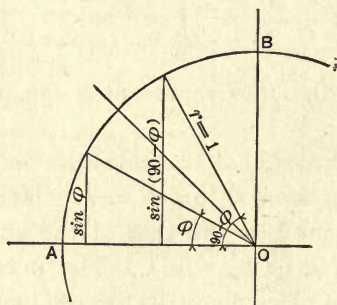


Fig. 7.

Let, in Fig. 7, AOB represent a quadrant of a circle with radius 1.

Then, since the sines of any angle ϕ and its complementary angle, $90^\circ - \phi$, fulfill the condition,—

$$\sin^2 \phi + \sin^2 (90 - \phi) = 1,$$

the sines in the quadrant, AOB , can be grouped into pairs, so that the sum of the squares of any pair = 1; or, in other words, the mean square of the sine = $1/2$, and the square root of the mean square, or the effective value of the sine, = $1/\sqrt{2}$. That is:

The effective value of a sine function bears to its maximum value the ratio, —

$$\frac{1}{\sqrt{2}} \div 1 = .70711.$$

Hence, we have for the sine curve the following relations :

MAX.	EFF.	ARITH. MEAN.	
		Half Period.	Whole Period.
1	$\frac{1}{\sqrt{2}}$	$\frac{2}{\pi}$	0
1	.7071	.63663	0
1.4142	1	.90034	0
1.5708	1.1107	1	0

10. Coming now to the general alternating curve, —

$$i = A_1 \sin 2\pi Nt + A_2 \sin 4\pi Nt + A_3 \sin 6\pi Nt + \dots \\ + B_1 \cos 2\pi Nt + B_2 \cos 4\pi Nt + B_3 \cos 6\pi Nt + \dots,$$

we find, by squaring this expression and canceling all the products which give 0 as mean square, the *effective value*, —

$$I = \sqrt{A_1^2 + A_2^2 + A_3^2 + \dots + B_1^2 + B_2^2 + B_3^2 \dots}$$

The *mean value* does not give a simple expression, and is of no general interest.

CHAPTER III.

LAW OF ELECTRO-MAGNETIC INDUCTION.

11. If an electric conductor moves relatively to a magnetic field, an E.M.F. is induced in the conductor which is proportional to the intensity of the magnetic field, to the length of the conductor, and to the speed of its motion perpendicular to the magnetic field and the direction of the conductor; or, in other words, proportional to the number of lines of magnetic force cut per second by the conductor.

As a practical unit of E.M.F., the *volt* is defined as the E.M.F. induced in a conductor, which cuts $10^8 = 100,000,000$ lines of magnetic force per second.

If the conductor is closed upon itself, the induced E.M.F. produces a current.

A closed conductor may be called a turn or a convolution. In such a turn, the number of lines of magnetic force cut per second is the increase or decrease of the number of lines inclosed by the turn, or n times as large with n turns.

Hence the E.M.F. in volts induced in n turns, or convolutions, is n times the increase or decrease, per second, of the flux inclosed by the turns, times 10^{-8} .

If the change of the flux inclosed by the turn, or by n turns, does not take place uniformly, the product of the number of turns, times change of flux per second, gives the average E.M.F.

If the magnetic flux, Φ , alternates relatively to a number of turns, n — that is, when the turns either revolve through the flux, or the flux passes in and out of the turns, during each complete alternation or cycle, — the total flux is cut four times, twice passing into, and twice out of, the turns.

Hence, if N = number of complete cycles per second, or the frequency of the relative alternation of flux Φ , the average E.M.F. induced in n turns is, —

$$E_{\text{avg.}} = 4 n \Phi N 10^{-8} \text{ volts.}$$

This is the fundamental equation of electrical engineering, and applies to continuous-current, as well as to alternating-current, apparatus.

12. In continuous-current machines and in many alternators, the turns revolve through a constant magnetic field; in other alternators and in induction motors, the magnetic field revolves; in transformers, the field alternates with respect to the stationary turns.

Thus, in the continuous-current machine, if n = number of turns in series from brush to brush, Φ = flux inclosed per turn, and N = frequency, the E.M.F. induced in the machine is $E = 4n \Phi N 10^{-8}$ volts, independent of the number of poles, or series or multiple connection of the armature, whether of the ring, drum, or other type.

In an alternator or transformer, if n is the number of turns in series, Φ the maximum flux inclosed per turn, and N the frequency, this formula gives,

$$E_{\text{avg.}} = 4 n \Phi N 10^{-8} \text{ volts.}$$

Since the maximum E.M.F. is given by, —

$$E_{\text{max.}} = \frac{\pi}{2} \text{ avg. } E,$$

we have

$$E_{\text{max.}} = 2 \pi n \Phi N 10^{-8} \text{ volts.}$$

And since the effective E.M.F. is given by, —

$$E_{\text{eff.}} = \frac{E_{\text{max.}}}{\sqrt{2}}$$

we have

$$\begin{aligned} E_{\text{eff.}} &= \sqrt{2} \pi n \Phi N 10^{-8} \\ &= 4.44 n \Phi N 10^{-8} \text{ volts,} \end{aligned}$$

which is the fundamental formula of alternating-current induction by sine waves.

13. If, in a circuit of n turns, the magnetic flux, Φ , inclosed by the circuit is produced by the current flowing in the circuit, the ratio —

$$\frac{\text{flux} \times \text{number of turns} \times 10^{-8}}{\text{current}}$$

is called the *inductance*, L , of the circuit, in henrys.

The product of the number of turns, n , into the maximum flux, Φ , produced by a current of I amperes effective, or $I\sqrt{2}$ amperes maximum, is therefore —

$$n\Phi = LI\sqrt{2} 10^8;$$

and consequently the effective E.M.F. of self-inductance is :

$$\begin{aligned} E &= \sqrt{2} \pi n \Phi N 10^{-8} \\ &= 2 \pi NLI \text{ volts.} \end{aligned}$$

The product, $x = 2 \pi NL$, is of the dimension of resistance, and is called the *reactance* of the circuit; and the E.M.F. of self-inductance of the circuit, or the reactance voltage, is

$$E = Ix,$$

and lags 90° behind the current, since the current is in phase with the magnetic flux produced by the current, and the E.M.F. lags 90° behind the magnetic flux. The E.M.F. lags 90° behind the magnetic flux, as it is proportional to the change in flux; thus it is zero when the magnetism is at its maximum value, and a maximum when the flux passes through zero, where it changes quickest.

CHAPTER IV.

GRAPHIC REPRESENTATION.

14. While alternating waves can be, and frequently are, represented graphically in rectangular coördinates, with the time as abscissæ, and the instantaneous values of the wave as ordinates, the best insight with regard to the mutual relation of different alternate waves is given by their representation in polar coördinates, with the time as an angle or the amplitude, — one complete period being represented by one revolution, — and the instantaneous values as radii vectores.

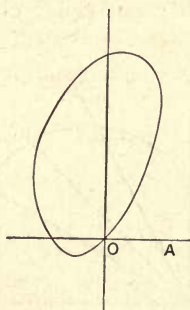


Fig. 8.

Thus the two waves of Figs. 2 and 3 are represented in polar coördinates in Figs. 8 and 9 as closed characteristic curves, which, by their intersection with the radius vector, give the instantaneous value of the wave, corresponding to the time represented by the amplitude of the radius vector.

These instantaneous values are positive if in the direction of the radius vector, and negative if in opposition. Hence the two half-waves in Fig. 2 are represented by the same

polar characteristic curve, which is traversed by the point of intersection of the radius vector twice per period, — once in the direction of the vector, giving the positive half-wave,

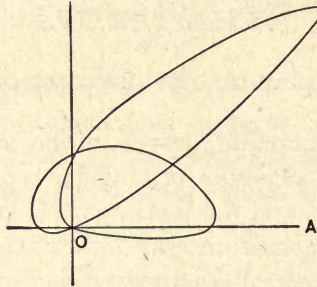


Fig. 9.

and once in opposition to the vector, giving the negative half-wave. In Figs. 3 and 9, where the two half-waves are different, they give different polar characteristics.

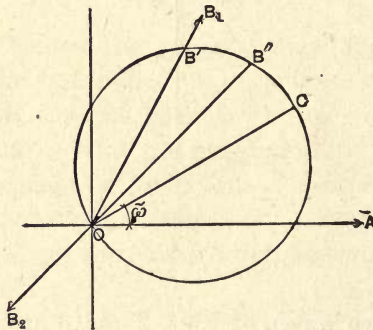


Fig. 10.

15. The sine wave, Fig. 1, is represented in polar coordinates by one circle, as shown in Fig. 10. The diameter of the characteristic curve of the sine wave, $I = \overline{OC}$, represents the *intensity* of the wave; and the amplitude of the diameter, \overline{OC} , $\angle \hat{\omega} = AOC$, is the *phase* of the

wave, which, therefore, is represented analytically by the function :—

$$i = I \cos (\phi - \hat{\omega}),$$

where $\phi = 2\pi t / T$ is the instantaneous value of the amplitude corresponding to the instantaneous value, i , of the wave.

The instantaneous values are cut out on the movable radius vector by its intersection with the characteristic circle. Thus, for instance, at the amplitude $AOB_1 = \phi_1 = 2\pi t_1 / T$ (Fig. 10), the instantaneous value is \overline{OB}' ; at the amplitude $AOB_2 = \phi_2 = 2\pi t_2 / T$, the instantaneous value is \overline{OB}'' , and negative, since in opposition to the vector OB_2 .

The characteristic circle of the alternating sine wave is determined by the length of its diameter — the intensity of the wave, and by the amplitude of the diameter — the phase of the wave.

Hence, wherever the integral value of the wave is considered alone, and not the instantaneous values, the characteristic circle may be omitted altogether, and the wave represented in intensity and in phase by the diameter of the characteristic circle.

Thus, in polar coördinates, the alternate wave is represented in intensity and phase by the length and direction of a vector, \overline{OC} , Fig. 10.

Instead of the maximum value of the wave, the *effective* value, or square root of mean square, may be used as the vector, which is more convenient; and the maximum value is then $\sqrt{2}$ times the vector \overline{OC} , so that the instantaneous values, when taken from the diagram, have to be increased by the factor $\sqrt{2}$.

16. To combine different sine waves, their graphical representations, or vectors, are combined by the parallelogram law.

If, for instance, two sine waves, \overline{OB} and \overline{OC} (Fig. 11), are superposed, — as, for instance, two E.M.Fs. acting in the same circuit, — their resultant wave is represented by

\overline{OD} , the diagonal of a parallelogram with \overline{OB} and \overline{OC} as sides.

For at any time, t , represented by angle $\phi = AOX$, the instantaneous values of the three waves, \overline{OB} , \overline{OC} , \overline{OD} , are their projections upon \overline{OX} , and the sum of the projections of \overline{OB} and \overline{OC} is equal to the projection of \overline{OD} ; that is, the instantaneous values of the wave \overline{OD} are equal to the sum of the instantaneous values of waves \overline{OB} and \overline{OC} .

From the foregoing considerations we have the conclusions :

The sine wave is represented graphically in polar coördinates by a vector, which by its length, \overline{OC} , denotes the in-

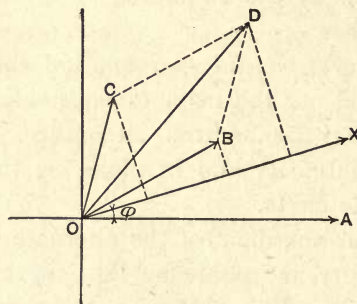


Fig. 11.

tensity, and by its amplitude, AOC , the phase, of the sine wave.

Sine waves are combined or resolved graphically, in polar coördinates, by the law of parallelogram or the polygon of sine waves.

Kirchhoff's laws now assume, for alternating sine waves, the form :—

a.) The resultant of all the E.M.Fs. in a closed circuit, as found by the parallelogram of sine waves, is zero if the counter E.M.Fs. of resistance and of reactance are included.

b.) The resultant of all the currents flowing towards a

distributing point, as found by the parallelogram of sine waves, is zero.

The energy equation expressed graphically is as follows :

The power of an alternating-current circuit is represented in polar coördinates by the product of the current ; I , into the projection of the E.M.F., E , upon the current, or by the E.M.F., E , into the projection of the current, I , upon the E.M.F., or $IE \cos (I_1 E)$.

17. Suppose, as an instance, that over a line having the resistance, r , and the reactance, $x = 2\pi NL$, — where $N =$ frequency and $L =$ inductance, — a current of I amperes be sent into a non-inductive circuit at an E.M.F. of E

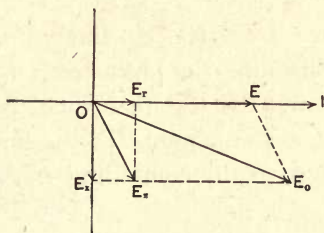


Fig. 12.

volts. What will be the E.M.F. required at the generator end of the line ?

In the polar diagram, Fig. 12, let the phase of the current be assumed as the initial or zero line, \overline{OI} . Since the receiving circuit is non-inductive, the current is in phase with its E.M.F. Hence the E.M.F., E , at the end of the line, impressed upon the receiving circuit, is represented by a vector, \overline{OE} . To overcome the resistance, r , of the line, an E.M.F., I_r , is required in phase with the current, represented by $\overline{OE_r}$, in the diagram. The self-inductance of the line induces an E.M.F. which is proportional to the current I and reactance x , and lags a quarter of a period, or 90° , behind the current. To overcome this counter E.M.F.

of self-induction, an E.M.F. of the value Ix is required, in phase 90° ahead of the current, hence represented by vector \overline{OE}_x . Thus resistance consumes E.M.F. in phase, and reactance an E.M.F. 90° ahead of the current. The E.M.F. of the generator, E_o , has to give the three E.M.F.s., E , E_r , and E_x , hence it is determined as their resultant. Combining by the parallelogram law, \overline{OE}_r and \overline{OE}_x , give \overline{OE}_z , the E.M.F. required to overcome the impedance of the line, and similarly \overline{OE}_z and \overline{OE} give \overline{OE}_o , the E.M.F. required at the generator side of the line, to yield the E.M.F. E at the receiving end of the line. Algebraically, we get from Fig. 12 —

$$E_o = \sqrt{(E + Ir)^2 + (Ix)^2};$$

or,

$$E = \sqrt{E_o^2 - (Ix)^2} - Ir.$$

In this instance we have considered the E.M.F. consumed by the resistance (in phase with the current) and the E.M.F. consumed by the reactance (90° ahead of the current) as parts, or components, of the impressed E.M.F., E_o , and have derived E_o by combining E_r , E_x , and E .

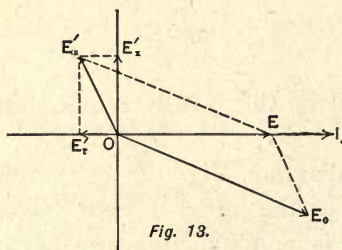


Fig. 13.

18. We may, however, introduce the effect of the inductance directly as an E.M.F., E_x' , the counter E.M.F. of self-induction = Ix , and lagging 90° behind the current; and the E.M.F. consumed by the resistance as a counter E.M.F., $E_r' = Ir$, but in opposition to the current, as is done in Fig. 13; and combine the three E.M.F.s. E_o , E_r' , E_x' , to form a resultant E.M.F., E , which is left at the end of the line.

E_r' and E_x' combine to form E_z' , the counter E.M.F. of impedance; and since E_z' and E_o must combine to form E , E_o is found as the side of a parallelogram, OE_oEE' , whose other side, $\overline{OE_z'}$, and diagonal, \overline{OE} , are given.

Or we may say (Fig. 14), that to overcome the counter E.M.F. of impedance, $\overline{OE_z'}$, of the line, the component, $\overline{OE_x}$, of the impressed E.M.F., together with the other component \overline{OE} , must give the impressed E.M.F., $\overline{OE_o}$.

As shown, we can represent the E.M.F.s. produced in a circuit in two ways — either as counter E.M.F.s., which combine with the impressed E.M.F., or as parts, or components,

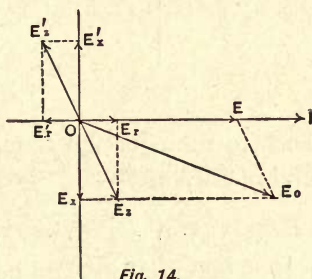


Fig. 14.

of the impressed E.M.F., in the latter case being of opposite phase. According to the nature of the problem, either the one or the other way may be preferable.

As an example, the E.M.F. consumed by the resistance is I_r , and in phase with the current; the counter E.M.F. of resistance is in opposition to the current. The E.M.F. consumed by the reactance is I_x , and 90° ahead of the current, while the counter E.M.F. of reactance is 90° behind the current; so that, if, in Fig. 15, \overline{OI} , is the current, —

$$\begin{aligned} \overline{OE_r} &= \text{E.M.F. consumed by resistance,} \\ \overline{OE_r'} &= \text{counter E.M.F. of resistance,} \\ \overline{OE_x} &= \text{E.M.F. consumed by inductance,} \\ \overline{OE_x'} &= \text{counter E.M.F. of inductance,} \\ \overline{OE_z} &= \text{E.M.F. consumed by impedance,} \\ \overline{OE_z'} &= \text{counter E.M.F. of impedance.} \end{aligned}$$

Obviously, these counter E.M.F.s. are different from, for instance, the counter E.M.F. of a synchronous motor, in so far as they have no independent existence, but exist only through, and as long as, the current flows. In this respect they are analogous to the opposing force of friction in mechanics.

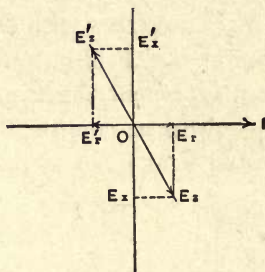


Fig. 15.

19. Coming back to the equation found for the E.M.F. at the generator end of the line,—

$$E_o = \sqrt{(E + Ir)^2 + (Ix)^2},$$

we find, as the drop of potential in the line —

$$\Delta E = E_o - E = \sqrt{(E + Ir)^2 + (Ix)^2} - E.$$

This is different from, and less than, the E.M.F. of impedance —

$$E_z = I_z = I\sqrt{r^2 + x^2}.$$

Hence it is wrong to calculate the drop of potential in a circuit by multiplying the current by the impedance; and the drop of potential in the line depends, with a given current fed over the line into a non-inductive circuit, not only upon the constants of the line, r and x , but also upon the E.M.F., E , at end of line, as can readily be seen from the diagrams.

20. If the receiver circuit is inductive, that is, if the current, I , lags behind the E.M.F., E , by an angle $\hat{\omega}$, and we choose again as the zero line, the current \overline{OI} (Fig. 16), the E.M.F., \overline{OE} is ahead of the current by angle $\hat{\omega}$. The

E.M.F. consumed by the resistance, Ir , is in phase with the current, and represented by \overline{OE}_r ; the E.M.F. consumed by the reactance, Ix , is 90° ahead of the current, and represented by \overline{OE}_x . Combining \overline{OE} , \overline{OE}_r , and \overline{OE}_x , we get \overline{OE}_o , the E.M.F. required at the generator end of the line. Comparing Fig. 16 with Fig. 13, we see that in the former \overline{OE}_o is larger; or conversely, if E_o is the same, E will be less with an inductive load. In other words, the drop of potential in an inductive line is greater, if the receiving circuit is inductive, than if it is non-inductive. From Fig. 16,—

$$E_o = \sqrt{(E \cos \hat{\omega} + Ir)^2 + (E \sin \hat{\omega} + Ix)^2}.$$

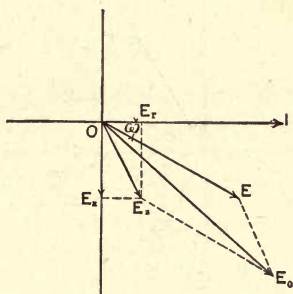


Fig. 16.

If, however, the current in the receiving circuit is leading, as is the case when feeding condensers or synchronous motors whose counter E.M.F. is larger than the impressed E.M.F., then the E.M.F. will be represented, in Fig. 17, by a vector, \overline{OE} , lagging behind the current, \overline{OI} , by the angle of lead $\hat{\omega}'$; and in this case we get, by combining \overline{OE} with \overline{OE}_r , in phase with the current, and \overline{OE}_x , 90° ahead of the current, the generator E.M.F., \overline{OE}_o , which in this case is not only less than in Fig. 16 and in Fig. 13, but may be even less than E ; that is, the potential rises in the line. In other words, in a circuit with leading current, the self-induction of the line raises the potential, so that the drop of potential is less than with

a non-inductive load, or may even be negative, and the voltage at the generator lower than at the other end of the line.

These same diagrams, Figs. 13 to 17, can be considered as polar diagrams of an alternating-current generator of an E.M.F., E_o , a resistance E.M.F., $E_r = Ir$, a reactance, $E_x = Ix$, and a difference of potential, E , at the alternator terminals; and we see, in this case, that with an inductive load the potential difference at the alternator terminals will be lower than with a non-inductive load, and that with a non-inductive load it will be lower than when feeding into

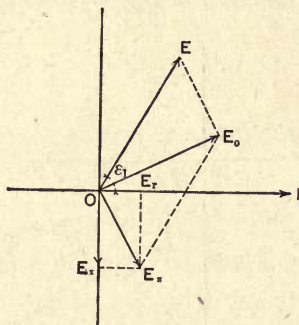


Fig. 17.

a circuit with leading current, as, for instance, a synchronous motor circuit under the circumstances stated above.

21. As a further example, we may consider the diagram of an alternating-current transformer, feeding through its secondary circuit an inductive load.

For simplicity, we may neglect here the magnetic hysteresis, the effect of which will be fully treated in a separate chapter on this subject.

Let the time be counted from the moment when the magnetic flux is zero. The phase of the flux, that is, the amplitude of its maximum value, is 90° in this case, and, consequently, the phase of the induced E.M.F., is 180° ,

since the induced E.M.F. lags 90° behind the inducing flux. Thus the secondary induced E.M.F., E_1 , will be represented by a vector, $\overline{OE_1}$, in Fig. 18, at the phase 180° . The secondary current, I_1 , lags behind the E.M.F. E_1 by an angle $\hat{\omega}_1$, which is determined by the resistance and inductance of the secondary circuit; that is, by the load in the secondary circuit, and is represented in the diagram by the vector OF_1 , of phase $180 + \hat{\omega}$.

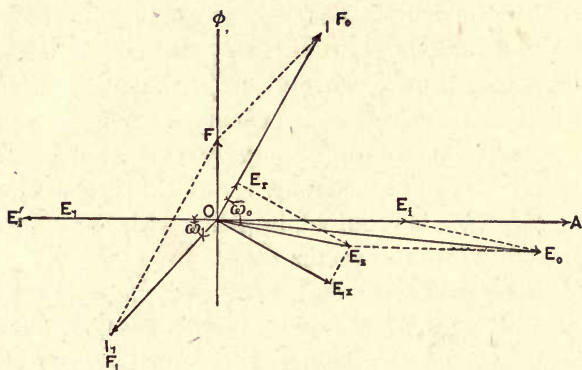


Fig. 18.

Instead of the secondary current, I_1 , we plot, however, the secondary M.M.F., $F_1 = n_1 I_1$, where n_1 is the number of secondary turns, and F_1 is given in ampere-turns. This makes us independent of the ratio of transformation.

From the secondary induced E.M.F., E_1 , we get the flux, Φ , required to induce this E.M.F., from the equation —

$$\text{where —} \quad E_1 = \sqrt{2} \pi n_1 N \Phi 10^{-8}.$$

E_1 = secondary induced E.M.F., in effective volts,

N = frequency, in cycles per second.

n_1 = number of secondary turns.

Φ = maximum value of magnetic flux, in webers.

The derivation of this equation has been given in a preceding chapter.

This magnetic flux, Φ , is represented by a vector, $\overline{O\Phi}$, at

the phase 90° , and to induce it an M.M.F., \mathfrak{F} , is required, which is determined by the magnetic characteristic of the iron, and the section and length of the magnetic circuit of the transformer; it is in phase with the flux Φ , and represented by the vector \overline{OF} , in effective ampere-turns.

The effect of hysteresis, neglected at present, is to shift \overline{OF} ahead of \overline{OM} , by an angle α , the angle of hysteretic lead. (See Chapter on Hysteresis.)

This M.M.F., \mathfrak{F} , is the resultant of the secondary M.M.F., \mathfrak{F}_1 , and the primary M.M.F., \mathfrak{F}_o ; or graphically, \overline{OF} is the diagonal of a parallelogram with \overline{OF}_1 and \overline{OF}_o as sides. \overline{OF}_1 and \overline{OF} being known, we find \overline{OF}_o , the primary ampere-turns, n_o , and therefrom, the primary current, $I_o = \mathfrak{F}_o / n_o$, which corresponds to the secondary current, I_1 .

To overcome the resistance, r_o , of the primary coil, an E.M.F., $E_r = I_r r_o$, is required, in phase with the current, I_o , and represented by the vector \overline{OE}_r .

To overcome the reactance, $x_o = 2\pi n_o L_o$, of the primary coil, an E.M.F. $E_x = I_o x_o$ is required, 90° ahead of the current I_o , and represented by vector, \overline{OE}_x .

The resultant magnetic flux, Φ , which in the secondary coil induces the E.M.F., E_1 , induces in the primary coil an E.M.F. proportional to E_1 by the ratio of turns n_o / n_1 , and in phase with E_1 , or, —

$$E_i' = \frac{n_o}{n_1} E_1,$$

which is represented by the vector \overline{OE}_i' . To overcome this counter E.M.F., E_i' , a primary E.M.F., E_i , is required, equal but opposite to E_i' , and represented by the vector, \overline{OE}_i .

The primary impressed E.M.F., E_o , must thus consist of the three components, \overline{OE}_i , \overline{OE}_r , and \overline{OE}_x , and is, therefore, a resultant \overline{OE}_o , while the difference of phase in the primary circuit is found to be $\sphericalangle \hat{\omega}_o = E_o OA$.

22. Thus, in Figs. 18, 19, and 20, the diagram of an alternating-current transformer is drawn for the same sec-

ondary E.M.F., E_1 , and secondary current, I_1 , but with different conditions of secondary displacement:—

In Fig. 18, the secondary current, I_1 , lags 60° behind the secondary E.M.F., E_1 .

In Fig. 19, the secondary current, I_1 , is in phase with the secondary E.M.F., E_1 .

In Fig. 20, the secondary current, I_1 , leads by 60° the secondary E.M.F., E_1 .

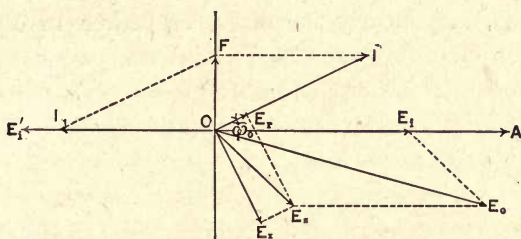


Fig. 19.

These diagrams show that lag in the secondary circuit increases and lead decreases, the primary current and primary E.M.F. required to produce in the secondary circuit the same E.M.F. and current; or conversely, at a given primary

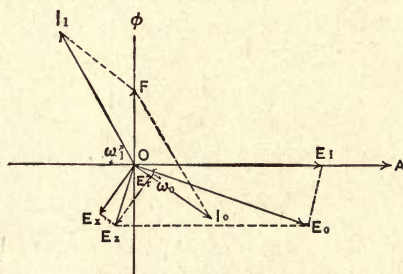


Fig. 20.

impressed E.M.F., E_0 , the secondary E.M.F., E_1 , will be smaller with an inductive, and larger with a condenser (leading current) load, than with a non-inductive load.

At the same time we see that a difference of phase existing in the secondary circuit of a transformer reappears

in the primary circuit, somewhat decreased if leading, and slightly increased if lagging. Later we shall see that hysteresis reduces the displacement in the primary circuit, so that, with an excessive lag in the secondary circuit, the lag in the primary circuit may be less than in the secondary.

A conclusion from the foregoing is that the transformer is not suitable for producing currents of displaced phase; since primary and secondary current are, except at very light loads, very nearly in phase, or rather, in opposition, to each other.

CHAPTER V.

SYMBOLIC METHOD.

23. The graphical method of representing alternating-current phenomena by polar coördinates of time affords the best means for deriving a clear insight into the mutual relation of the different alternating sine waves entering into the problem. For numerical calculation, however, the graphical method is frequently not well suited, owing to the widely different magnitudes of the alternating sine waves represented in the same diagram, which make an exact diagrammatic determination impossible. For instance, in the transformer diagrams (*cf.* Figs. 18-20), the different magnitudes will have numerical values in practice, somewhat like $E_1 = 100$ volts, and $I_1 = 75$ amperes, for a non-inductive secondary load, as of incandescent lamps. Thus the only reactance of the secondary circuit is that of the secondary coil, or, $x_1 = .08$ ohms, giving a lag of $\hat{\omega}_1 = 3.6^\circ$. We have also,

$$\begin{aligned} n_1 &= 30 \text{ turns.} \\ n_o &= 300 \text{ turns.} \\ \mathfrak{F}_1 &= 2250 \text{ ampere-turns.} \\ \mathfrak{F} &= 100 \text{ ampere-turns.} \\ E_r &= 10 \text{ volts.} \\ E_x &= 60 \text{ volts.} \\ E_i &= 1000 \text{ volts.} \end{aligned}$$

The corresponding diagram is shown in Fig. 21. Obviously, no exact numerical values can be taken from a parallelogram as flat as OF_1FF_o , and from the combination of vectors of the relative magnitudes 1:6:100.

Hence the importance of the graphical method consists

not so much in its usefulness for practical calculation, as to aid in the simple understanding of the phenomena involved.

24. Sometimes we can calculate the numerical values trigonometrically by means of the diagram. Usually, however, this becomes too complicated, as will be seen by trying

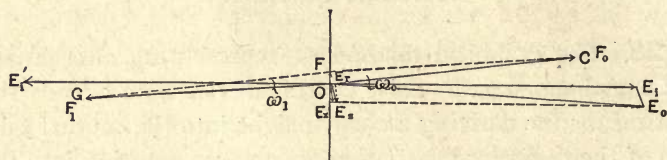


Fig. 21.

to calculate, from the above transformer diagram, the ratio of transformation. The primary M.M.F. is given by the equation:—

$$\mathcal{F}_o = \sqrt{\mathcal{F}^2 + \mathcal{F}_1^2 + 2\mathcal{F}\mathcal{F}_1 \sin \omega_1},$$

an expression not well suited as a starting-point for further calculation.

A method is therefore desirable which combines the exactness of analytical calculation with the clearness of the graphical representation.

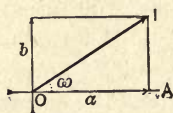


Fig. 22.

25. We have seen that the alternating sine wave is represented in intensity, as well as phase, by a vector, \overline{OI} , which is determined analytically by two numerical quantities — the length, \overline{OI} , or intensity; and the amplitude, AOI , or phase $\hat{\omega}$, of the wave, I .

Instead of denoting the vector which represents the sine wave in the polar diagram by the polar coördinates,

I and $\hat{\omega}$, we can represent it by its rectangular coördinates, a and b (Fig. 22), where —

$a = I \cos \hat{\omega}$ is the horizontal component,

$b = I \sin \hat{\omega}$ is the vertical component of the sine wave.

This representation of the sine wave by its rectangular components is very convenient, in so far as it avoids the use of trigonometric functions in the combination or resolution of sine waves.

Since the rectangular components a and b are the horizontal and the vertical projections of the vector representing the sine wave, and the projection of the diagonal of a parallelogram is equal to the sum of the projections of its sides, the combination of sine waves by the parallelogram

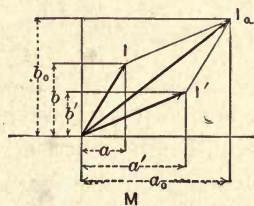


Fig. 23.

law is reduced to the addition, or subtraction, of their rectangular components. That is,

Sine waves are combined, or resolved, by adding, or subtracting, their rectangular components.

For instance, if a and b are the rectangular components of a sine wave, I , and a' and b' the components of another sine wave, I' (Fig. 23), their resultant sine wave, I_o , has the rectangular components $a_o = (a + a')$, and $b_o = (b + b')$.

To get from the rectangular components, a and b , of a sine wave, its total intensity, i , and phase, $\hat{\omega}$, we may combine a and b by the parallelogram, and derive, —

$$i = \sqrt{a^2 + b^2};$$

$$\tan \hat{\omega} = \frac{b}{a}.$$

Hence we can analytically operate with sine waves, as with forces in mechanics, by resolving them into their rectangular components.

26. To distinguish, however, the horizontal and the vertical components of sine waves, so as not to be confused in lengthier calculation, we may mark, for instance, the vertical components, by a distinguishing index, or the addition of an otherwise meaningless symbol, as the letter j , and thus represent the sine wave by the expression, —

$$I = a + jb,$$

which now has the meaning, that a is the horizontal and b the vertical component of the sine wave I ; and that both components are to be combined in the resultant wave of intensity, —

$$i = \sqrt{a^2 + b^2},$$

and of phase, $\tan \hat{\omega} = b/a$.

Similarly, $a - jb$, means a sine wave with a as horizontal, and $-b$ as vertical, components, etc.

Obviously, the plus sign in the symbol, $a + jb$, does not imply simple addition, since it connects heterogeneous quantities — horizontal and vertical components — but implies combination by the parallelogram law.

For the present, j is nothing but a distinguishing index, and otherwise free for definition except that it is not an ordinary number.

27. A wave of equal intensity, and differing in phase from the wave $a + jb$ by 180° , or one-half period, is represented in polar coördinates by a vector of opposite direction, and denoted by the symbolic expression, $-a - jb$. Or —

Multiplying the algebraic expression, $a + jb$, of a sine wave by -1 means reversing the wave, or rotating it through 180° , or one-half period.

A wave of equal intensity, but lagging 90° , or one-quarter period, behind $a + jb$, has (Fig. 24) the horizontal

component, $-b$, and the vertical component, a , and is represented algebraically by the expression, $ja - b$.

Multiplying, however, $a + jb$ by j , we get:—

$$ja + j^2 b;$$

therefore, if we define the heretofore meaningless symbol, j , by the condition, —

$$j^2 = -1,$$

we have —

$$j(a + jb) = ja - b;$$

hence:—

Multiplying the algebraic expression, $a + jb$, of a sine wave by j means rotating the wave through 90° , or one-quarter period; that is, retarding the wave through one-quarter period.

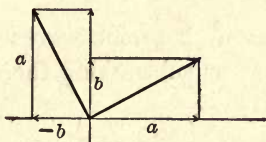


Fig. 24.

Similarly, —

Multiplying by $-j$ means advancing the wave through one-quarter period.

since $j^2 = -1$, $j = \sqrt{-1}$;
that is, —

j is the imaginary unit, and the sine wave is represented by a complex imaginary quantity, $a + jb$.

As the imaginary unit j has no numerical meaning in the system of ordinary numbers, this definition of $j = \sqrt{-1}$ does not contradict its original introduction as a distinguishing index. For a more exact definition of this complex imaginary quantity, reference may be made to the text books of mathematics.

28. In the polar diagram of time, the sine wave is represented in intensity as well as phase by one complex quantity —

$$a + jb,$$

where a is the horizontal and b the vertical component of the wave ; the intensity is given by —

$$i = \sqrt{a^2 + b^2},$$

the phase by —

$$\tan \hat{\omega} = \frac{b}{a},$$

and

$$a = i \cos \hat{\omega},$$

$$b = i \sin \hat{\omega};$$

hence the wave $a + jb$ can also be expressed by —

$$i (\cos \hat{\omega} + j \sin \hat{\omega}),$$

or, by substituting for $\cos \omega$ and $\sin \hat{\omega}$ their exponential expressions, we obtain —

$$ie^{j\hat{\omega}}.$$

Since we have seen that sine waves may be combined or resolved by adding or subtracting their rectangular components, consequently : —

Sine waves may be combined or resolved by adding or subtracting their complex algebraic expressions.

For instance, the sine waves, —

$$a + jb$$

and

$$a' + jb',$$

combined give the sine wave —

$$I = (a + a') + j(b + b').$$

It will thus be seen that the combination of sine waves is reduced to the elementary algebra of complex quantities.

29. If $I = i + ji'$ is a sine wave of alternating current, and r is the resistance, the E.M.F. consumed by the resistance is in phase with the current, and equal to the product of the current and resistance. Or —

$$rI = ri + jri'.$$

If L is the inductance, and $x = 2\pi NL$ the reactance, the E.M.F. produced by the reactance, or the counter

E.M.F. of self-inductance, is the product of the current and reactance, and lags 90° behind the current; it is, therefore, represented by the expression —

$$jxI = jxi - xi'.$$

The E.M.F. required to overcome the reactance is consequently 90° ahead of the current (or, as usually expressed, the current lags 90° behind the E.M.F.), and represented by the expression —

$$-jxI = -jxi + xi'.$$

Hence, the E.M.F. required to overcome the resistance, r , and the reactance, x , is —

$$(r - jx) I;$$

that is —

Z = r - jx is the expression of the impedance of the circuit, in complex quantities.

Hence, if $I = i + ji'$ is the current, the E.M.F. required to overcome the impedance, $Z = r - jx$, is —

$$E = ZI = (r - jx)(i + ji');$$

hence, since $j^2 = -1$

$$E = (ri + xi') + j(ri' - xi');$$

or, if $E = e + je'$ is the impressed E.M.F., and $Z = r - jx$ the impedance, the current flowing through the circuit is: —

$$I = \frac{E}{Z} = \frac{e + je'}{r - jx};$$

or, multiplying numerator and denominator by $(r + jx)$ to eliminate the imaginary from the denominator, we have —

$$I = \frac{(e + je')(r + jx)}{r^2 + x^2} = \frac{er - \ell x}{r^2 + x^2} + j \frac{\ell r + ex}{r^2 + x^2};$$

or, if $E = e + je'$ is the impressed E.M.F., and $I = i + ji'$ the current flowing in the circuit, its impedance is —

$$Z = \frac{E}{I} = \frac{e + je'}{i + ji'} = \frac{(e + je')(i - ji')}{i^2 + i'^2} = \frac{ei + \ell i'}{i^2 + i'^2} + j \frac{\ell i' - ei'}{i^2 + i'^2}.$$

30. If C is the capacity of a condenser in series in a circuit of current $I = i + ji'$, the E.M.F. impressed upon the terminals of the condenser is $E = \frac{I}{2\pi NC}$, 90° behind the current; and may be represented by $\frac{jI}{2\pi NC}$, or $jx_1 I$, where $x_1 = \frac{1}{2\pi NC}$ is the *capacity reactance* or *condensance* of the condenser.

Capacity reactance is of opposite sign to magnetic reactance; both may be combined in the name reactance.

We therefore have the conclusion that

If $r =$ resistance and $L =$ inductance,
then $x = 2\pi NL =$ magnetic reactance.

If $C =$ capacity, $x_1 = \frac{1}{2\pi NC} =$ capacity reactance, or condensance;

$Z = r - j(x - x_1)$, is the impedance of the circuit.

Ohm's law is then reestablished as follows:

$$E = ZI, \quad I = \frac{E}{Z}, \quad Z = \frac{E}{I}.$$

The more general form gives not only the intensity of the wave, but also its phase, as expressed in complex quantities.

31. Since the combination of sine waves takes place by the addition of their symbolic expressions, Kirchhoff's laws are now reestablished in their original form:—

a.) The sum of all the E.M.Fs. acting in a closed circuit equals zero, if they are expressed by complex quantities, and if the resistance and reactance E.M.Fs. are also considered as counter E.M.Fs.

b.) The sum of all the currents flowing towards a distributing point is zero, if the currents are expressed as complex quantities.

Since, if a complex quantity equals zero, the real part as well as the imaginary part must be zero individually, if

$$a + jb = 0, \quad a = 0, b = 0,$$

and if both the E.M.Fs. and currents are resolved, we find:—

a.) The sum of the components, in any direction, of all the E.M.Fs. in a closed circuit, equals zero, if the resistance and reactance are considered as counter E.M.Fs.

b.) The sum of the components, in any direction, of all the currents flowing towards a distributing point, equals zero.

Joule's Law and the energy equation do not give a simple expression in complex quantities, since the effect or power is a quantity of double the frequency of the current or E.M.F. wave, and therefore cannot be represented as a vector in the diagram.

In what follows, complex quantities will always be denoted by capitals, absolute quantities and real quantities by small letters.

32. Referring to the instance given in the fourth chapter, of a circuit supplied with an E.M.F., E , and a current, I , over an inductive line, we can now represent the impedance of the line by $Z = r - jx$, where r = resistance, x = reactance of the line, and have thus as the E.M.F. at the beginning of the line, or at the generator, the expression —

$$E_o = E + ZI.$$

Assuming now again the current as the zero line, that is, $I = i$, we have in general —

$$E_o = E + ir - jix;$$

hence, with non-inductive load, or $E = e$,

$$E_o = (e + ir) - jix,$$

$$e_o = \sqrt{(e + ir)^2 + (ix)^2}, \quad \tan \hat{\omega}_o = \frac{ix}{e + ir}.$$

In a circuit with lagging current, that is, with leading E.M.F., $E = e - je'$, and

$$\begin{aligned} E_o &= e - je' + (r - jx) i \\ &= (e + ir) - j(\ell' + ix), \end{aligned}$$

or
$$e_o = \sqrt{(e + ir)^2 + (\ell' + ix)^2}, \quad \tan \hat{\omega}_o = \frac{\ell' + ix}{e + ir}.$$

In a circuit with leading current, that is, with lagging E.M.F., $E = e + je'$, and

$$\begin{aligned} E_o &= (e + j\ell') + (r - jx) i \\ &= (e + ir) + j(\ell' - ix), \end{aligned}$$

$$e_o = \sqrt{(e + ir)^2 + (\ell' - ix)^2}, \quad \tan \hat{\omega}_o = \frac{\ell' - ix}{e + ir};$$

values which easily permit calculation.

CHAPTER VI.

TOPOGRAPHIC METHOD.

33. In the representation of alternating sine waves by vectors in a polar diagram, a certain ambiguity exists, in so far as one and the same quantity — an E.M.F., for instance — can be represented by two vectors of opposite direction, according as to whether the E.M.F. is considered as a part of the impressed E.M.F., or as a counter E.M.F. This is analogous to the distinction between action and reaction in mechanics.

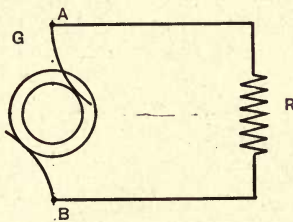


Fig. 25.

Further, it is obvious that if in the circuit of a generator, G (Fig. 25), the current flowing from terminal A over resistance R to terminal B , is represented by a vector \overline{OI} (Fig. 26), or by $I = i + ji'$, the same current can be considered as flowing in the opposite direction, from terminal B to terminal A in opposite phase, and therefore represented by a vector \overline{OI}_1 (Fig. 26), or by $I_1 = -i - ji'$.

Or, if the difference of potential from terminal B to terminal A is denoted by the $E = e + je'$, the difference of potential from A to B is $E_1 = -e - je'$.

Hence, in dealing with alternating-current sine waves, it is necessary to consider them in their proper direction with regard to the circuit. Especially in more complicated circuits, as interlinked polyphase systems, careful attention has to be paid to this point.

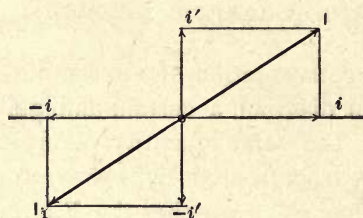


Fig. 26.

34. Let, for instance, in Fig. 27, an interlinked three-phase system be represented diagrammatically, and consisting of three E.M.Fs., of equal intensity, differing in phase by one-third of a period. Let the E.M.Fs. in the direction

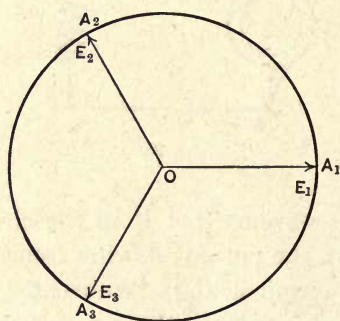


Fig. 27.

from the common connection O of the three branch circuits to the terminals A_1, A_2, A_3 , be represented by E_1, E_2, E_3 . Then the difference of potential from A_2 to A_1 is $E_2 - E_1$, since the two E.M.Fs., E_1 and E_2 , are connected in circuit between the terminals A_1 and A_2 , in the direction,

$A_1 - O - A_2$; that is, the one, E_2 , in the direction OA_2 , from the common connection to terminal, the other, E_1 , in the opposite direction, A_1O , from the terminal to common connection, and represented by $-E_1$. Conversely, the difference of potential from A_1 to A_2 is $E_1 - E_2$.

It is then convenient to go still a step farther, and drop, in the diagrammatic representation, the vector line altogether; that is, denote the sine wave by a point only, the end of the corresponding vector.

Looking at this from a different point of view, it means that we choose one point of the system—for instance, the common connection O —as a zero point, or point of zero potential, and represent the potentials of all the other points of the circuit by points in the diagram, such that their distances from the zero point gives the intensity; their amplitude the phase of the difference of potential of the respective point with regard to the zero point; and their distance and amplitude with regard to other points of the diagram, their difference of potential from these points in intensity and phase.

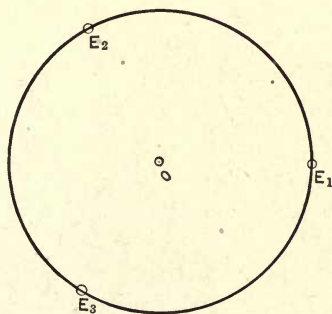


Fig. 28.

Thus, for example, in an interlinked three-phase system with three E.M.F.s. of equal intensity, and differing in phase by one-third of a period, we may choose the common connection of the star-connected generator as the zero point, and represent, in Fig. 28, one of the E.M.F.s., or the poten-

tial at one of the three-phase terminals, by point E_1 . The potentials at the two other terminals will then be given by the points E_2 and E_3 , which have the same distance from O as E_1 , and are equidistant from E_1 and from each other.

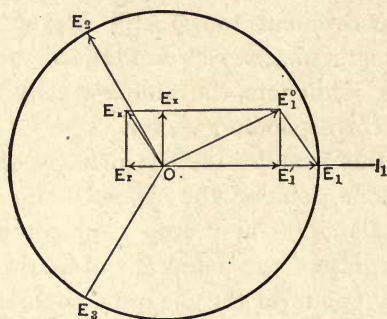


Fig. 29.

The difference of potential between any pair of terminals—for instance E_1 and E_2 —is then the distance $\overline{E_2E_1}$, or $\overline{E_1E_2}$, according to the direction considered.

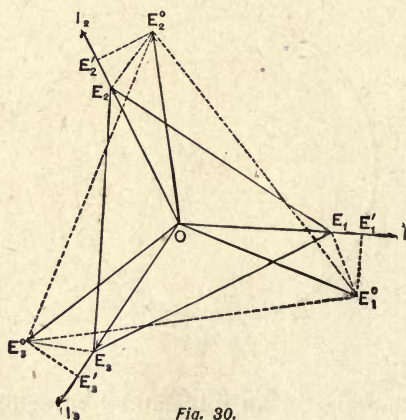


Fig. 30.

35. If, now, in Fig. 29, a current, I_1 , in phase with E.M.F., E_1 , passes through a circuit, the counter E.M.F. of resistance, r , is $E_r = I_1 r$, in opposition to I_1 or E_1 ,

and hence represented in the diagram by point E_r , and its combination with E_1 by E_1' . The counter E.M.F. of reactance, x , is $E_x = Ix$, 90° behind the current I_1 , or E.M.F., E_1 , and therefore represented by point E_x , and giving, by its combination with E_1' , the terminal potential of the generator E_1^o , which, as seen, is less than the E.M.F., E_1 .

If all the three branches are loaded equally by three currents flowing into a non-inductive circuit, and thus in

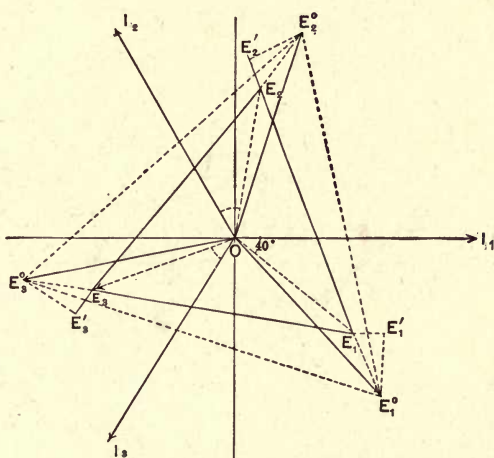


Fig. 31.

phase with the E.M.F.s. at the generator terminals (represented in the diagram, Fig. 30, by the points E_1, E_2, E_3 , equidistant from each other, and equidistant from the zero point, O), the counter E.M.F.s. of resistance, I_r , are represented by the distances EE' , as E_1E_1' , etc., in phase with the currents, I ; and the counter E.M.F.s. of reactance, I_x , are represented by the distance, $E'E^o$ in quadrature with the current, thereby giving, at the generator E.M.F.s., the points E_1^o, E_2^o, E_3^o .

Thus, the triangle of generator E.M.F.s. $E_1^oE_2^oE_3^o$, produces, with equal load on the three branches and non-

inductive circuit, the equilateral triangle, $E_1E_2E_3$, of terminal potentials.

If the load is inductive, and the currents, I , lag behind the terminal voltages, E , by, say, 40° , we get the diagram shown in Fig. 31, which explains itself, and shows that the drop of potential in the generator is larger on an inductive load than on a non-inductive load.

Conversely, if the currents lead the terminal E.M.F.s. by, say, 40° , as shown in Fig. 32, the drop of potential in the generator is less, or a rise may even take place.

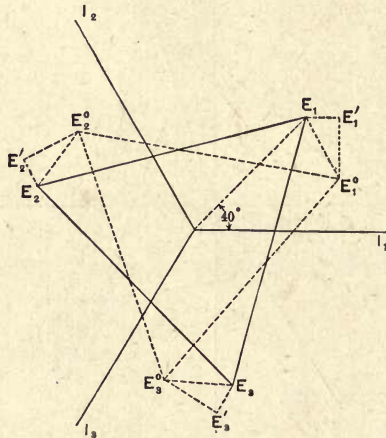


Fig. 32.

36. If, however, only one branch of the three-phase circuit is loaded, as, for instance, $E_1^\circ E_2^\circ$, the E.M.F. producing the current (Fig. 33), is $\overline{E_1E_2}$; and, if the current lags 20° , it has the direction \overline{OI} , where \overline{OI} forms with $\overline{E_1E_2}$ the angle $\omega - 20^\circ$; that is, the current in E_1 is $\overline{OI_1}$, and the current in E_2 is $\overline{OI_2}$, the return current of $\overline{OI_1}$.

Hence the potential at the first terminal is E_1 , as derived by combining with E_1° the resistance E.M.F., $\overline{E_1^\circ E_1'}$, in phase, and the reactance, E.M.F., $\overline{E_1' E_1}$, in quadrature, with the current; and in the same way, the E.M.F. at the

second terminal is E_2 , derived by the combination of E_2^o with $E_2^o E_2'$ in phase, and $E_2' E_2$ in quadrature, with the current.

Hence the three terminal potentials are now, E_1 , E_2 , E_3^o , and the differences of potential between the terminals of the generators are the sides of the triangle, $E_1 E_2 E_3^o$; or, in other words, the equilateral triangle of E.M.F., $E_1^o E_2^o E_3^o$, produces at the generator terminals the triangle of voltages, $E_1 E_2 E_3^o$, whose three sides are unequal; one, $E_1 E_2$, or the loaded branch, being less than $E_1^o E_2^o$, or the two unloaded branches. That is, the one has decreased, the other has increased, and the system has become unbalanced.

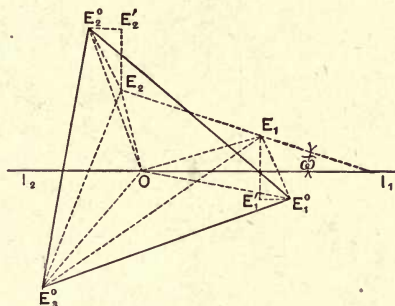


Fig. 33.

In the same manner, if two branches, $E_1^o E_2^o$, and $E_2^o E_3^o$, are loaded, and the third, $E_1^o E_3^o$, is unloaded, and the currents lag 20° , we find the current I_3 in E_1^o to be 20° behind $E_1^o E_2^o$, the current I_1 in E_3^o 20° behind $E_2^o E_3^o$, and the current I_2 in E_2^o , the common return of I_1 and I_3 ; by combining again the generator E.M.F.s., E^o , with the resistance E.M.F.s., $E^o E'$, in phase, and the reactance E.M.F.s., $E' E$, in quadrature, with the respective currents, we get the terminal potentials, E . We thus see that the E.M.F. triangle, $E_1^o E_2^o E_3^o$, is, by loading two branches, changed to an unbalanced triangle of terminal voltages, $E_1 E_2 E_3$, as shown in Fig. 34.

If all the three branches of the three-phase system are loaded equally, we see, from Fig. 31, that the system remains balanced.

37. As another instance, we may consider the unbalancing of a two-phase system with a common return.

If, in a two-phase system, we choose the potential of the common return at the generator terminal as zero, the potentials of the two outside terminals of the generator are repre-

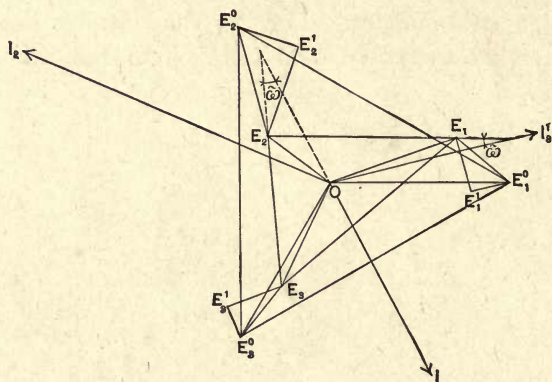


Fig. 34.

sented by E_1^0 and E_2^0 , at right angles to each other, and equidistant from O , as shown in Fig. 35.

Let, now, both branches be loaded equally by currents lagging 40° . Then, the currents in E_1^0 and E_2^0 are represented by I_1 and I_2 , and their common return current by I_3 . If, now, these currents are sent over lines containing resistance and reactance, we get the potentials at the end of the line by combining the generator potentials E_1^0 , E_2^0 and O , with the resistance E.M.F.s., $E_1^0E_1'$, $E_2^0E_2'$ and OE_3' , in phase with the currents, and with the reactance E.M.F.s., $E_1'E_1$, $E_2'E_2$, $E_3'E_3$, in quadrature with the currents; and thereby derive as the potentials at the end of the line the points E_1 , E_2 , E_3 , which form neither an isosceles

nor a rectangular triangle. That is, the two-phase system with a common return becomes, even at equal distribution of load, unbalanced in intensity and in phase.

These instances will be sufficient to explain the general method of topographic representation of alternating sine waves.

It is obvious now, since the potential of every point of

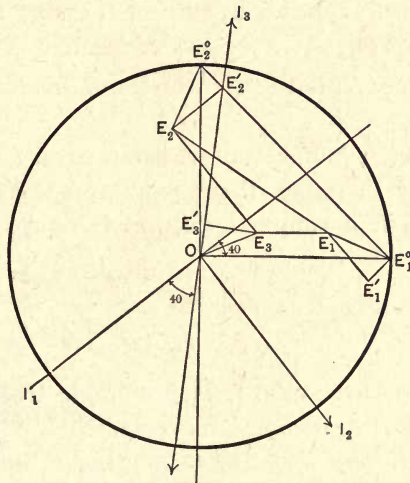


Fig. 35.

the circuit is represented by a point in the topographic diagram, that the whole circuit will be represented by a closed figure, which may be called the topographic circuit characteristic.

Such a characteristic is, for instance, $OE_1^{\circ}E_1'E_1E_2E_2'E_2^{\circ}$, in Figs. 31 to 34, etc.; further instances are shown in the following chapters, as curved characteristics in the chapter on distributed capacity, etc.

CHAPTER VII.

ADMITTANCE, CONDUCTANCE, SUSCEPTANCE.

38. If in a continuous-current circuit, a number of resistances, r_1, r_2, r_3, \dots are connected in series, their joint resistance, R , is the sum of the individual resistances $R = r_1 + r_2 + r_3 + \dots$

If, however, a number of resistances are connected in multiple or in parallel, their joint resistance, R , cannot be expressed in a simple form, but is represented by the expression:—

$$R = \frac{1}{\frac{1}{r_1} + \frac{1}{r_2} + \frac{1}{r_3} + \dots}$$

Hence, in the latter case it is preferable to introduce, instead of the term *resistance*, its reciprocal, or inverse value, the term *conductance*, $g = 1/r$. If, then, a number of conductances, g_1, g_2, g_3, \dots are connected in parallel, their joint conductance is the sum of the individual conductances, or $G = g_1 + g_2 + g_3 + \dots$. When using the term conductance, the joint conductance of a number of series-connected conductances becomes similarly a complicated expression—

$$G = \frac{1}{\frac{1}{g_1} + \frac{1}{g_2} + \frac{1}{g_3} + \dots}$$

Hence the term *resistance* is preferable in case of series connection, and the use of the reciprocal term *conductance* in parallel connections; therefore,

The joint resistance of a number of series-connected resistances is equal to the sum of the individual resistances; the

joint conductance of a number of parallel-connected conductances is equal to the sum of the individual conductances.

39. In alternating-current circuits, instead of the term *resistance* we have the term *impedance*, $Z = r - jx$, with its two components, the *resistance*, r , and the *reactance*, x , in the formula of Ohm's law, $E = IZ$. The resistance, r , gives the component of E.M.F. in phase with the current, or the energy component of the E.M.F., Ir ; the reactance, x , gives the component of the E.M.F. in quadrature with the current, or the wattless component of E.M.F., Ix ; both combined give the total E.M.F., —

$$Iz = I\sqrt{r^2 + x^2}.$$

Since E.M.Fs. are combined by adding their complex expressions, we have :

The joint impedance of a number of series-connected impedances is the sum of the individual impedances, when expressed in complex quantities.

In graphical representation impedances have not to be added, but are combined in their proper phase by the law of parallelogram in the same manner as the E.M.Fs. corresponding to them. The term impedance becomes inconvenient, however, when dealing with parallel-connected circuits; or, in other words, when several currents are produced by the same E.M.F., such as in cases where Ohm's law is expressed in the form,

$$I = \frac{E}{Z}.$$

It is preferable, then, to introduce the reciprocal of impedance, which may be called the *admittance* of the circuit, or

$$Y = \frac{1}{Z}.$$

As the reciprocal of the complex quantity, $Z = r - jx$, the admittance is a complex quantity also, or

$$Y = g + jb;$$

it consists of the component g , which represents the coefficient of current in phase with the E.M.F., or energy current, gE , in the equation of Ohm's law, —

$$I = YE = (g + jb) E,$$

and the component b , which represents the coefficient of current in quadrature with the E.M.F., or wattless component of current, bE .

g may be called the *conductance*, and b the *susceptance*, of the circuit. Hence the conductance, g , is the energy component, and the susceptance, b , the wattless component, of the admittance, $Y = g + jb$, while the numerical value of admittance is —

$$y = \sqrt{g^2 + b^2};$$

the resistance, r , is the energy component, and the reactance, x , the wattless component, of the impedance, $Z = r - jx$, the numerical value of impedance being —

$$z = \sqrt{r^2 + x^2}.$$

40. As shown, the term *admittance* implies resolving the current into two components, in phase and in quadrature with the E.M.F., or the energy current and the wattless current; while the term *impedance* implies resolving the E.M.F. into two components, in phase and in quadrature with the current, or the energy E.M.F. and the wattless E.M.F.

It must be understood, however, that the conductance is not the reciprocal of the resistance, but depends upon the resistance as well as upon the reactance. Only when the reactance $x = 0$, or in continuous-current circuits, is the conductance the reciprocal of resistance.

Again, only in circuits with zero resistance ($r = 0$) is the susceptance the reciprocal of reactance; otherwise, the susceptance depends upon reactance and upon resistance.

The conductance is zero for two values of the resistance:—

1.) If $r = \infty$, or $x = \infty$, since in this case no current passes, and either component of the current = 0.

2.) If $r = 0$, since in this case the current which passes through the circuit is in quadrature with the E.M.F., and thus has no energy component.

Similarly, the susceptance, b , is zero for two values of the reactance:—

1.) If $x = \infty$, or $r = \infty$.

2.) If $x = 0$.

From the definition of admittance, $Y = g + jb$, as the reciprocal of the impedance, $Z = r - jx$,

we have
$$Y = \frac{1}{Z}, \text{ or, } g + jb = \frac{1}{r - jx};$$

or, multiplying numerator and denominator on the right side by $(r + jx)$

$$g + jb = \frac{r + jx}{(r - jx)(r + jx)};$$

hence, since

$$(r - jx)(r + jx) = r^2 + x^2 = z^2,$$

$$g + jb = \frac{r}{r^2 + x^2} + j \frac{x}{r^2 + x^2} = \frac{r}{z^2} + j \frac{x}{z^2};$$

or

$$g = \frac{r}{r^2 + x^2} = \frac{r}{z^2},$$

$$b = \frac{x}{r^2 + x^2} = \frac{x}{z^2};$$

and conversely

$$r = \frac{g}{g^2 + b^2} = \frac{g}{y^2},$$

$$x = \frac{b}{g^2 + b^2} = \frac{b}{y^2}.$$

By these equations, the conductance and susceptance can be calculated from resistance and reactance, and conversely.

Multiplying the equations for g and r , we get:—

$$gr = \frac{rg}{z^2 y^2};$$

hence,

$$z^2 y^2 = (r^2 + x^2)(g^2 + b^2) = 1;$$

and,

$$z = \frac{1}{y} = \frac{1}{\sqrt{g^2 + b^2}}, \quad \left\{ \begin{array}{l} \text{the absolute value of} \\ \text{impedance;} \end{array} \right.$$

$$y = \frac{1}{z} = \frac{1}{\sqrt{r^2 + x^2}}, \quad \left\{ \begin{array}{l} \text{the absolute value of} \\ \text{admittance.} \end{array} \right.$$

41. If, in a circuit, the reactance, x , is constant, and the resistance, r , is varied from $r = 0$ to $r = \infty$, the susceptance, b , decreases from $b = 1/x$ at $r = 0$, to $b = 0$ at $r = \infty$; while the conductance, $g = 0$ at $r = 0$, increases, reaches a maximum for $r = x$, where $g = 1/2r$ is equal to the susceptance, or $g = b$, and then decreases again, reaching $g = 0$ at $r = \infty$.

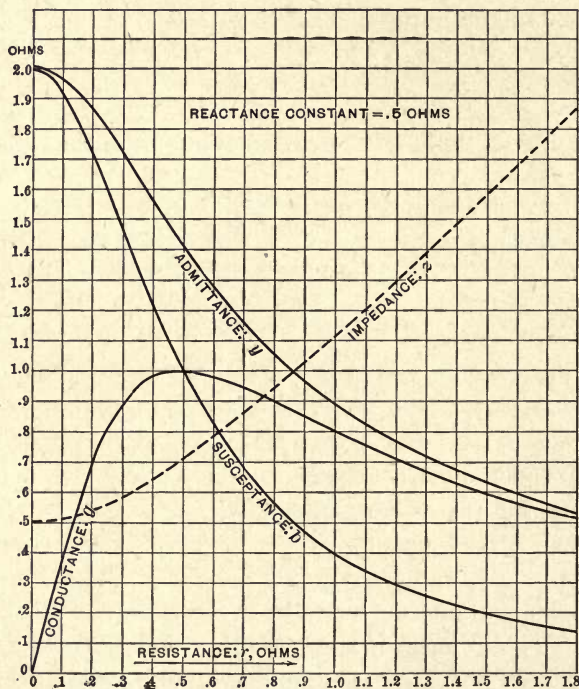


Fig. 36.

In Fig. 36, for constant reactance $x = .5$ ohm, the variation of the conductance, g , and of the susceptance, b , are shown as functions of the varying resistance, r . As shown, the absolute value of admittance, susceptance, and conductance are plotted in full lines, and in dotted line the absolute value of impedance,

$$z = \sqrt{r^2 + x^2} = \frac{1}{y}.$$

Obviously, if the resistance, r , is constant, and the reactance, x , is varied, the values of conductance and susceptance are merely exchanged, the conductance decreasing steadily from $g = 1 / r$ to 0, and the susceptance passing from 0 at $x = 0$ to the maximum, $b = 1 / 2 r = g = 1 / 2 x$ at $x = r$, and to $b = 0$ at $x = \infty$.

The resistance, r , and the reactance, x , vary as functions of the conductance, g , and the susceptance, b , varies, similarly to g and b , as functions of r and x .

The sign in the complex expression of admittance is always opposite to that of impedance; it follows that if the current lags behind the E.M.F., the E.M.F. leads the current, and conversely.

We can thus express Ohm's law in the two forms —

$$\begin{aligned} E &= IZ, \\ I &= EY, \end{aligned}$$

and therefore —

The joint impedance of a number of series-connected impedances is equal to the sum of the individual impedances; the joint admittance of a number of parallel-connected admittances, if expressed in complex quantities, is equal to the sum of the individual admittances. In diagrammatic representation, combination by the parallelogram law takes the place of addition of the complex quantities.

CHAPTER VIII.

CIRCUITS CONTAINING RESISTANCE, INDUCTANCE, AND CAPACITY.

42. Having, in the foregoing, reestablished Ohm's law and Kirchhoff's laws as being also the fundamental laws of alternating-current circuits, or, as expressed in their complex form,

$$E = ZI, \quad \text{or, } I = YE,$$

and

$$\Sigma E = 0 \text{ in a closed circuit,}$$

$$\Sigma I = 0 \text{ at a distributing point,}$$

where E , I , Z , Y , are the expressions of E.M.F., current, impedance, and admittance in complex quantities, — these laws representing not only the intensity, but also the phase, of the alternating wave, — we can now — by application of these laws, and in the same manner as with continuous-current circuits, keeping in mind, however, that E , I , Z , Y , are complex quantities — calculate alternating-current circuits and networks of circuits containing resistance, inductance, and capacity in any combination, without meeting with greater difficulties than when dealing with continuous-current circuits.

It is obviously not possible to discuss with any completeness all the infinite varieties of combinations of resistance, inductance, and capacity which can be imagined, and which may exist, in a system or network of circuits; therefore only some of the more common combinations will here be considered.

1.) *Resistance in series with a circuit.*

43. In a constant-potential system with impressed E.M.F.,

$$E_o = e_o + je_o', \quad E_o = \sqrt{e_o^2 + e_o'^2},$$

let the receiving circuit of impedance

$$Z = r - jx, \quad z = \sqrt{r^2 + x^2},$$

be connected in series with a resistance, r_o .

The total impedance of the circuit is then

$$Z + r_o = r + r_o - jx;$$

hence the current is

$$I = \frac{E_o}{Z + r_o} = \frac{E_o}{r + r_o - jx} = \frac{E_o(r + r_o + jx)}{(r + r_o)^2 + x^2};$$

and the E.M.F. of the receiving circuit, becomes

$$\begin{aligned} E = IZ &= \frac{E_o(r - jx)}{r + r_o - jx} = \frac{E_o\{r(r + r_o) + x^2 - jr_o x\}}{(r + r_o)^2 + x^2} \\ &= \frac{E_o\{z^2 + rr_o - jr_o x\}}{z^2 + 2rr_o + r_o^2}; \end{aligned}$$

or, in absolute values we have the following:—

Impressed E.M.F.,

$$E_o = \sqrt{e_o^2 + e_o'^2};$$

current,

$$I = \frac{E_o}{\sqrt{(r + r_o)^2 + x^2}} = \frac{E_o}{\sqrt{z^2 + 2rr_o + r_o^2}};$$

E.M.F. at terminals of receiver circuit,

$$E = E_o \sqrt{\frac{r^2 + x^2}{(r + r_o)^2 + x^2}} = \frac{E_o z}{\sqrt{z^2 + 2rr_o + r_o^2}};$$

difference of phase in receiver circuit,

$$\tan \hat{\omega} = \frac{r}{x};$$

difference of phase in supply circuit,

$$\tan \hat{\omega}_o = \frac{r + r_o}{x}$$

a.) If x is negligible with respect to r , as in a non-inductive receiving circuit,

$$I = \frac{E_o}{r + r_o}, \quad E = E_o \frac{r}{r + r_o},$$

and the current and E.M.F. at receiver terminals decrease steadily with increasing r_o .

b.) If r is negligible compared with x , as in a wattless receiver circuit,

$$I = \frac{E_o}{\sqrt{r_o^2 + x^2}}, \quad E = E_o \frac{x}{\sqrt{r_o^2 + x^2}};$$

or, for small values of r_o ,

$$I = \frac{E_o}{x}, \quad E = E_o;$$

that is, the current and E.M.F. at receiver terminals remain approximately constant for small values of r_o , and then decrease with increasing rapidity.

44. In the general equations, x appears in the expressions for I and E only as x^2 , so that I and E assume the same value when x is negative, as when x is positive; or, in other words, series resistance acts upon a circuit with leading current, or in a condenser circuit, in the same way as upon a circuit with lagging current, or an inductive circuit.

For a given impedance, z , of the receiver circuit, the current I , and E.M.F., E , are smaller, as r is larger; that is, the less the difference of phase in the receiver circuit.

As an instance, in Fig. 37 are shown in dotted lines the current, I , and the E.M.F., E , at the receiver circuit, for $E_o = \text{const.} = 100$ volts, $z = 1$ ohm, and—

$$\begin{aligned} a.) \quad r_o &= .2 \text{ ohm} && (\text{Curve I.}) \\ b.) \quad r_o &= .8 \text{ ohm} && (\text{Curve II.}) \end{aligned}$$

with values of reactance, $x = \sqrt{z^2 - r^2}$, for abscissæ, from $x = +1.0$ to $x = -1.0$ ohm.

As shown, I and E are smallest for $x = 0$, $r = 1.0$, or for the non-inductive receiver circuit, and largest for $x = \pm 1.0$, $r = 0$, or for the wattless circuit, in which latter a series resistance causes but a very small drop of potential.

Hence the control of a circuit by series resistance depends upon the difference of phase in the circuit.

For $r_o = .8$ and $x = 0$, $x = +.8$, and $x = -.8$, the polar diagrams are shown in Figs. 37, 38, 39.

2.) *Reactance in series with a circuit.*

45. In a constant potential system of impressed E.M.F.,

$$E_o = e_o + je_o', \quad E_o = \sqrt{e_o^2 + e_o'^2},$$

let a reactance, x_o , be connected in series in a receiver circuit of impedance

$$Z = r - jx, \quad z = \sqrt{r^2 + x^2}.$$

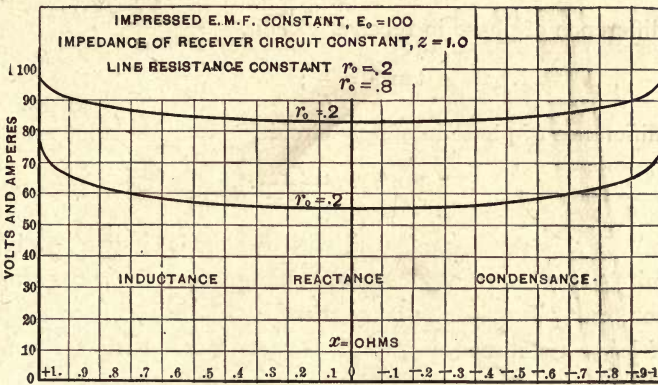


Fig. 37. Variation of Voltage at Constant Series Resistance with Phase Relation of Receiver Circuit.

Then, the total impedance of the circuit is

$$Z + x_o = r - j(x + x_o).$$



Fig. 38.

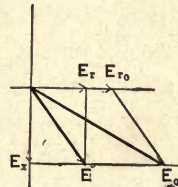


Fig. 39.

and the current is,

$$I = \frac{E_o}{Z + x_o} = \frac{E_o}{r - j(x + x_o)};$$

while the difference of potential at the receiver terminals is,

$$E = IZ = E_o \frac{r - jx}{r - j(x + x_o)}.$$

Or, in absolute quantities :—

Current,

$$I = \frac{E_0}{\sqrt{r^2 + (x + x_0)^2}} = \frac{E_0}{\sqrt{z^2 + 2xx_0 + x_0^2}};$$

E.M.F. at receiver terminals,

$$E = E_0 \sqrt{\frac{r^2 + x^2}{r^2 + (x + x_0)^2}} = \frac{E_0 z}{\sqrt{z^2 + 2xx_0 + x_0^2}};$$

difference of phase in receiver circuit,

$$\tan \hat{\omega} = \frac{r}{x};$$

difference of phase in supply circuit,

$$\tan \hat{\omega}_0 = \frac{r}{x + x_0}.$$

a.) If x is small compared with r , that is, if the receiver circuit is non-inductive, I and E change very little for small values of x_0 ; but if x is large, that is, if the receiver circuit is of large reactance, I and E change much with a change of x_0 .

b.) If x is negative, that is, if the receiver circuit contains condensers, synchronous motors, or other apparatus which produce leading currents—above a certain value of x_0 the denominator in the expression of E , becomes $< z$, or $E > E_0$; that is, the reactance, x_0 , raises the potential.

c.) $E = E_0$, or the insertion of a series inductance, x_0 , does not affect the potential difference at the receiver terminals, if

$$\sqrt{z^2 + 2xx_0 + x_0^2} = z;$$

or,

$$x_0 = -2x.$$

That is, if the reactance which is connected in series in the circuit is of opposite sign, but twice as large as the reactance of the receiver circuit, the voltage is not affected, but $E = E_0$, $I = E_0/z$. If $x_0 > -2x$, it raises, if $x < -2x$, it lowers, the voltage.

We see, then, that a reactance inserted in series in an alternating-current circuit will lower the voltage at the

receiver terminals only when of the same sign as the reactance of the receiver circuit; when of opposite sign, it will lower the voltage if larger, raise the voltage if less, than twice the numerical value of the reactance of the receiver circuit.

d.) If $x = 0$, that is, if the receiver circuit is non-inductive, the E.M.F. at receiver terminals is :

$$E = \frac{E_0 r}{\sqrt{r^2 + x_0^2}} = \frac{E_0}{\sqrt{1 + \left(\frac{x_0}{r}\right)^2}}$$

$$= E_0 \left\{ 1 - \frac{1}{2} \left(\frac{x_0}{r}\right)^2 + \frac{3}{8} \left(\frac{x_0}{r}\right)^4 - + \dots \right\}$$

$\left(\frac{1}{\sqrt{1+x}} = (1+x)^{-\frac{1}{2}}\right)$ expanded by the binomial theorem is

$$(1+x)^n = 1 + nx + \frac{n(n-1)}{1 \cdot 2} x^2 + \dots$$

Therefore, if x_0 is small compared with r :—

$$E = E_0 \left(1 - \frac{1}{2} \left(\frac{x_0}{r}\right)^2 \right),$$

$$\frac{E_0 - E}{E_0} = \frac{1}{2} \left(\frac{x_0}{r}\right)^2.$$

That is, the percentage drop of potential by the insertion of reactance in series in a non-inductive circuit is, for small

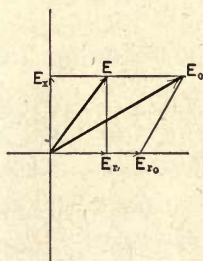


Fig. 40.

values of reactance, independent of the sign, but proportional to the square of the reactance, or the same whether it be inductance or condensance reactance.

46. As an instance, in Fig. 41 the changes of current, I , and of E.M.F. at receiver terminals, E , at constant impressed E.M.F., E_0 , are shown for various conditions of a receiver circuit and amounts of reactance inserted in series.

Fig. 41 gives for various values of reactance, x_0 (if positive, inductance — if negative, condensance), the E.M.F.s, E , at receiver terminals, for constant impressed E.M.F.,

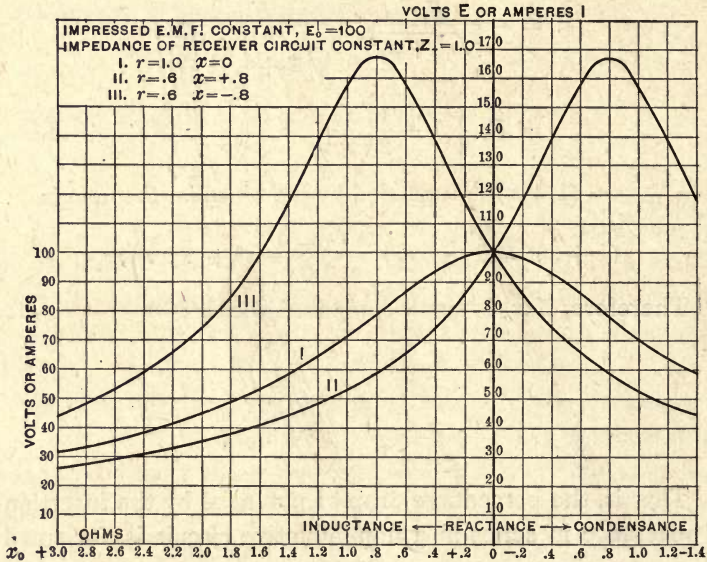


Fig. 41.

$E_0 = 100$ volts, and the following conditions of receiver circuit :—

$$z = 1.0, r = 1.0, x = 0 \text{ (Curve I.)}$$

$$z = 1.0, r = .6, x = .8 \text{ (Curve II.)}$$

$$z = 1.0, r = .6, x = -.8 \text{ (Curve III.)}$$

As seen, curve I is symmetrical, and with increasing x_0 the voltage E remains first almost constant, and then drops off with increasing rapidity.

In the inductive circuit series inductance, or, in a condenser circuit series condensance, causes the voltage to drop off very much faster than in a non-inductive circuit.

Series inductance in a condenser circuit, and series condensance in an inductive circuit, cause a rise of potential. This rise is a maximum for $x_o = \pm .8$, or, $x_o = -x$ (the condition of resonance), and the E.M.F. reaches the value, $E = 167$ volts, or, $E = E_o \sqrt{r}$. This rise of potential by series reactance continues up to $x_o = \pm 1.6$, or, $x_o = -2x$,

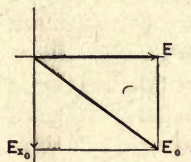


Fig. 42.

where $E = 100$ volts again; and for $x_o > 1.6$ the voltage drops again.

At $x_o = \pm .8$, $x = \mp .8$, the total impedance of the circuit is $r - j(x + x_o) = r = .6$, $x + x_o = 0$, and $\tan \phi_o = 0$; that is, the current and E.M.F. in the supply circuit are in phase with each other, or the circuit is in *electrical resonance*.

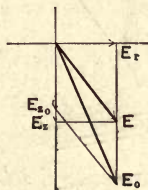


Fig. 43.

Since a synchronous motor in the condition of efficient working acts as a condensance, we get the remarkable result that, in synchronous motor circuits, choking coils, or reactive coils, can be used for raising the voltage.

In Figs. 42 to 44, the polar diagrams are shown for the conditions —

$E_o = 100$, $x_o = .6$, $x = 0$	(Fig. 42) $E = 85.7$
$x = +.4$	(Fig. 43) $E = 73.7$
$x = -.4$	(Fig. 44) $E = 106.6$

47. In Fig. 45 the dependence of the potential, E , upon the difference of phase, $\hat{\omega}$, in the receiver circuit is shown for the constant impressed E.M.F., $E_o = 100$; for the constant receiver impedance, $z = 1.0$ (but of various phase differences $\hat{\omega}$), and for various series reactances, as follows :

$x_o = .2$	(Curve I.)
$x_o = .6$	(Curve II.)
$x_o = .8$	(Curve III.)
$x_o = 1.0$	(Curve IV.)
$x_o = 1.6$	(Curve V.)
$x_o = 3.2$	(Curve VI.)

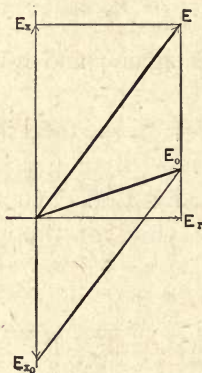


Fig. 44.

Since $z = 1.0$, the current, I , in all these diagrams has the same value as E .

In Figs. 46 and 47, the same curves are plotted as in Fig. 45, but in Fig. 46 with the reactance, x , of the receiver circuit as abscissæ; and in Fig. 47 with the resistance, r , of the receiver circuit as abscissæ.

As shown, the receiver voltage, E , is always lowest when x_o and x are of the same sign, and highest when they are of opposite sign.

The rise of voltage due to the balance of x_o and x is a maximum for $x_o = +1.0$, $x = -1.0$, and $r = 0$, where

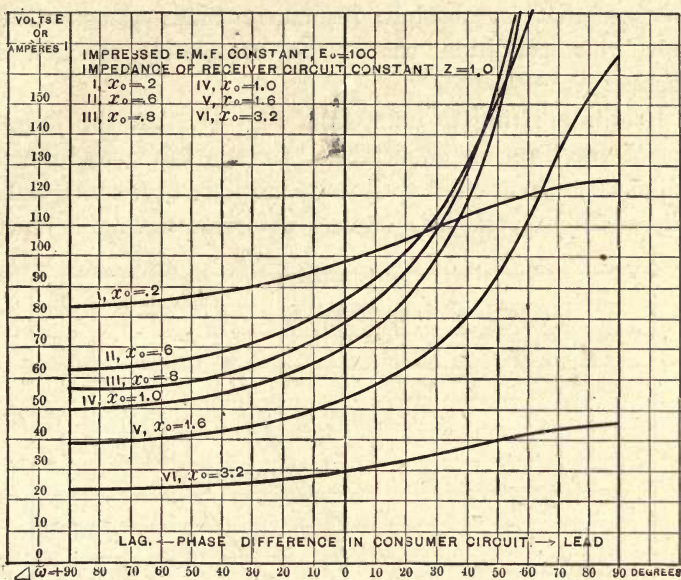


Fig. 45. Variation of Voltage at Constant Series Reactance with Phase Angle of Receiver Circuit.

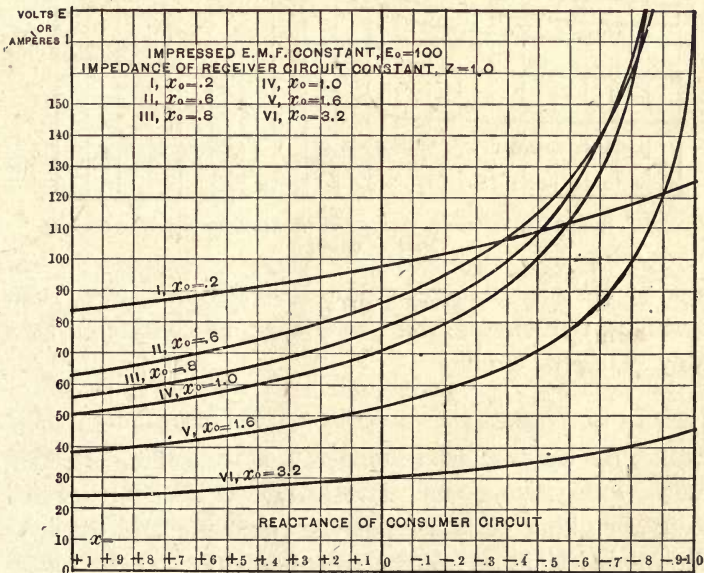


Fig. 46. Variation of Voltage at Constant Series Reactance with Reactance of Receiver Circuit.

$E = \infty$; that is, absolute resonance takes place. Obviously, this condition cannot be completely reached in practice.

It is interesting to note, from Fig. 47, that the largest part of the drop of potential due to inductance, and rise to condensance — or conversely — takes place between $r = 1.0$ and $r = .9$; or, in other words, a circuit having a power

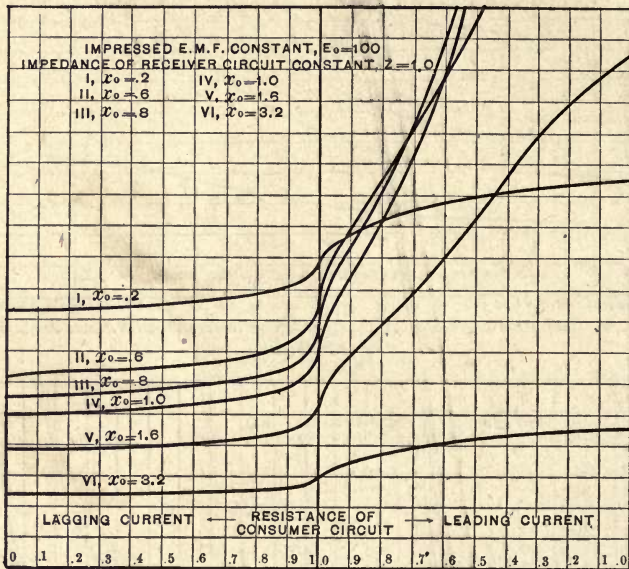


Fig. 47. Variation of Voltage at Constant Series Reactance with Resistance of Receiver Circuit.

factor of $\cos \hat{\omega} = .9$, gives a drop several times larger than a non-inductive circuit, and hence must be considered as a highly inductive circuit.

3.) Impedance in series with a circuit.

48. By the use of reactance for controlling electric circuits, a certain amount of resistance is also introduced, due to the ohmic resistance of the conductor and the hysteric loss, which, as will be seen hereafter, can be represented as an effective resistance.

Hence the impedance of a reactive coil (choking coil) may be written thus:—

$$Z_o = r_o - jx_o, z_o = \sqrt{r_o^2 + x_o^2},$$

where r_o is in general small compared with x_o .

From this, if the impressed E.M.F. is

$$E_o = e_o + je_o', E_o = \sqrt{e_o^2 + e_o'^2}$$

and the impedance of the consumer circuit is

$$Z = r - jx = z = \sqrt{r^2 + x^2}$$

we get the current, $I = \frac{E_o}{Z + Z_o} = \frac{E_o}{(r + r_o) - j(x + x_o)}$

and the E.M.F. at receiver terminals,

$$E = E_o \frac{Z}{Z + Z_o} = E_o \frac{r - jx}{(r + r_o) - j(x + x_o)}.$$

Or, in absolute quantities,

the current is,

$$I = \frac{E_o}{\sqrt{(r + r_o)^2 + (x + x_o)^2}} = \frac{E_o}{\sqrt{z^2 + z_o^2 + 2(rr_o + xx_o)}};$$

the E.M.F. at receiver terminals is,

$$E = \frac{E_o z}{\sqrt{(r + r_o)^2 + (x + x_o)^2}} = \frac{E_o z}{\sqrt{z^2 + z_o^2 + 2(rr_o + xx_o)}};$$

the difference of phase in receiver circuit is,

$$\tan \hat{\omega} = \frac{r}{x};$$

and the difference of phase in the supply circuit is,

$$\tan \hat{\omega}_o = \frac{r + r_o}{x + x_o}.$$

49. In this case, the maximum drop of potential will not take place for either $x = 0$, as for resistance in series, or for $r = 0$, as for reactance in series, but at an intermediate point. The drop of voltage is a maximum; that is, E is a minimum if the denominator of E is a maximum; or, since z , z_o , r_o , x_o are constant if $rr_o + xx_o$ is a maximum, since $x = \sqrt{z^2 - r^2}$ if $rr_o + x_o \sqrt{z^2 - r^2}$ is a maximum,

a function, $f = rr_0 + x_0 \sqrt{z^2 - r^2}$ is a maximum when its differential coefficient equals zero. For, plotting f as curve with r as abscissæ, at the point where f is a maximum or a minimum, this curve is for a short distance horizontal, hence the tangens-function of its tangent equals zero. The tangens-function of the tangent of a curve, however, is the ratio of the change of ordinates to the change of abscissæ, or is the differential coefficient of the function represented by the curve.

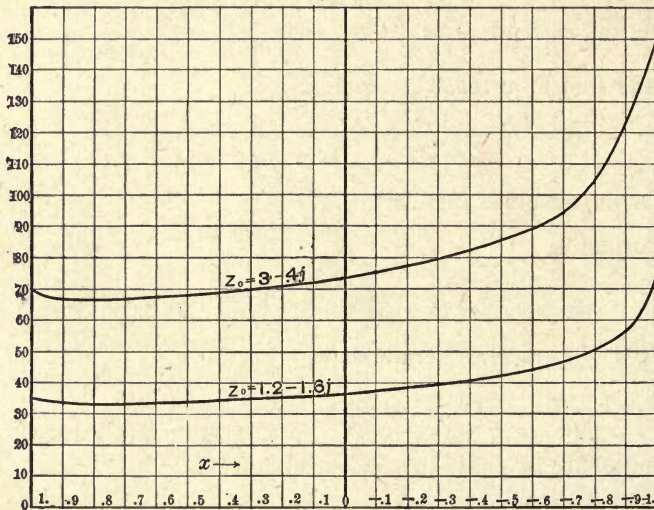


Fig. 48.

Thus we have :—

$$f = rr_0 + x_0 \sqrt{z^2 - r^2} = \text{maximum or minimum, if}$$

$$\frac{df}{dr} = 0.$$

Differentiating, we get :—

$$r_0 + \frac{1}{2} \frac{x_0}{\sqrt{z^2 - r^2}} (-2r) = 0;$$

or, expanded, —

$$r_0 \sqrt{z^2 - r^2} - x_0 r = r_0 x - x_0 r = 0,$$

or,

$$r \div x = r_0 \div x_0.$$

That is, the drop of potential is a maximum, if the reactance factor, x/r , of the receiver circuit equals the reactance factor, x_0/r_0 , of the series impedance.

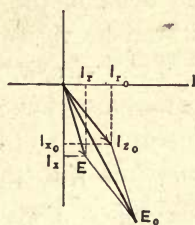


Fig. 49.

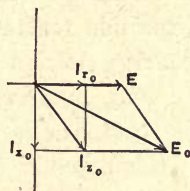


Fig. 50.

50. As an example, Fig. 48 shows the E.M.F., E , at the receiver terminals, at a constant impressed E.M.F., $E_0 = 100$, a constant impedance of the receiver circuit, $z = 1.0$, and constant series impedances,

$$Z = .3 - j.4 \quad (\text{Curve I.})$$

$$Z_0 = 1.2 - j1.6 \quad (\text{Curve II.})$$

as functions of the reactance, x , of the receiver circuit.

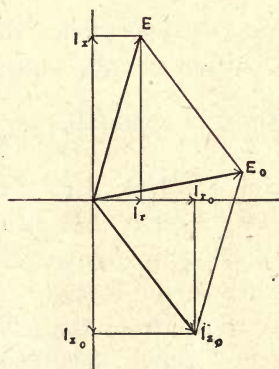


Fig. 51.

Figs. 49 to 51 give the polar diagram for $E_0 = 100$, $x = .9$, $x = 0$, $x = -.9$, and $Z_0 = .3 - j.4$.

4.) *Compensation for Lagging Currents by Shunted Condensance.*

51. We have seen in the latter paragraphs, that in a constant potential alternating-current system, the voltage at the terminals of a receiver circuit can be varied by the use of a variable reactance in series to the circuit, without loss of energy except the unavoidable loss due to the resistance and hysteresis of the reactance; and that, if the series reactance is very large compared with the resistance of the receiver circuit, the current in the receiver circuit becomes more or less independent of the resistance, — that is, of the power consumed in the receiver

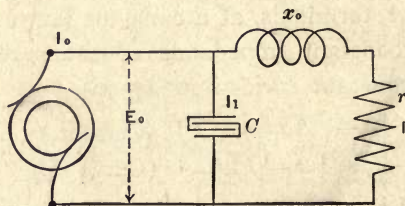


Fig. 52.

circuit, which in this case approaches the conditions of a constant alternating-current circuit, whose current is.

$$I = \frac{E_0}{\sqrt{r^2 + x_0^2}}, \text{ or approximately, } I = \frac{E_0}{x_0}.$$

This potential control, however, causes the current taken from the mains to lag greatly behind the E.M.F., and thereby requires a much larger current than corresponds to the power consumed in the receiver circuit.

Since a condenser draws from the mains a leading current, a condenser shunted across such a circuit with lagging current will compensate for the lag, the leading and the lagging current combining to form a resultant current more or less in phase with the E.M.F., and therefore proportional to the power expended.

In a circuit shown diagrammatically in Fig. 52, let the non-inductive receiver circuit of resistance, r , be connected in series with the inductance, x_o , and the whole shunted by a condenser of condensance, c , entailing but a negligible loss of energy.

Then, if $E_o =$ impressed E.M.F., —
the current in receiver circuit is,

$$I = \frac{E_o}{r - jx_o}, \quad I = \frac{E_o}{\sqrt{r^2 + x_o^2}};$$

the current in condenser circuit is,

$$I_1 = \frac{E_o}{jc}, \quad I_1 = \frac{E_o}{c}.$$

and the total current is

$$\begin{aligned} I_o = I + I_1 &= E_o \left\{ \frac{1}{r - jx_o} + \frac{1}{jc} \right\} \\ &= E_o \left\{ \frac{r}{r^2 + x_o^2} + j \left(\frac{x_o}{r^2 + x_o^2} - \frac{1}{c} \right) \right\}, \end{aligned}$$

or, in absolute terms, $I_o = E_o \sqrt{\left(\frac{r}{r^2 + x_o^2} \right)^2 + \left(\frac{x_o}{r^2 + x_o^2} - \frac{1}{c} \right)^2}$;

while the E.M.F. at receiver terminals is,

$$E = Ir = E_o \frac{r}{r - jx_o}, \quad E = \frac{E_o r}{\sqrt{r^2 + x_o^2}}.$$

52. The main current, I_o , is in phase with the impressed E.M.F., E_o , or the lagging current is completely balanced, or supplied by, the condensance, if the imaginary term in the expression of I_o disappears; that is, if

$$\frac{x_o}{r^2 + x_o^2} - \frac{1}{c} = 0.$$

This gives, expanded: $c = \frac{r^2 + x_o^2}{x_o}$.

Hence the capacity required to compensate for the lagging current produced by the insertion of inductance in series to a non-inductive circuit depends upon the resistance and the inductance of the circuit. x_o being constant,

with increasing resistance, r , the condensance has to be increased, or the capacity decreased, to keep the balance.

$$\text{Substituting } c = \frac{r^2 + x_o^2}{x_o},$$

we get, as the equations of the inductive circuit balanced by condensance:—

$$\begin{aligned} I &= \frac{E_o}{r - jx_o} = \frac{E_o (r + jx_o)}{r^2 + x_o^2}, & I &= \frac{E_o}{\sqrt{r^2 + x_o^2}}; \\ I_1 &= -\frac{jE_o x_o}{r^2 + x_o^2}, & I_1 &= \frac{E_o x_o}{r^2 + x_o^2}; \\ I_o &= \frac{E_o r}{r^2 + x_o^2}, & I_o &= \frac{E_o r}{r^2 + x_o^2}; \\ E &= \frac{E_o r}{r - jx_o}, & E &= \frac{E_o r}{\sqrt{r^2 + x_o^2}}; \end{aligned}$$

and for the power expended in the receiver circuit:—

$$I^2 r = \frac{E_o^2 r}{r^2 + x_o^2} = I_o E_o,$$

that is, the main current is proportional to the expenditure of power.

For $r = 0$ we have $x = x_o$, or the condition of balance.

Complete balance of the lagging component of current by shunted capacity thus requires that the condensance, c , be varied with the resistance, r ; that is, with the varying load on the receiver circuit.

In Fig. 53 are shown, for a constant impressed E.M.F., $E_o = 1000$ volts, and a constant series reactance, $x_o = 100$ ohms, values for the balanced circuit of,

- current in receiver circuit (Curve I.),
- current in condenser circuit (Curve II.),
- current in main circuit (Curve III.),
- E.M.F. at receiver terminals (Curve IV.),

with the resistance, r , of the receiver circuit as abscissæ.

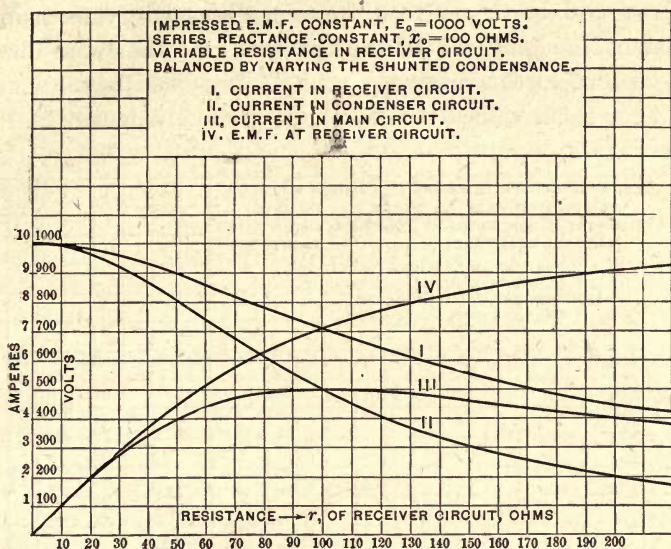


Fig. 53. Compensation of Lagging Currents in Receiving Circuit by Variable Shunted Condensance.

53. If, however, the condensance is left unchanged, $c = x_0$ at the no-load value, so that if the circuit is balanced for $r = 0$, it will be overbalanced for $r > 0$, and the main current will become leading.

We get in this case:—

$$c = x_0;$$

$$I = \frac{E_0}{r - jx_0}, \quad I = \frac{E_0}{\sqrt{r^2 + x_0^2}};$$

$$I_1 = -\frac{jE_0}{x_0}, \quad I_1 = \frac{E_0}{x_0};$$

$$I_0 = I + I_1 = \frac{E_0 r}{x_0(x_0 + jr)}, \quad I_0 = \frac{E_0 r}{x_0 \sqrt{r^2 + x_0^2}};$$

$$E = Ir = \frac{E_0 r}{r - jx_0}, \quad E = \frac{E_0 r}{\sqrt{r^2 + x_0^2}}.$$

The difference of phase in the main circuit is,—

$$\tan \hat{\omega}_0 = -\frac{r}{x_0} = 0$$

when $r = 0$ or at no load, and increases with increasing resistance, as the lead of the current. At the same time, the current in the receiver circuit, I , is approximately constant for small values of r , and then gradually decreases.

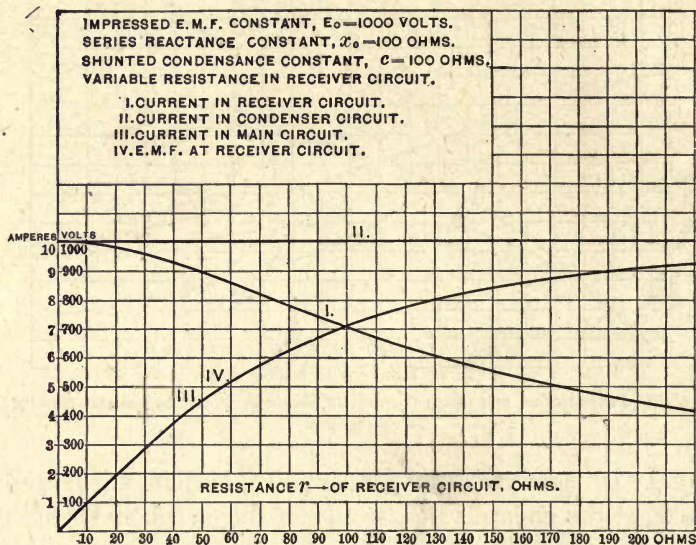


Fig. 54.

In Fig. 54 are shown the values of I , I_1 , I_0 , E , in Curves I., II., III., IV., similarly as in Fig. 50, for $E_0 = 1000$ volts, $c = x_0 = 100$ ohms, and r as abscissæ.

5.) Constant Potential—Constant Current Transformation.

54. In a constant potential circuit containing a large and constant reactance, x_1 , and a varying resistance, r , the current is approximately constant, and only gradually drops off with increasing resistance, r ,—that is, with increasing load,—but the current lags greatly behind the E.M.F. This lagging current in the receiver circuit can be supplied by a shunted condensance. Leaving, however, the condensance constant, $c = x_0$, so as to balance the lagging current at no

load, that is, at $r = 0$, it will overbalance with increasing load, that is, with increasing r , and thus the main current will become leading, while the receiver current decreases if the impressed E.M.F., E'_0 , is kept constant. Hence, to keep the current in the receiver circuit entirely constant, the impressed E.M.F., E_0 , has to be increased with increasing resistance, r ; that is, with increasing lead of the main current. Since, as explained before, in a circuit with leading current, a series inductance raises the potential, to maintain the current in the receiver circuit constant under all loads, an inductance, x_2 , inserted in the main circuit, as shown in the diagram, Fig. 55, can be used for raising the potential, E_0 , with increasing load.

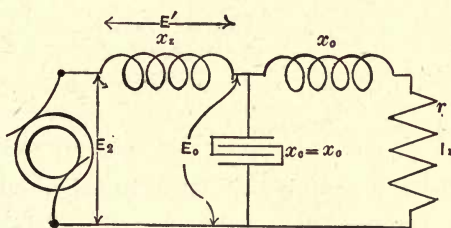


Fig. 55.

Let —

$$E_2 = e_2 + j e_2', \quad E_0 = \sqrt{e_2'^2 + e_2'^2},$$

be the impressed E.M.F. of the generator, or of the mains, and let the condensance be $x_c = x_0$; then —

Current in receiver circuit,

$$I = \frac{E_0}{r - j x_0};$$

current in condenser circuit,

$$I_1 = - \frac{j E_0}{x_0}.$$

Hence, the total current in main line is

$$\begin{aligned} I_0 &= I + I_1 = E_0 \left\{ \frac{1}{r - j x_0} - \frac{j}{x_0} \right\} \\ &= \frac{E_0 r}{j x_0 (r - j x_0)}, \end{aligned}$$

and the E.M.F. at receiver terminals,

$$E = Ir = \frac{E_o r}{r - jx_o};$$

E.M.F. at condenser terminals,

$$E_o;$$

E.M.F. consumed in main line,

$$E' = -jI_o x_2 = -\frac{E_o r x_2}{x_o(r - jx_o)};$$

hence, the E.M.F. at generator is

$$E_2 = E_o + E' = E_o \left\{ 1 - \frac{r^2}{x_o(r - jx_o)} \right\};$$

or,

$$= E_o \frac{r(x_o - x_2) - jx_o^2}{x_o(r - jx_o)}.$$

and the E.M.F. at condenser terminals,

$$E_o = \frac{E_2 x_o (r - jx_o)}{r(x_o - x_2) - jx_o^2};$$

current in receiver circuit,

$$I = \frac{E_o}{r - jx_o} = \frac{E_2 x_o}{r(x_o - x_2) - jx_o^2}.$$

This value of I contains the resistance, r , only as a factor to the difference, $x_o - x_2$; hence, if the reactance, x_2 , is chosen $= x_o$, r cancels altogether, and we find that if $x_2 = x_o$, the current in the receiver circuit is constant,

$$I = j \frac{E_2}{x_o},$$

and is independent of the resistance, r ; that is, of the load.

Thus, by substituting, we have, $x_2 = x_o$, -
Impressed E.M.F. at generator,

$$E_2 = e_2 + j e_2', \quad E_2 = \sqrt{e_2^2 + e_2'^2} = \text{constant};$$

current in receiver circuit,

$$I = j \frac{E_2}{x_o}, \quad I = \frac{E_2}{x_o} = \text{constant};$$

E.M.F. at receiver circuit,

$$E = Ir = j \frac{E_2 r}{x_o}, \quad E = \frac{E_2 r}{x_o}, \text{ or proportional to load } r;$$

E.M.F. at condenser terminals,

$$E_o = \frac{E_2(x_o + jr)}{x_o}$$

$$= E_2 \left(1 + j \frac{r}{x_o} \right), \quad E_o = E_2 \sqrt{1 + \left(\frac{r}{x_o} \right)^2}, \text{ hence } > E_2;$$

current in condenser circuit,

$$I_1 = -j \frac{E_2(x_o + jr)}{x_o^2}, \quad I_1 = \frac{E_2}{x_o} \sqrt{1 + \left(\frac{r}{x_o} \right)^2};$$

main current,

$$I_o = \frac{E_o r}{x_o(x_o + jr)};$$

$$= \frac{E_2 r}{x_o^2}, \quad I_o = \frac{E_2 r}{x_o^2}, \quad \left\{ \begin{array}{l} \text{proportional to the load,} \\ r, \text{ and in phase with} \\ \text{E.M.F., } E_2. \end{array} \right.$$

The power of the receiver circuit is,

$$IE = \frac{E_2^2 r}{x_o^2};$$

the power of the main circuit,

$$I_o E_2 = \frac{E_2^2 r}{x_o^2}, \text{ hence the same.}$$

55. This arrangement is entirely reversible; that is,

if $E_2 = \text{constant}$, $I = \text{constant}$; and

if $I_o = \text{constant}$, $E = \text{constant}$.

In the latter case we have, by expressing all the quantities by I_o :—

Current in main line,

$$I_o = \text{constant};$$

E.M.F. at receiver circuit,

$$E = I_o x_o = \text{constant};$$

current in receiver circuit,

$$I = I_o \frac{x_o}{r}, \text{ proportional to the load } \frac{1}{r};$$

current in condenser circuit,

$$I = I_o \sqrt{1 + \left(\frac{x_o}{r} \right)^2};$$

E.M.F. at condenser terminals,

$$E_o = x_o I_o \sqrt{1 + \left(\frac{x_o}{r}\right)^2};$$

Impressed E.M.F. at generator terminals,

$$E_2 = \frac{x_o^2}{r} I_o, \text{ or proportional to the load } \frac{1}{r}.$$

From the above we have the following deduction :

Connecting two reactances of equal value, x_o , in series to a non-inductive receiver circuit of variable resistance, r , and shunting across the circuit from midway between the inductances by a capacity of condensance, $x_c = x_o$, transforms a constant potential main circuit into a constant current receiver circuit, and, inversely, transforms a constant current main circuit into a constant potential receiver circuit. This combination of inductance and capacity acts as a transformer, and converts from constant potential to constant current and inversely, without introducing a displacement of phase between current and E.M.F.

It is interesting to note here that a short circuit in the receiver circuit acts like a break in the supply circuit, and a break in the receiver circuit acts like a short circuit in the supply circuit.

As an instance, in Fig. 56 are plotted the numerical values of a transformation from constant potential of 1,000 volts to constant current of 10 amperes.

Since $E_2 = 1,000$, $I = 10$, we have: $x_o = 100$; hence the constants of the circuit are:—

$$E_2 = 1000 \text{ volts};$$

$$I = 10 \text{ amperes};$$

$$E = 10r, \text{ plotted as Curve I., with the resistances, } r, \text{ as abscissæ};$$

$$E_o = 1000 \sqrt{1 + \left(\frac{r}{100}\right)^2}, \text{ plotted as Curve II.};$$

$$I_1 = 10 \sqrt{1 + \left(\frac{r}{100}\right)^2}, \text{ plotted as Curve III.}$$

$$I_o = .1r, \text{ plotted as Curve IV.}$$

56. In practice, the power consumed in the main circuit will be larger than the power delivered to the receiver circuit, due to the unavoidable losses of power in the inductances and condensances.

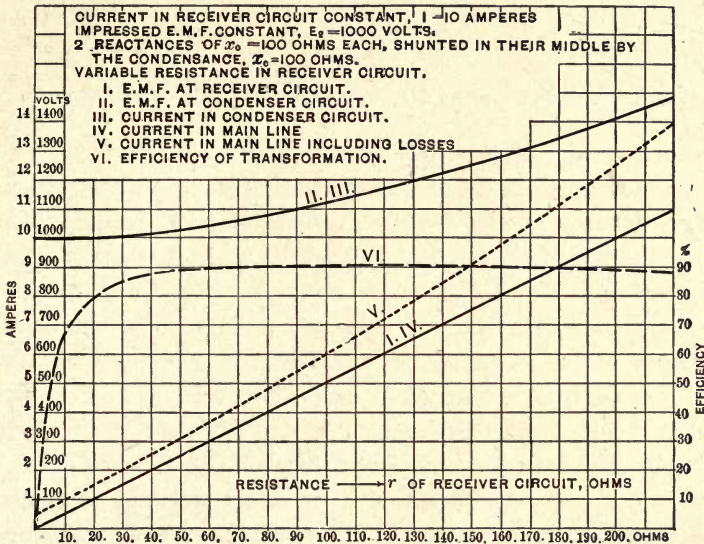


Fig. 56. Constant-Potential — Constant-Current Transformation.

Let —

- $r_1 = 2$ ohms = effective resistance of condensance ;
- $r_o = 3$ ohms = effective resistance of each of the inductances.

We then have :—

Power consumed in condensance, $I_1^2 r_1 = 200 + .02 r^2$;
 power consumed by first inductance, $I^2 r_o = 300$;
 power consumed by second inductance, $I_o^2 r_o = .03 r^2$.

Hence, the total loss of energy is $500 + .05 r^2$;

output of system, $I^2 r = 100 r$
 input, $500 + 100 r + .05 r^2$;
 efficiency, $\frac{100 r}{500 + 100 r + .05 r^2}$.

It follows that the main current, I_o , increases slightly by the amount necessary to supply the losses of energy in the apparatus.

This curve of current, I_0 , including losses in transformation, is shown in dotted lines as Curve V. in Fig. 56 ; and the efficiency is shown in broken line, as Curve VI. As shown, the efficiency is practically constant within a wide range.

CHAPTER IX.

RESISTANCE AND REACTANCE OF TRANSMISSION LINES.

57. In alternating-current circuits, E.M.F. is consumed in the feeders of distributing networks, and in the lines of long-distance transmissions, not only by the resistance, but also by the reactance, of the line. The E.M.F. consumed by the resistance is in phase, while the E.M.F. consumed by the reactance is in quadrature, with the current. Hence their influence upon the E.M.F. at the receiver circuit depends upon the difference of phase between the current and the E.M.F. in that circuit. As discussed before, the drop of potential due to the resistance is a maximum when the receiver current is in phase, a minimum when it is in quadrature, with the E.M.F. The change of potential due to line reactance is small if the current is in phase with the E.M.F., while a drop of potential is produced with a lagging, and a rise of potential with a leading, current in the receiver circuit.

Thus the change of potential due to a line of given resistance and inductance depends upon the phase difference in the receiver circuit, and can be varied and controlled by varying this phase difference; that is, by varying the admittance, $Y = g + jb$, of the receiver circuit.

The conductance, g , of the receiver circuit depends upon the consumption of power, — that is, upon the load on the circuit, — and thus cannot be varied for the purpose of regulation. Its susceptance, b , however, can be changed by shunting the circuit with a reactance, and will be increased by a shunted inductance, and decreased by a shunted condensation. Hence, for the purpose of investigation, the

receiver circuit can be assumed to consist of two branches, a conductance, g , — the non-inductive part of the circuit, — shunted by a susceptance, b , which can be varied without expenditure of energy. The two components of current can thus be considered separately, the energy component as determined by the load on the circuit, and the wattless component, which can be varied for the purpose of regulation.

Obviously, in the same way, the E.M.F. at the receiver circuit may be considered as consisting of two components, the energy component, in phase with the current, and the wattless component, in quadrature with the current. This will correspond to the case of a reactance connected in series to the non-inductive part of the circuit. Since the effect of either resolution into components is the same so far as the line is concerned, we need not make any assumption as to whether the wattless part of the receiver circuit is in shunt, or in series, to the energy part.

Let —

$Z_o = r_o - jx_o =$ impedance of the line ;

$$z_o = \sqrt{r_o^2 + x_o^2};$$

$Y = g + jb =$ admittance of receiver circuit ;

$$y = \sqrt{g^2 + b^2};$$

$E_o = e_o + je_o' =$ impressed E.M.F. at generator end of line ;

$$E_o = \sqrt{e_o^2 + e_o'^2};$$

$E = e + je' =$ E.M.F. at receiver end of line ;

$$E = \sqrt{e^2 + e'^2};$$

$I_o = i_o + ji_o' =$ current in the line ; $I_o = \sqrt{i_o^2 + i_o'^2}$.

The simplest condition is that of a non-inductive receiver circuit, such as a lighting circuit.

1.) *Non-inductive Receiver Circuit Supplied over an Inductive Line.*

58. In this case, the admittance of the receiver circuit is $Y = g$, since $b = 0$.

We have then —

current, $I_o = E g;$
 impressed E.M.F., $E_o = E + Z_o I_o = E (1 + Z_o g).$

Hence —

E.M.F. at receiver circuit,

$$E = \frac{E_o}{1 + Z_o g} = \frac{E_o}{1 + g r_o - j g x_o};$$

current, $I_o = \frac{E_o g}{1 + Z_o g} = \frac{E_o g}{1 + g r_o - j g x_o}.$

Hence, in absolute values —

E.M.F. at receiver circuit, $E = \frac{E_o}{\sqrt{(1 + g r_o)^2 + g^2 x_o^2}};$

current, $I_o = \frac{E_o g}{\sqrt{(1 + g r_o)^2 + g^2 x_o^2}}.$

The ratio of E.M.Fs. at receiver circuit and at generator, or supply circuit, is —

$$\alpha = \frac{E}{E_o} = \frac{1}{\sqrt{(1 + g r_o)^2 + g^2 x_o^2}};$$

and the power delivered in the non-inductive receiver circuit, or

output, $P = I_o E = \frac{E_o^2 g}{(1 + g r_o)^2 + g^2 x_o^2}.$

As a function of g , and with a given E_o , r_o , and x_o , this power is a maximum, if —

$$\frac{dP}{dg} = 0;$$

that is —

$$-1 + g^2 r_o^2 + g^2 x_o^2 = 0;$$

hence —

conductance of receiver circuit for maximum output,

$$g_m = \frac{1}{\sqrt{r_o^2 + x_o^2}} = \frac{1}{z_o}.$$

Resistance of receiver circuit, $r_m = \frac{1}{g_m} = z_o;$

and, substituting this in P —

$$\text{Maximum output, } P_m = \frac{E_o^2}{2(r_o + z_o)} = \frac{E_o^2}{\{2r_o + \sqrt{r_o^2 + x_o^2}\}};$$

and—

ratio of E.M.F. at receiver and at generator end of line,

$$a_m = \frac{E}{E_o} = \frac{1}{\sqrt{2\left(1 + \frac{r_o}{x_o}\right)}};$$

efficiency,

$$\frac{r_m}{r_m + r_o} = \frac{z_o}{r_o + z_o}.$$

That is, the output which can be transmitted over an inductive line of resistance, r_o , and reactance, x_o ,—that is, of impedance, z_o ,—into a non-inductive receiver circuit, is a maximum, if the resistance of the receiver circuit equals the impedance of the line, $r = z_o$, and is—

$$P_m = \frac{E_o^2}{2(r_o + z_o)}.$$

The output is transmitted at the efficiency of

$$\frac{z_o}{r_o + z_o},$$

and with a ratio of E.M.Fs. of

$$a_m = \frac{1}{\sqrt{2\left(1 + \frac{r_o}{z_o}\right)}}.$$

59. We see from this, that the maximum output which can be delivered over an inductive line is less than the output delivered over a non-inductive line of the same resistance—that is, which can be delivered by continuous currents with the same generator potential.

In Fig. 57 are shown, for the constants

$E_o = 1000$ volts,

$Z_o = 2.5 - 6j$; that is, $r_o = 2.5$ ohms, $x_o = 6$ ohms, $z_o = 6.5$ ohms,

with the current I_o as abscissæ, the values—

- E.M.F. at Receiver Circuit, E , (Curve I.);
- Output of Transmission, P , (Curve II.);
- Efficiency of Transmission, (Curve III.).

The same quantities, E and P , for a non-inductive line of resistance, $r_o = 2.5$ ohms, $x_o = 0$, are shown in Curves IV., V., and VI.

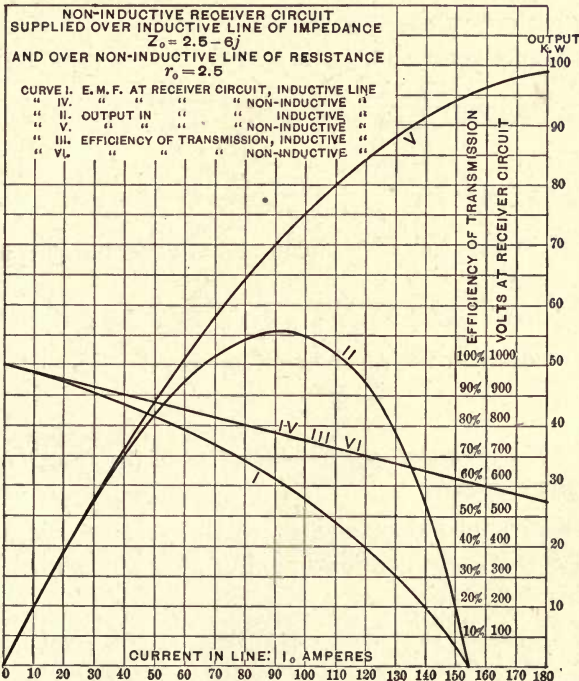


Fig. 57. Non-inductive Receiver Circuit Supplied Over Inductive Line.

2.) Maximum Power Supplied over an Inductive Line.

60. If the receiver circuit contains the susceptance, b , in addition to the conductance, g , its admittance can be written thus:—

$$Y = g + jb, \quad y = \sqrt{g^2 + b^2}.$$

Then —

current,

$$I_o = EY;$$

Impressed E.M.F., $E_o = E + I_o Z_o = E (1 + YZ_o)$.

Hence —

E.M.F. at receiver terminals,

$$E = \frac{E_o}{1 + YZ_o} = \frac{E_o}{(1 + r_o g + x_o b) - j(x_o g - r_o b)};$$

current,

$$I_o = \frac{E_o Y}{1 + YZ_o} = \frac{E_o (g + jb)}{(1 + r_o g + x_o b) - j(x_o g - r_o b)};$$

or, in absolute values —

E.M.F. at receiver circuit,

$$E = \frac{E_o}{\sqrt{(1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2}};$$

current,

$$I_o = E_o \sqrt{\frac{g^2 + b^2}{(1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2}};$$

ratio of E.M.Fs. at receiver circuit and at generator circuit,

$$\alpha = \frac{E}{E_o} = \frac{1}{\sqrt{(1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2}};$$

and the output in the receiver circuit is,

$$P = E^2 g = E_o^2 \alpha^2 g.$$

61. a.) *Dependence of the output upon the susceptance of the receiver circuit.*

At a given conductance, g , of the receiver circuit, its output, $P = E_o^2 \alpha^2 g$, is a maximum, if α^2 is a maximum; that is, when —

$$f = \frac{1}{\alpha^2} = (1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2$$

is a minimum.

The condition necessary is —

$$\frac{df}{db} = 0,$$

or, expanding, $x_o (1 + r_o g + x_o b) - r_o (x_o g - r_o b) = 0.$

Hence —

Susceptance of receiver circuit,

$$b = -\frac{x_o}{r_o^2 + x_o^2} = -\frac{x_o}{z_o^2} = -b_o;$$

or

$$b + b_o = 0,$$

that is, if the sum of the susceptances of line and of receiver circuit equals zero.

Substituting this value, we get —

ratio of E.M.Fs. at maximum output,

$$a_1 = \frac{E}{E_o} = \frac{1}{z_o(g + g_o)};$$

maximum output,

$$P_1 = \frac{E_o^2 g^2}{z_o^2 (g + g_o)^2};$$

current,

$$\begin{aligned} I_o &= \frac{E_o Y}{1 + Z_o Y} = \frac{E_o (g - j b_o)}{1 + (r_o - j x_o)(g - j b_o)} \\ &= \frac{E_o (g - j b_o)}{(1 + r_o g - x_o b_o) - j (r_o b_o + x_o g)}; \end{aligned}$$

$$I_o = E_o \sqrt{\frac{g^2 + b_o^2}{(1 + r_o g - x_o b_o)^2 + (r_o b_o + x_o g)^2}};$$

and, expanding,

$$I_o = \frac{E_o \sqrt{g^2 + b_o^2}}{z_o (g + g_o)};$$

phase difference in receiver circuit,

$$\tan \hat{\omega} = \frac{b}{g} = - \frac{b_o}{g};$$

phase difference in generator circuit,

$$\tan \hat{\omega}_o = \frac{x + x_o}{r + r_o} = \frac{b_o (y^2 - y_o^2)}{g_o y^2 + g y_o^2}.$$

62. b.) *Dependence of the output upon the conductance of the receiver circuit.*

At a given susceptance, b , of the receiver circuit, its output, $P = E_o^2 a^2 g$, is a maximum, if —

$$\frac{dP}{dg} = 0,$$

$$\text{or, } \frac{d}{dg} \left(\frac{1}{a^2 g} \right) = \frac{d}{dg} \left(\frac{(1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2}{g} \right) = 0;$$

that is, expanding, —

$$(1 + r_0 g + x_0 b)^2 + (x_0 g - r_0 b)^2 - 2g(r_0 + r_0^2 g + x_0^2 g) = 0;$$

or, expanding, —

$$(b + b_0)^2 = g^2 - g_0^2; \quad g = \sqrt{g_0^2 + (b + b_0)^2}.$$

Substituting this value in the equation for a , page 88, we get —

ratio of E.M.Fs.,

$$\begin{aligned} a_2 &= \frac{1}{z_0 \sqrt{2 \{g_0^2 + (b + b_0)^2 + g_0 \sqrt{g_0^2 + (b + b_0)^2}\}}} \\ &= \frac{1}{z_0 \sqrt{2g(g + g_0)}} = \frac{y_0}{\sqrt{2g(g + g_0)}}; \end{aligned}$$

power,

$$\begin{aligned} P_2 &= \frac{E_0^2 y_0^2}{2(g + g_0)} = \frac{E_0^2 y_0^2}{2 \{g_0 + \sqrt{g_0^2 + (b + b_0)^2}\}} \\ &= \frac{E_0^2}{2 \left\{ r_0 + \sqrt{r_0^2 + \left(x_0 + x \frac{z_0^2}{z^2} \right)^2} \right\}}. \end{aligned}$$

As a function of the susceptance, b , this power becomes a maximum for $dP_2/db = 0$, that is, according to § 61, if —

$$b = -b_0.$$

Substituting this value, we get —

$$\begin{aligned} b &= -b_0, \quad g = g_0, \quad y = y_0, \quad \text{hence: } Y = g + jb = g_0 - jb_0; \\ x &= -x_0, \quad r = r_0, \quad z = z_0, \quad Z = r - jx = r_0 + jx_0; \end{aligned}$$

substituting this value, we get —

$$\text{ratio of E.M.Fs.,} \quad a_m = \frac{y_0}{2g_0} = \frac{z_0}{2r_0};$$

$$\text{power,} \quad P_m = \frac{E_0^2}{4r_0};$$

that is, the same as with a continuous-current circuit; or, in other words, the inductance of the line and of the receiver circuit can be perfectly balanced in its effect upon the output.

63. As a summary, we thus have :

The output delivered over an inductive line of impe-

dance, $Z_o = r_o - jx_o$, into a non-inductive receiver circuit, is a maximum for the resistance, $r = z_o$, or conductance, $g = y_o$, of the receiver circuit, or —

$$P = \frac{1}{2} \frac{E_o^2}{(r_o + z_o)},$$

at the ratio of potentials,

$$\alpha = \frac{1}{\sqrt{2 \left(1 + \frac{r_o}{z_o}\right)}}.$$

With a receiver circuit of constant susceptance, b , the output, as a function of the conductance, g , is a maximum for the conductance, —

$$g = \sqrt{g_o^2 + (b + b_o)^2},$$

and is

$$P = \frac{E_o^2 y_o^2}{2 (g + g_o)},$$

at the ratio of potentials,

$$\alpha = \frac{y_o}{\sqrt{2 g (g + g_o)}}.$$

With a receiver circuit of constant conductance, g , the output, as a function of the reactance, b , is a maximum for the reactance, $b = -b_o$, and is

$$P = \frac{E_o^2 g^2}{z_o^2 (g + g_o)^2},$$

at the ratio of potentials,

$$\alpha = \frac{1}{y_o (g + g_o)}.$$

The maximum output which can be delivered over an inductive line, as a function of the admittance or impedance of the receiver circuit, takes place when $Z = r_o + jx_o$, or $Y = g_o - jb_o$; that is, when the resistance or conductance of a receiver circuit and line are equal, the reactance or susceptance of the receiver circuit and line are equal but of opposite sign, and is, $P = E_o^2 / 4 r_o$, or independent of the reactances, but equal to the output of a continuous-current

circuit of equal line resistance. The ratio of potentials is, in this case, $a = z_o / 2 r_o$, while in a continuous-current circuit it is equal to $\frac{1}{2}$. The efficiency is equal to 50 per cent.

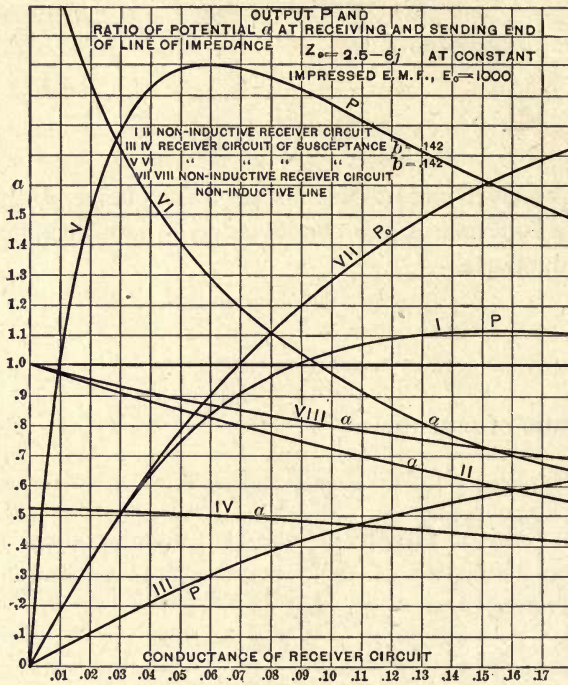


Fig. 58. Variation of the Potential in Line at Different Loads.

64. As an instance, in Fig. 58 are shown, for the constants —

$$E_o = 1000 \text{ volts, and } Z_o = 2.5 - 6j; \text{ that is, for}$$

$$r_o = 2.5 \text{ ohms, } x_o = 6 \text{ ohms, } z_o = 6.5 \text{ ohms,}$$

and with the variable conductances as abscissæ, the values of the —

output, in Curve I., Curve III., and Curve V. ;
 ratio of potentials, in Curve II., Curve IV., and Curve VI. ;

Curves I. and II. refer to a non-inductive receiver circuit ;

Curves III. and IV. refer to a receiver circuit of constant susceptance $b = .142$
 Curves V. and VI. refer to a receiver circuit of constant susceptance' $b = -.142$;
 Curves VII. and VIII. refer to a non-inductive receiver circuit of a non-inductive line.

In Fig. 59, the output is shown as Curve I., and the ratio of potentials as Curve II., for the same line constants, for a constant conductance, $g = .0592$ ohms, and for variable susceptances, b , of the receiver circuit.

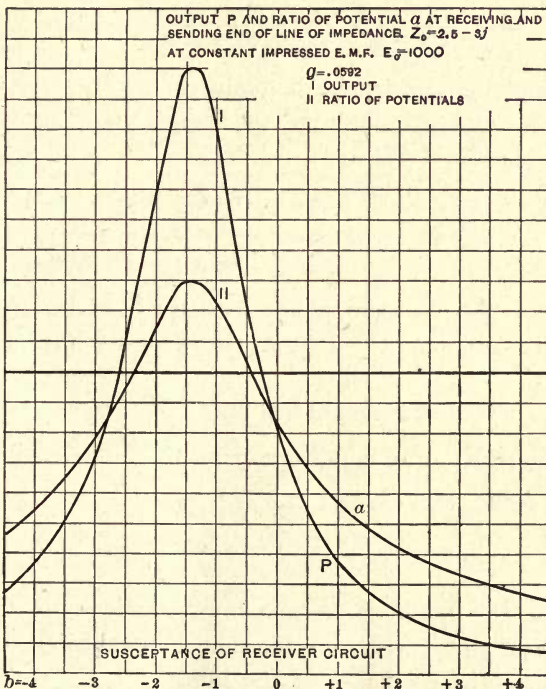


Fig. 59. Variation of Potential in Line at Various Loads.

3.) Maximum Efficiency.

65. The output, for a given conductance, g , of a receiver circuit, is a maximum if $b = -b_0$. This, however, is generally not the condition of maximum efficiency.

The loss of energy in the line is constant if the current is constant; the output of the generator for a given current and given generator E.M.F. is a maximum if the current is in phase with the E.M.F. at the generator terminals. Hence the condition of maximum output at given loss, or of maximum efficiency, is —

$$\tan \hat{\omega}_0 = 0.$$

The current is —

$$\begin{aligned} I_0 &= \frac{E_0 Y}{1 + Z_0 Y} = \frac{E_0 (g + jb)}{1 + (r_0 - jx_0)(g + jb)} \\ &= \frac{E_0 (g + jb)}{(1 + r_0 g + x_0 b) - j(x_0 g - r_0 b)}; \end{aligned}$$

multiplying numerator and denominator by $(1 + r_0 g + x_0 b) + j(x_0 g - r_0 b)$, to eliminate the imaginary quantity from the denominator, we have —

$$I = E_0 \frac{\left(\{g(1 + r_0 g + x_0 b) - b(x_0 g - r_0 b)\} + j \{b(1 + r_0 g + x_0 b) + g(x_0 g - r_0 b)\} \right)}{(1 + r_0 g + x_0 b)^2 + (x_0 g - r_0 b)^2}.$$

The current, I_0 , is in phase with the E.M.F., E_0 , if its quadrature component — that is, the imaginary term — disappears, or

$$b(1 + r_0 g + x_0 b) + g(x_0 g - r_0 b) = 0.$$

This, therefore, is the condition of maximum efficiency.

Expanding, we have,

$$x_0 = -\frac{b}{g^2 + b^2} = -x, \text{ or: } x = -x_0.$$

Hence, the condition of maximum efficiency is, that the reactance of the receiver circuit shall be equal, but of opposite sign, to the reactance of the line.

Substituting $x = -x_0$, we have, ratio of E.M.Fs.,

$$a = \frac{E}{E_0} = \frac{z}{(r + r_0)} = \frac{\sqrt{r^2 + x_0^2}}{(r + r_0)};$$

power,

$$P = E_0^2 g a^2 = \frac{E_0^2 r}{(r + r_0)^2},$$

and depending upon the resistance only, and not upon the reactance.

This power is a maximum if $g = g_o$, as shown before; hence, substituting $g = g_o, r = r_o$,

maximum power at maximum efficiency, $P_m = \frac{E_o^2}{4 r_o}$,

at a ratio of potentials, $a_m = \frac{z_o}{2 r_o}$,

or the same result as in § 62.

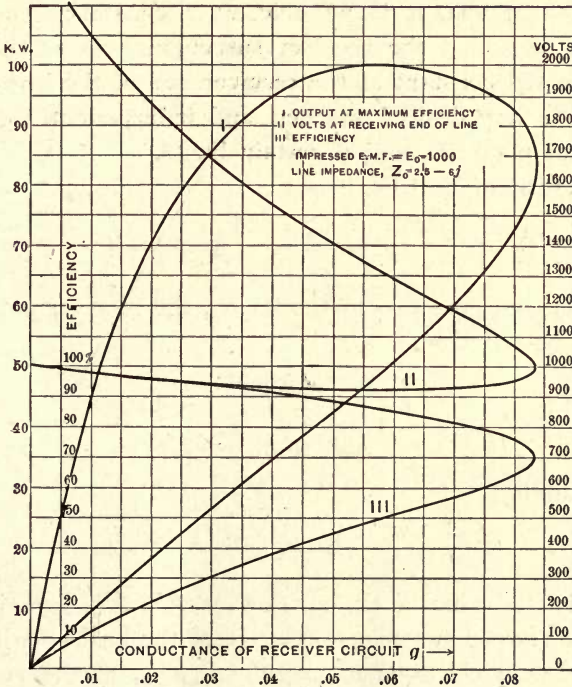


Fig. 60. Load Characteristic of Transmission Line.

In Fig. 60 are shown, for the constants —

$E_o = 1,000$ volts,

$Z_o = 2.5 - 6j; r_o = 2.5$ ohms, $x_o = 6$ ohms, $z_o = 6.5$ ohms,

and with the variable conductances, g , of the receiver circuit as abscissæ, the —

$$\begin{aligned} &\text{Output at maximum efficiency,} && \text{(Curve I.) ;} \\ &\text{Volts at receiving end of line,} && \text{(Curve II.) ;} \\ &\text{Efficiency} = \frac{r}{r + r_o}, && \text{(Curve III.)} \end{aligned}$$

4.) *Control of Receiver Voltage by Shunted Susceptance.*

66. By varying the susceptance of the receiver circuit, the potential at the receiver terminals is varied greatly. Therefore, since the susceptance of the receiver circuit can be varied at will, it is possible, at a constant generator E.M.F., to adjust the receiver susceptance so as to keep the potential constant at the receiver end of the line, or to vary it in any desired manner, and independently of the generator potential, within certain limits.

The ratio of E.M.Fs. is —

$$a = \frac{E}{E_o} = \frac{1}{\sqrt{(1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2}}.$$

If at constant generator potential E_o , the receiver potential E shall be constant,

$$a = \text{constant ;}$$

hence,

$$(1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2 = \frac{1}{a^2};$$

or, expanding,

$$b = -b_o + \sqrt{\left(\frac{y_o}{a}\right)^2 - (g + g_o)^2},$$

which is the value of the susceptance, b , as a function of the receiver conductance, — that is, of the load, — which is required to yield constant potential, aE_o , at the receiver circuit.

For increasing g , that is, for increasing load, a point is reached, where, in the expression —

$$b = -b_o + \sqrt{\left(\frac{y_o}{a}\right)^2 - (g + g_o)^2},$$

the term under the root becomes imaginary, and it thus becomes impossible to maintain a constant potential, aE_o . Therefore, the maximum output which can be transmitted at potential aE , is given by the expression —

$$\sqrt{\left(\frac{y_o}{a}\right)^2 - (g + g_o)^2} = 0;$$

hence $b = -o_o$, the susceptance of receiver circuit,
and $g = -g_o + \frac{y_o}{a}$, the conductance of receiver circuit;

$$P = E_o^2 g a^2 \\ = a^2 E_o^2 \left(\frac{y_o}{a} - g_o\right), \text{ the output.}$$

67. If $a = 1$, that is, if the voltage at the receiver circuit equals the generator potential —

$$g = y_o - g_o; \\ P = a^2 E_o^2 (y_o - g_o).$$

If $a = 1$ when $g = 0$, $b = 0$
when $g > 0$, $b < 0$;

if $a > 1$ when $g = 0$, or $g > 0$, $b < 0$,
that is, condensance;

if $a < 1$ when $g = 0$, $b > 0$,
when $g = -g_o + \sqrt{\left(\frac{y_o}{a}\right)^2 - b_o^2}$, $b = 0$;
when $g > -g_o + \sqrt{\left(\frac{y_o}{a}\right)^2 - b_o^2}$, $b < 0$,

or, in other words, if $a < 1$, the phase difference in the main line must change from lag to lead with increasing load.

68. The value of a giving the maximum possible output in a receiver circuit, is determined by $dP / da = 0$;

expanding :

$$2 a \left(\frac{y_o}{a} - g_o\right) - \frac{a^2 y_o}{a^2} = 0;$$

hence,

$$y_o = 2 a g_o,$$

and

$$a = \frac{y_o}{2 g_o} = \frac{1}{2 \sqrt{g_o r_o}} = \frac{z_o}{2 r_o};$$

the maximum output is determined by —

$$g = -g_0 + \frac{y_0}{a} = g_0;$$

and is,

$$P = \frac{E_0^2}{4r}.$$

From:

$$a = \frac{y_0}{2g_0} = \frac{z_0}{2r_0},$$

the line reactance, x_0 , can be found, which delivers a maximum output into the receiver circuit at the ratio of potentials, a ,

and

$$z_0 = 2r_0 a,$$

$$x_0 = r_0 \sqrt{4a^2 - 1};$$

for $a = 1$,

$$z_0 = 2r_0;$$

$$x_0 = r_0 \sqrt{3}.$$

If, therefore, the line impedance equals $2a$ times the line resistance, the maximum output, $P = E_0^2/4r_0$, is transmitted into the receiver circuit at the ratio of potentials, a .

If $z_0 = 2r_0$, or $x_0 = r_0 \sqrt{3}$, the maximum output, $P = E_0^2/4r_0$, can be supplied to the receiver circuit, without change of potential at the receiver terminals.

Obviously, in an analogous manner, the law of variation of the susceptance of the receiver circuit can be found which is required to increase the receiver voltage proportionally to the load; or, still more generally, — to cause any desired variation of the potential at the receiver circuit independently of any variation of the generator potential, as, for instance, to keep the potential of a receiver circuit constant, even if the generator potential fluctuates widely.

69. In Figs. 61, 62, and 63, are shown, with the output, $P = E_0^2 g a^2$, as abscissæ, and a constant impressed E.M.F., $E_0 = 1,000$ volts, and a constant line impedance, $Z_0 = 2.5 - 6j$, or, $r_0 = 2.5$ ohms, $x_0 = 6$ ohms, $z = 6.5$ ohms, the following values:

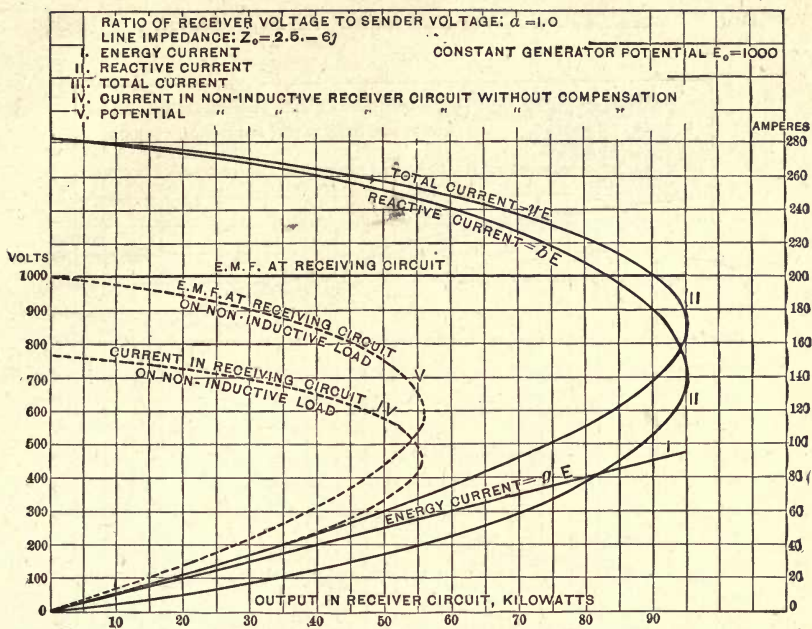


Fig. 61. Variation of Voltage Transmission Lines.

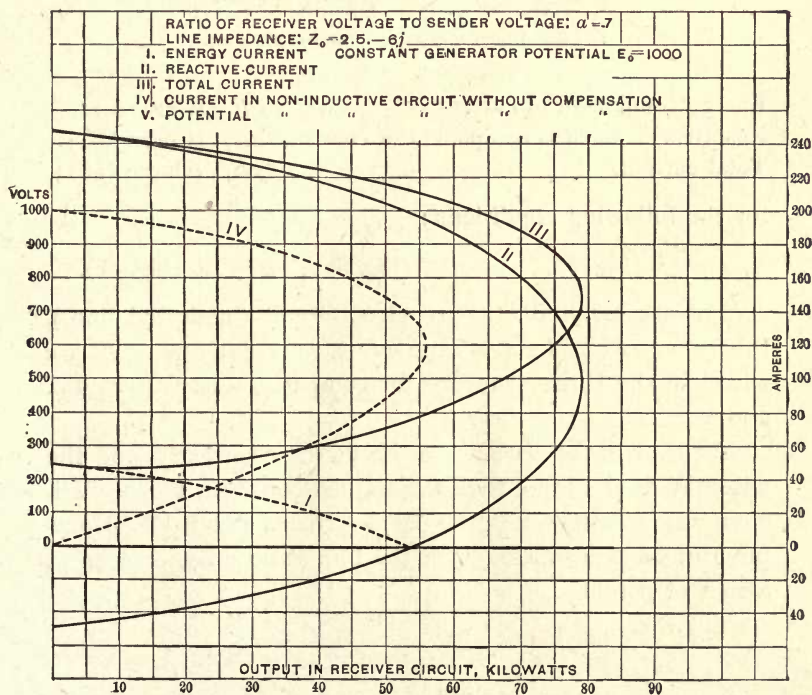


Fig. 62. Variation of Voltage Transmission Lines.

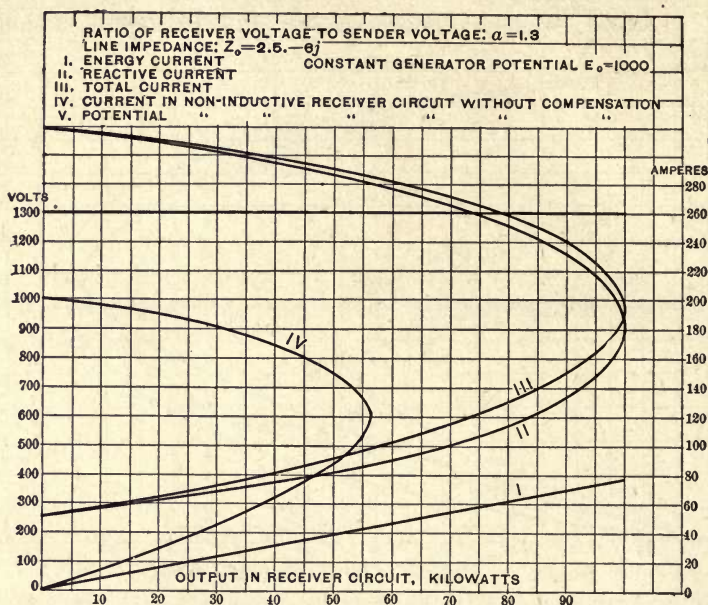


Fig. 63. Variation of Voltage Transmission Lines.

Energy component of current, gE , (Curve I.);
 Reactive, or wattless component of current, bE , (Curve II.);
 Total current, yE , (Curve III.);

for the following conditions :

$a = 1.0$ (Fig. 58) ; $a = .7$ (Fig. 59) ; $a = 1.3$ (Fig. 60).

For the non-inductive receiver circuit (in dotted lines), the curve of E.M.F., E , and of the current, $I = gE$, are added in the three diagrams for comparison, as Curves IV. and V.

As shown, the output can be increased greatly, and the potential at the same time maintained constant, by the judicious use of shunted reactance, so that a much larger output can be transmitted over the line at no drop, or even at a rise, of potential.

5.) *Maximum Rise of Potential at Receiver Circuit.*

70. Since, under certain circumstances, the potential at the receiver circuit may be higher than at the generator, it is of interest to determine what is the maximum value of potential, E , that can be produced at the receiver circuit with a given generator potential, E_o .

The condition is that

$$a = \text{maximum or } \frac{1}{a^2} = \text{minimum};$$

that is,

$$\frac{d(1/a^2)}{dg} = 0, \quad \frac{d(1/a^2)}{db} = 0;$$

substituting,

$$\frac{1}{a^2} = (1 + r_o g + x_o b)^2 + (x_o g - r_o b)^2,$$

and expanding, we get,

$$\frac{d(1/a^2)}{dg} = 0; \quad g = -\frac{r_o}{z_o^2};$$

— a value which is impossible, since neither r_o nor g can be negative. The next possible value is $g = 0$, — a wattless circuit.

Substituting this value, we get,

$$\frac{1}{a^2} = (1 + x_o b)^2 + r_o^2 b^2;$$

and by substituting, in

$$\frac{d(1/a^2)}{db} = 0, \quad b = -\frac{x_o}{z_o^2} = -b_o,$$

$$b + b_o = 0;$$

that is, the sum of the susceptances = 0, or the condition of resonance is present.

Substituting,

$$b = -b_o,$$

we have

$$a = \frac{1}{\sqrt{r_o g_o}} = \frac{z_o}{r_o} = \frac{y_o}{b_o}.$$

The current in this case is,

$$I = E_o g_o = \frac{E_o}{r_o},$$

or the same as if the line resistance were short-circuited without any inductance.

This is the condition of perfect resonance, with current and E.M.F. in phase.

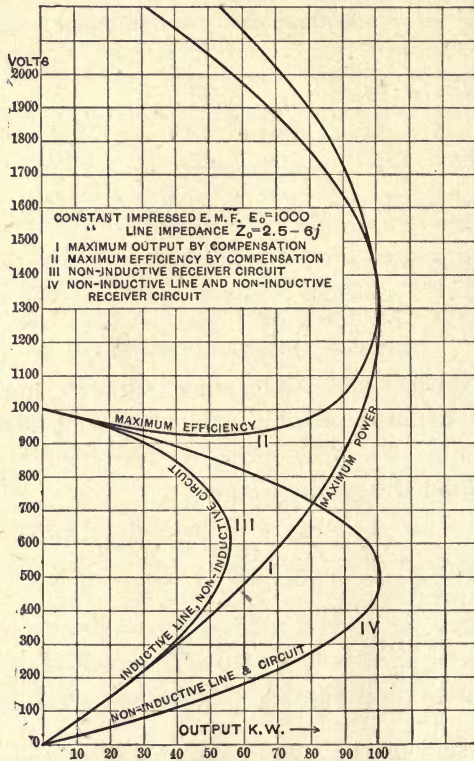


Fig. 64. Efficiency and Output of Transmission Line.

71. As summary to this chapter, in Fig. 64 are plotted, for a constant generator E.M.F., $E_o = 1000$ volts, and a line impedance, $Z_o = 2.5 - 6j$, or, $r_o = 2.5$ ohms, $x_o = 6$ ohms, $z_o = 6.5$ ohms; and with the receiver output as

abscissæ and the receiver voltages as ordinates, curves representing —

- the condition of maximum output, (Curve I.);
- the condition of maximum efficiency, (Curve II.);
- the condition $b = 0$, or a non-inductive receiver circuit, (Curve III.);
- the condition $b = 0$, $b_0 = 0$, or a non-inductive line and non-inductive receiver circuit, or a non-inductive receiver circuit and a non-inductive line.

In conclusion, it may be remarked here that of the sources of susceptance, or reactance,

- a choking coil or reactive coil corresponds to an inductance;
- a condenser corresponds to a condensance;
- a polarization cell corresponds to a condensance;
- a synchronizing alternator (motor or generator) corresponds to an inductance or a condensance, at will;
- an induction motor or generator corresponds to an inductance or condensance, at will.

The choking coil and the polarization cell are specially suited for series reactance, and the condenser and synchronizer for shunted susceptance.

CHAPTER X.

EFFECTIVE RESISTANCE AND REACTANCE.

72. The resistance of an electric circuit is determined :—

1.) By direct comparison with a known resistance (Wheatstone bridge method, etc.).

This method gives what may be called the true ohmic resistance of the circuit.

2.) By the ratio :

$$\frac{\text{Volts consumed in circuit}}{\text{Amperes in circuit}}$$

In an alternating-current circuit, this method gives, not the resistance of the circuit, but the impedance,

$$z = \sqrt{r^2 + x^2}.$$

3.) By the ratio :

$$r = \frac{\text{Power consumed}}{(\text{Current})^2} = \frac{(\text{E.M.F.})^2}{\text{Power consumed}};$$

where, however, the "power" and the "E.M.F." do not include the work done by the circuit, and the counter E.M.Fs. representing it, as, for instance, in the case of the counter E.M.F. of a motor.

In alternating-current circuits, this value of resistance is the energy coefficient of the E.M.F.,

$$r = \frac{\text{Energy component of E.M.F.}}{\text{Total current}}.$$

It is called the *effective resistance* of the circuit, since it represents the effect, or power, expended by the circuit. The energy coefficient of current,

$$g = \frac{\text{Energy component of current}}{\text{Total E.M.F.}},$$

is called the *effective conductance* of the circuit.

In the same way, the value,

$$x = \frac{\text{Wattless component of E.M.F.}}{\text{Total current}},$$

is the *effective reactance*, and

$$b = \frac{\text{Wattless component of current}}{\text{Total E.M.F.}},$$

is the *effective susceptance* of the circuit.

While the true ohmic resistance represents the expenditure of energy as heat inside of the electric conductor by a current of uniform density, the effective resistance represents the total expenditure of energy.

Since, in an alternating-current circuit in general, energy is expended not only in the conductor, but also outside of it, through hysteresis, secondary currents, etc., the effective resistance frequently differs from the true ohmic resistance in such way as to represent a larger expenditure of energy.

In dealing with alternating-current circuits, it is necessary, therefore, to substitute everywhere the values "effective resistance," "effective reactance," "effective conductance," and "effective susceptance," to make the calculation applicable to general alternating-current circuits, such as ferric inductances, etc.

While the true ohmic resistance is a constant of the circuit, depending only upon the temperature, but not upon the E.M.F., etc., the effective resistance and effective reactance are, in general, not constants, but depend upon the E.M.F., current, etc. This dependence is the cause of most of the difficulties met in dealing analytically with alternating-current circuits containing iron.

73. The foremost sources of energy loss in alternating-current circuits, outside of the true ohmic resistance loss, are as follows:

- 1.) Molecular friction, as,
 - a.) Magnetic hysteresis;
 - b.) Dielectric hysteresis.

- 2.) Primary electric currents, as,
 - a.) Leakage or escape of current through the insulation, brush discharge ;
 - b.) Eddy currents in the conductor or unequal current distribution.
- 3.) Secondary or induced currents, as,
 - a.) Eddy or Foucault currents in surrounding magnetic materials ;
 - b.) Eddy or Foucault currents in surrounding conducting materials ;
 - c.) Secondary currents of mutual inductance in neighboring circuits.
- 4.) Induced electric charges, electrostatic influence.

While all these losses can be included in the terms effective resistance, etc., only the magnetic hysteresis and the eddy currents in the iron will form the subject of what follows.

Magnetic Hysteresis.

74. In an alternating-current circuit surrounded by iron or other magnetic material, energy is expended outside of the conductor in the iron, by a kind of molecular friction, which, when the energy is supplied electrically, appears as magnetic hysteresis, and is caused by the cyclic reversals of magnetic flux in the iron in the alternating magnetic field of force.

To examine this phenomenon, first a circuit may be considered, of very high inductance, but negligible true ohmic resistance ; that is, a circuit entirely surrounded by iron, as, for instance, the primary circuit of an alternating-current transformer with open secondary circuit.

The wave of current produces in the iron an alternating magnetic flux which induces in the electric circuit an E.M.F.,—the counter E.M.F. of self-induction. If the ohmic resistance is negligible, the counter E.M.F. equals the impressed E.M.F. ; hence, if the impressed E.M.F. is

a sine wave, the counter E.M.F., and, therefore, the magnetic flux which induces the counter E.M.F. must follow sine waves also. The alternating wave of current is not a sine wave in this case, but is distorted by hysteresis. It is possible, however, to plot the current wave in this case from the hysteretic cycle of magnetic flux.

From the number of turns, n , of the electric circuit, the effective counter E.M.F., E , and the frequency, N , of the current, the maximum magnetic flux, Φ , is found by the formula:

$$E = \sqrt{2} \pi n N \Phi 10^{-8};$$

hence,

$$\Phi = \frac{E 10^8}{\sqrt{2} \pi n N}.$$

A maximum flux, Φ , and magnetic cross-section, S , give the maximum magnetic induction, $\mathfrak{B} = \Phi / S$.

If the magnetic induction varies periodically between $+\mathfrak{B}$ and $-\mathfrak{B}$, the M.M.F. varies between the corresponding values $+\mathfrak{F}$ and $-\mathfrak{F}$, and describes a looped curve, the cycle of hysteresis.

If the ordinates are given in lines of magnetic force, the abscissæ in tens of ampere-turns, then the area of the loop equals the energy consumed by hysteresis in ergs per cycle.

From the hysteretic loop the instantaneous value of M.M.F. is found, corresponding to an instantaneous value of magnetic flux, that is, of induced E.M.F.; and from the M.M.F., \mathfrak{F} , in ampere-turns per unit length of magnetic circuit, the length, l , of the magnetic circuit, and the number of turns, n , of the electric circuit, are found the instantaneous values of current, i , corresponding to a M.M.F., \mathfrak{F} , that is, as magnetic induction \mathfrak{B} , and thus induced E.M.F. e , as:

$$i = \frac{\mathfrak{F} l}{n}.$$

75. In Fig. 65, four magnetic cycles are plotted, with maximum values of magnetic inductions, $\mathfrak{B} = 2,000, 6,000, 10,000$, and $16,000$, and corresponding maximum M.M.Fs.,

$\mathcal{F} = 1.8, 2.8, 4.3, 20.0$. They show the well-known hysteretic loop, which becomes pointed when magnetic saturation is approached.

These magnetic cycles correspond to average good sheet iron or sheet steel, having a hysteretic coefficient, $\eta = .0033$, and are given with ampere-turns per cm as abscissæ, and kilo-lines of magnetic force as ordinates.

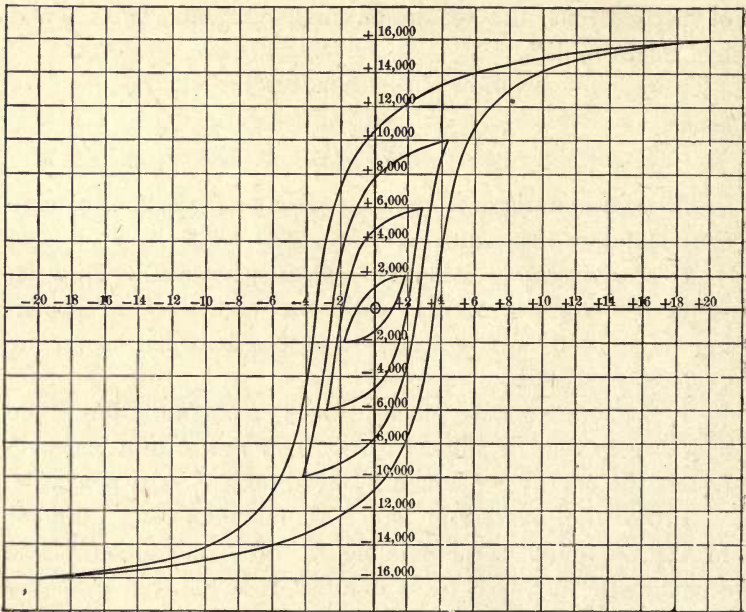
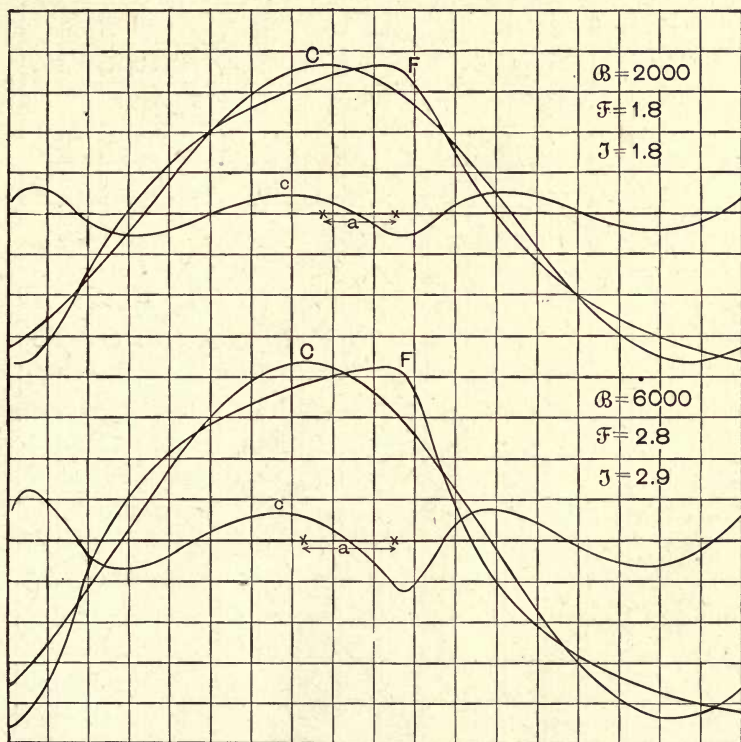


Fig. 65. Hysteretic Cycle of Sheet Iron.

In Figs. 66, 67, 68, and 69, the sine curve of magnetic induction as derived from the induced E.M.F. is plotted in dotted lines. For the different values of magnetic induction of this sine curve, the corresponding values of M.M.F., hence of current, are taken from Fig. 66, and plotted, giving thus the exciting current required to produce the sine wave of magnetism; that is, the wave of current which a sine wave of impressed E.M.F. will send through the circuit.

As shown in Figs. 66, 67, 68, and 69, these waves of alternating current are not sine waves, but are distorted by the superposition of higher harmonics, and are complex harmonic waves. They reach their maximum value at the same time with the maximum of magnetism, that is, 90°

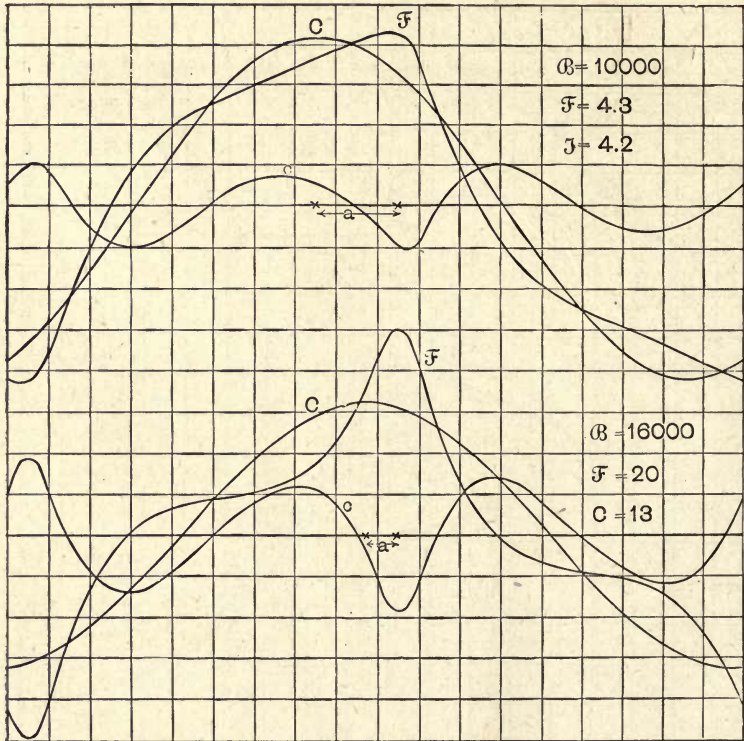


Figs. 66 and 67. Distortion of Current Wave by Hysteresis.

ahead of the maximum induced E.M.F., and hence about 90° behind the maximum impressed E.M.F., but pass the zero line considerably ahead of the zero value of magnetism, or 42° , 52° , 50° , and 41° , respectively.

The general character of these current waves is, that the maximum point of the wave coincides in time with the max-

imum point of the sine wave of magnetism ; but the current wave is bulged out greatly at the rising, and hollowed in at the decreasing, side. With increasing magnetization, the maximum of the current wave becomes more pointed, as shown by the curve of Fig. 68, for $\mathcal{B} = 10,000$; and at still



Figs. 68 and 69. Distortion of Current Wave by Hysteresis.

higher saturation a peak is formed at the maximum point, as in the curve of Fig. 69, for $\mathcal{B} = 16,000$. This is the case when the curve of magnetization remains within the range of magnetic saturation, since in the proximity of saturation the current near the maximum point of magnetization has to rise abnormally to cause even a small increase of magnetization.

The four curves, Figs. 66, 67, 68, and 69, are not drawn to the same scale. The maximum values of M.M.F., corresponding to the maximum values of magnetic induction, $\mathfrak{B} = 2,000, 6,000, 10,000,$ and $16,000$ lines of force per cm^2 , are $\mathfrak{F} = 1.8, 2.8, 4.3,$ and 20.0 ampere-turns per cm. In the different diagrams these are represented in the ratio of $8:6:4:1$, in order to bring the curves of current to approximately the same height.

The M.M.F., in C.G.S. units, is

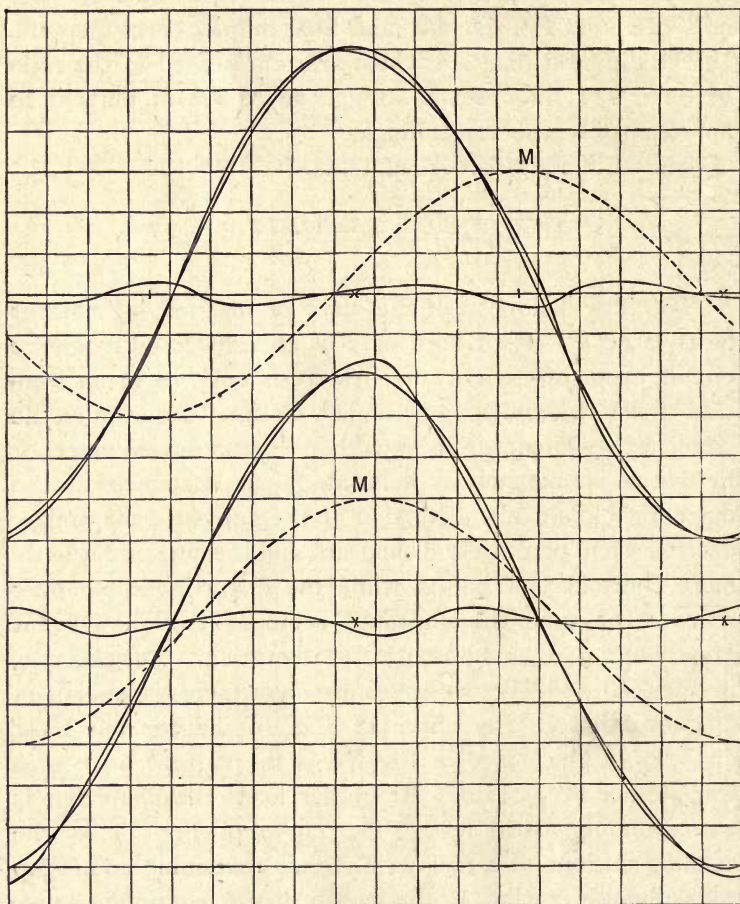
$$\mathfrak{F}_c = \frac{4\pi}{10} \mathfrak{F} = 1.257 \mathfrak{F}.$$

76. The distortion of the wave of magnetizing current is as large as shown here only in an iron-closed magnetic circuit expending energy by hysteresis only, as in an iron-clad transformer on open secondary circuit. As soon as the circuit expends energy in any other way, as in resistance, or by mutual inductance, or if an air-gap is introduced in the magnetic circuit, the distortion of the current wave rapidly decreases and practically disappears, and the current becomes more sinusoidal. That is, while the distorting component remains the same, the sinusoidal component of the current greatly increases, and obscures the distortion. For example, in Figs. 70 and 71, two waves are shown, corresponding in magnetization to the curve of Fig. 67, as the one most distorted. The curve in Fig. 70 is the current wave of a transformer at $\frac{1}{10}$ load. At higher loads the distortion is correspondingly still less. The curve of Fig. 71 is the exciting current of a magnetic circuit containing an air-gap whose length equals $\frac{1}{40}$ the length of the magnetic circuit. These two curves are drawn to $\frac{1}{3}$ the size of the curve in Fig. 67. As shown, both curves are practically sine waves.

77. The distorted wave of current can be resolved into two components: *A true sine wave of equal effective intensity and equal power to the distorted wave, called the equivalent*

sine wave, and a *wattless higher harmonic*, consisting chiefly of a term of triple frequency.

In Figs. 66 to 71 are shown, in full lines, the equiva-



Figs. 70 and 71. Distortion of Current Wave by Hysteresis.

lent sine waves and the wattless complex higher harmonics, which together form the distorted current wave. The equivalent sine wave of M.M.F. or of current, in Figs. 66 to 69, leads the magnetism by 34° , 44° , 38° , and $15^\circ.5$,

respectively. In Fig. 71 the equivalent sine wave almost coincides with the distorted curve, and leads the magnetism by only 9° .

It is interesting to note, that even in the greatly distorted curves of Figs. 66 to 68, the maximum value of the equivalent sine wave is nearly the same as the maximum value of the original distorted wave, of M.M.F., so long as magnetic saturation is not approached, being 1.8, 2.9, and 4.2, respectively, against 1.8, 2.8, and 4.3, the maximum values of the distorted curve. Since, by the definition, the effective value of the equivalent sine wave is the same as that of the distorted wave, it follows, that the distorted wave of exciting current shares with the sine wave the feature, that the maximum value and the effective value have the ratio of $\sqrt{2} \div 1$. Hence, below saturation, the maximum value of the distorted curve can be calculated from the effective value — which is given by the reading of an electro-dynamometer — by using the same ratio that applies to a true sine wave, and the magnetic characteristic can thus be determined by means of alternating currents, with sufficient exactness, by the electro-dynamometer method.

78. In Fig. 72 is shown the true magnetic characteristic of a sample of good average sheet iron, as found by the method of slow reversals with the magnetometer; for comparison there is shown in dotted lines the same characteristic, as determined with alternating currents by the electro-dynamometer, with ampere-turns per cm as ordinates, and magnetic inductions as abscissæ. As represented, the two curves practically coincide up to $\mathfrak{B} = 10,000$ to 14,000; that is, up to the highest inductions practicable in alternating-current apparatus. For higher saturations, the curves rapidly diverge, and the electro-dynamometer curve shows comparatively small M.M.F.s. producing apparently very high magnetizations.

The same Fig. 72 gives the curve of hysteretic loss, in ergs per cm^3 and cycle, as ordinates, and magnetic inductions as abscissæ.

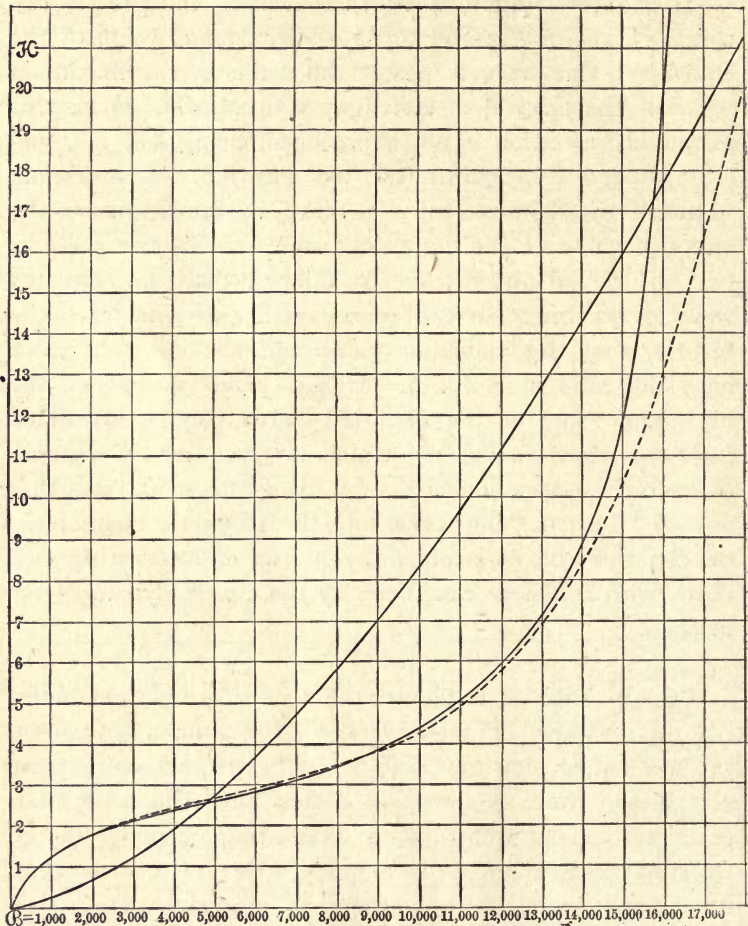


Fig. 72. Magnetization and Hysteresis Curve.

The electro-dynamometer method of determining the magnetic characteristic is preferable for use with alternating-current apparatus, since it is not affected by the phenomenon of magnetic "creeping," which, especially at

low densities, brings in the magnetometer tests the magnetism usually very much higher, or the M.M.F. lower, than found in practice in alternating-current apparatus.

So far as current strength and energy consumption are concerned, the distorted wave can be replaced by the equivalent sine wave, and the higher harmonic neglected.

All the measurements of alternating currents, with the single exception of instantaneous readings, yield the equivalent sine wave only, and suppress the higher harmonic; since all measuring instruments give either the mean square of the current wave, or the mean product of instantaneous values of current and E.M.F., which, by definition, are the same in the equivalent sine wave as in the distorted wave.

Hence, in all practical applications, it is permissible to neglect the higher harmonic altogether, and replace the distorted wave by its equivalent sine wave, keeping in mind, however, the existence of a higher harmonic as a possible disturbing factor which may become noticeable in those very rare cases where the frequency of the higher harmonic is near the frequency of resonance of the circuit.

79. The equivalent sine wave of exciting current leads the sine wave of magnetism by an angle α , which is called the *angle of hysteretic advance of phase*. Hence the current lags behind the E.M.F. by $\sphericalangle 90^\circ - \alpha$, and the power is therefore,

$$P = IE \cos (90^\circ - \alpha) = IE \sin \alpha.$$

Thus the exciting current, I , consists of an energy component, $I \sin \alpha$, which is called the *hysteretic energy current*, and a wattless component, $I \cos \alpha$, which is called the *magnetizing current*. Or, conversely, the E.M.F. consists of an energy component, $E \sin \alpha$, the *hysteretic energy E.M.F.*, and a wattless component, $E \cos \alpha$, the *E.M.F. of self-induction*.

Denoting the absolute value of the impedance of the

circuit, E/I , by z , — where z is determined by the magnetic characteristic of the iron, and the shape of the magnetic and electric circuits, — the impedance is represented, in phase and intensity, by the symbolic expression,

$$Z = r - jx = z \sin a - jz \cos a;$$

and the admittance by,

$$Y = g + jb = \frac{1}{z} \sin a + j \frac{1}{z} \cos a = y \sin a + jy \cos a.$$

The quantities, z , r , x , and y , g , b , are, however, not constants as in the case of the circuit without iron, but depend upon the intensity of magnetization, \mathfrak{B} , — that is, upon the E.M.F.

This dependence complicates the investigation of circuits containing iron.

In a circuit entirely inclosed by iron, a is quite considerable, ranging from 30° to 50° for values below saturation. Hence, even with negligible true ohmic resistance, no great lag can be produced in ironclad alternating-current circuits.

80. The loss of energy by hysteresis due to molecular friction is, with sufficient exactness, proportional to the 1.6th power of magnetic induction \mathfrak{B} . Hence it can be expressed by the formula:

$$W_H = \eta \mathfrak{B}^{1.6}$$

where —

W_H = loss of energy per cycle, in ergs or (C.G.S.) units ($= 10^{-7}$ Joules) per cm^3 ,

\mathfrak{B} = maximum magnetic induction, in lines of force per cm^2 , and

η = the *coefficient of hysteresis*.

This I found to vary in iron from .00124 to .0055. As a fair mean, .0033 can be accepted for good average annealed sheet iron or sheet steel. In gray cast iron, η averages .013; it varies from .0032 to .028 in cast steel, according to the chemical or physical constitution; and reaches values as high as .08 in hardened steel (tungsten and manganese

steel). Soft nickel and cobalt have about the same coefficient of hysteresis as gray cast iron; in magnetite I found $\eta = .023$.

In the curves of Fig. 62 to 69, $\eta = .0033$.

At the frequency, N , the loss of power in the volume, V , is, by this formula, —

$$P = \eta NV \Phi^{1.6} 10^{-7} \text{ watts}$$

$$= \eta NV \left(\frac{\Phi}{S} \right)^{1.6} 10^{-7} \text{ watts,}$$

where S is the cross-section of the total magnetic flux, Φ .

The maximum magnetic flux, Φ , depends upon the counter E.M.F. of self-induction,

$$E = \sqrt{2} \pi N n \Phi 10^{-8},$$

or

$$\Phi = \frac{E 10^8}{\sqrt{2} \pi N n},$$

where n = number of turns of the electric circuit.

Substituting this in the value of the power, P , and canceling, we get, —

$$P = \eta \frac{E^{1.6}}{N^{.6}} \frac{V 10^{5.8}}{2^{.8} \pi^{1.6} S^{1.6} n^{1.6}} = 58 \eta \frac{E^{1.6}}{N^{.6}} \frac{V 10^8}{S^{1.6} n^{1.6}};$$

or $P = \frac{AE^{1.6}}{N^{.6}}$, where $A = \eta \frac{V 10^{5.8}}{2^{.8} \pi^{1.6} S^{1.6} n^{1.6}} = 58 \eta \frac{V 10^8}{S^{1.6} n^{1.6}};$

or, substituting $\eta = .0033$, we have $A = 191.4 \frac{V}{S^{1.6} n^{1.6}};$

or, substituting $V = SL$, where L = length of magnetic circuit,

$$A = \frac{\eta L 10^{5.8}}{2^{.8} \pi^{1.6} S^{.6} n^{1.6}} = \frac{58 \eta L 10^8}{S^{.6} n^{1.6}} = 191.4 \frac{L}{S^{.6} n^{1.6}};$$

and $P = \frac{58 \eta E^{1.6} L 10^8}{N^{.6} S^{.6} n^{1.6}} = \frac{191.4 E^{1.6} L}{N^{.6} S^{.6} n^{1.6}}.$

In Figs. 73, 74, and 75, is shown a curve of hysteretic loss, with the loss of power as abscissæ, and

in curve 73, with the E.M.F., E , as ordinates, for $L = 1$, $S = 1$, $N = 100$, and $n = 100$;

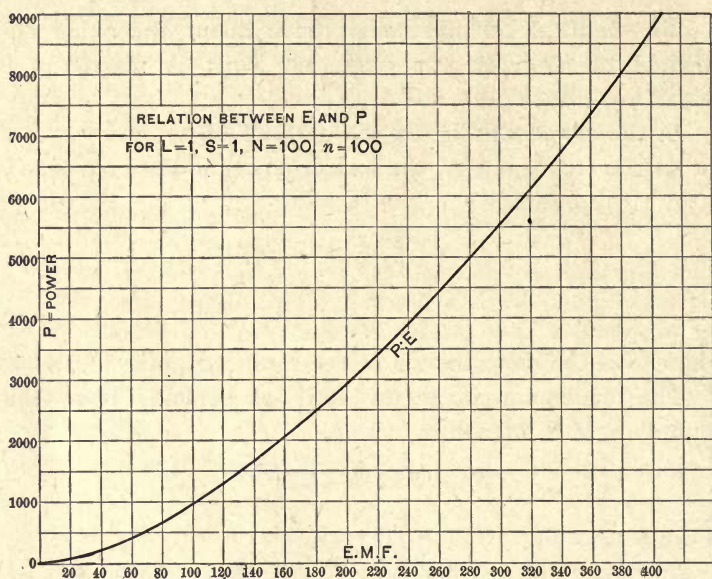


Fig. 73. Hysteresis Loss as Function of E. M. F.

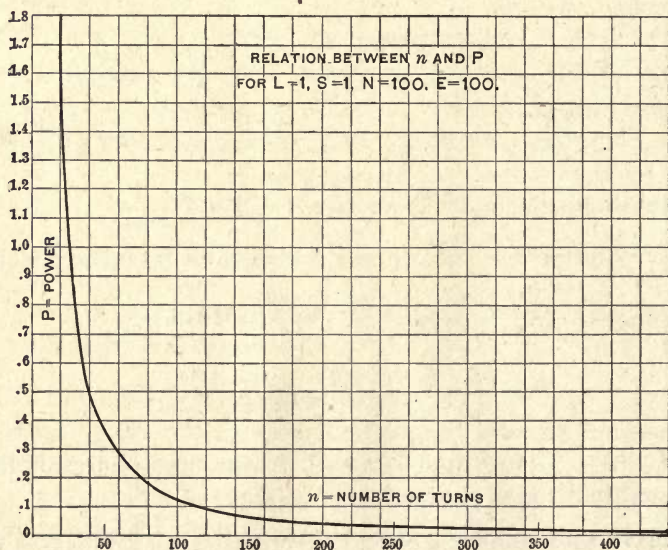


Fig. 74. Hysteresis Loss as Function of Number of Turns.

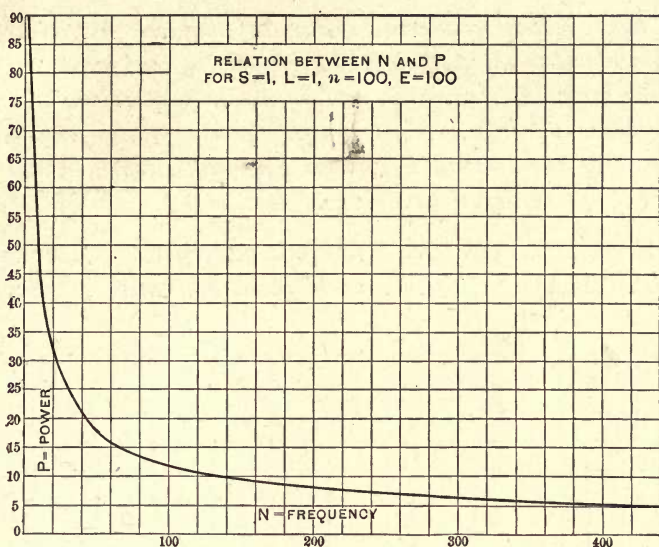


Fig. 75. Hysteresis Loss as Function of Cycles.

in curve 74, with the number of turns as ordinates, for $L = 1, S = 1, N = 100,$ and $E = 100$;

in curve 75, with the frequency, $N,$ or the cross-section, $S,$ as ordinates, for $L = 1, n = 100,$ and $E = 100.$

As shown, the hysteretic loss is proportional to the 1.6th power of the E.M.F., inversely proportional to the 1.6th power of the number of turns, and inversely proportional to the .6th power of frequency, and of cross-section.

81. If $g =$ effective conductance, the energy component of a current is $I = Eg,$ and the energy consumed in a conductance, $g,$ is $P = IE = E^2g.$

Since, however :

$$P = A \frac{E^{1.6}}{N^{.6}}, \text{ we have } A \frac{E^{1.6}}{N^{.6}} = E^2g;$$

or

$$g = \frac{A}{N^{.6}E^{.4}} = \frac{58 \eta L 10^3}{E^{.4} N^{.6} S^{.6} n^{1.6}} = 191.4 \frac{L}{E^{.4} N^{.6} S^{.6} n^{1.6}}.$$

From this we have the following deduction :

The effective conductance due to magnetic hysteresis is proportional to the coefficient of hysteresis, η , and to the length of the magnetic circuit, L , and inversely proportional to the 4th power of the E.M.F., to the 6th power of the frequency, N , and of the cross-section of the magnetic circuit, S , and to the 1.6th power of the number of turns, n .

Hence, the effective hysteretic conductance increases with decreasing E.M.F., and decreases with increasing

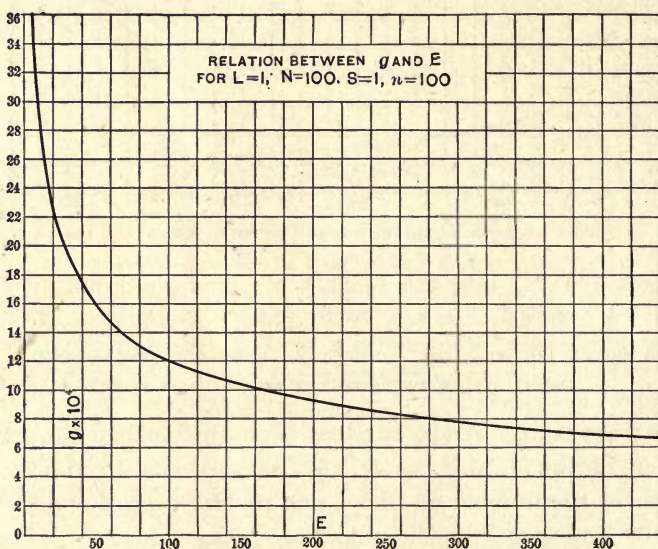


Fig. 76. Hysteresis Conductance as Function of E.M.F.

E.M.F.; it varies, however, much slower than the E.M.F., so that, if the hysteretic conductance represents only a part of the total energy consumption, it can, within a limited range of variation—as, for instance, in constant potential transformers—be assumed as constant without serious error.

In Figs. 76, 77, and 78, the hysteretic conductance, g , is plotted, for $L = 1$, $E = 100$, $N = 100$, $S = 1$, and $n = 100$, respectively, with the conductance, g , as ordinates, and with

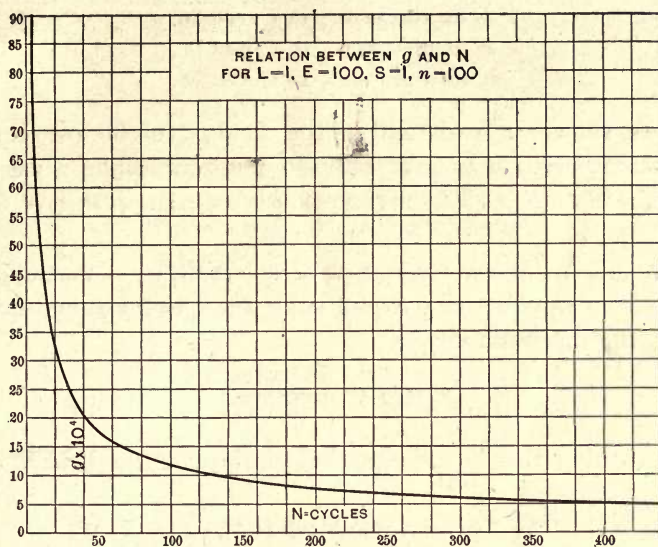


Fig. 77. Hysteresis Conductance as Function of Cycles.

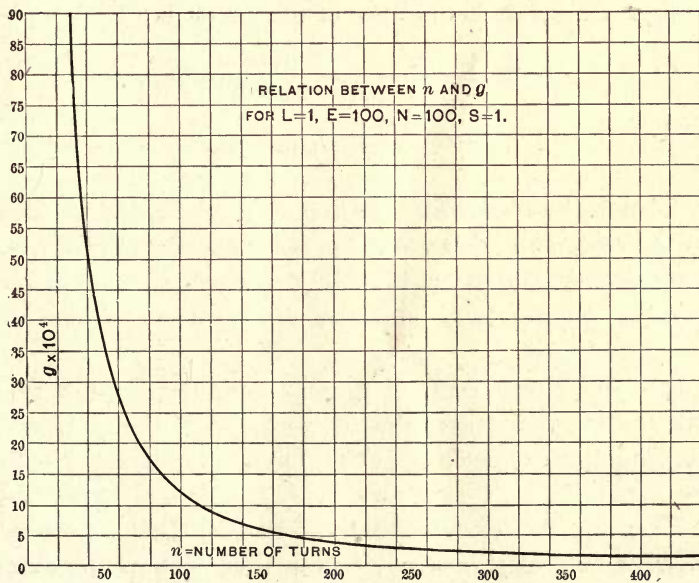


Fig. 78. Hysteresis Conductance as Function of Number of Turns.

E as abscissæ in Curve 76.

N as abscissæ in Curve 77.

n as abscissæ in Curve 78.

As shown, a variation in the E.M.F. of 50 per cent causes a variation in g of only 14 per cent, while a variation in N or S by 50 per cent causes a variation in g of 21 per cent.

If \mathcal{R} = magnetic reluctance of a circuit, \mathcal{F}_A = maximum M.M.F., I = effective current, since $I\sqrt{2}$ = maximum current, the magnetic flux,

$$\Phi = \frac{\mathcal{F}_A}{\mathcal{R}} = \frac{n I \sqrt{2}}{\mathcal{R}}.$$

Substituting this in the equation of the counter E.M.F. of self-induction,

$$E = \sqrt{2} \pi N n \Phi 10^{-8},$$

we have

$$E = \frac{2 \pi n^2 N L 10^{-8}}{\mathcal{R}};$$

hence, the absolute admittance of the circuit is

$$y = \sqrt{g^2 + b^2} = \frac{I}{E} = \frac{\mathcal{R} 10^8}{2 \pi n^2 N} = \frac{a \mathcal{R}}{N},$$

where

$$a = \frac{10^8}{2 \pi n^2}, \text{ a constant.}$$

Therefore, the absolute admittance, y , of a circuit of negligible resistance is proportional to the magnetic reluctance, \mathcal{R} , and inversely proportional to the frequency, N , and to the square of the number of turns, n .

82. In a circuit containing iron, the reluctance, \mathcal{R} , varies with the magnetization; that is, with the E.M.F. Hence the admittance of such a circuit is not a constant, but is also variable.

In an ironclad electric circuit, — that is, a circuit whose magnetic field exists entirely within iron, such as the magnetic circuit of a well-designed alternating-current trans-

former, — \mathcal{R} is the reluctance of the iron circuit. Hence, if μ = permeability, since —

$$\mathcal{R} = \frac{\mathcal{F}_A}{\Phi},$$

and $\mathcal{F}_A = LF = \frac{10}{4\pi} L \mathcal{H} = \text{M.M.F.},$

$$\Phi = S \mathcal{B} = \mu S \mathcal{H} = \text{magnetic flux},$$

and $\mathcal{R} = \frac{10 L}{4\pi \mu S};$

substituting this value in the equation of the admittance,

$$y = \frac{\mathcal{R} 10^6}{2\pi n^2 N}, \text{ we have } \frac{L 10^9}{8\pi^2 n^2 \mu S N} = \frac{z}{N\mu},$$

where $z = \frac{L 10^9}{8\pi^2 n^2 S} = \frac{127 L 10^6}{n^2 S}.$

Therefore, in an ironclad circuit, the absolute admittance, y , is inversely proportional to the frequency, N , to the permeability, μ , to the cross-section, S , and to the square of the number of turns, n ; and directly proportional to the length of the magnetic circuit, L .

The conductance is $g = \frac{A}{N^6 E^4};$

and the admittance, $y = \frac{z}{N\mu};$

hence, the angle of hysteretic advance is

$$\sin \alpha = \frac{g}{y} = \frac{A \mu N^4}{z E^4};$$

or, substituting for A and z (p. 117),

$$\begin{aligned} \sin \alpha &= \mu \frac{N^4}{E^4} \frac{\eta L 10^{5.8}}{2.8 \pi^{1.6} S^6 n^{1.6}} \frac{8 \pi^2 n^2 S}{L 10^9}, \\ &= \frac{\mu \eta N^4 n^4 S^4 \pi^4 2^{2.2}}{E^4 10^{8.2}}; \end{aligned}$$

or, substituting

$$E = 2.5 \pi N n S \mathcal{B} 10^{-8},$$

we have $\sin \alpha = \frac{4 \mu \eta}{\mathcal{B}^4},$

which is independent of frequency, number of turns, and shape and size of the magnetic and electric circuit.

Therefore, in an ironclad inductance, the angle of hysteretic advance, α , depends upon the magnetic constants, permeability and coefficient of hysteresis, and upon the maximum magnetic induction, but is entirely independent of the frequency, of the shape and other conditions of the magnetic and electric circuit; and, therefore, all ironclad magnetic circuits constructed of the same quality of iron and using the same magnetic density, give the same angle of hysteretic advance.

The angle of hysteretic advance, α , in a closed circuit transformer, depends upon the quality of the iron, and upon the magnetic density only.

The sine of the angle of hysteretic advance equals $\frac{1}{4}$ times the product of the permeability and coefficient of hysteresis, divided by the $\frac{1}{4}$ th power of the magnetic density.

83. If the magnetic circuit is not entirely ironclad, and the magnetic structure contains air-gaps, the total reluctance is the sum of the iron reluctance and of the air reluctance, or

$$\mathcal{R} = \mathcal{R}_i + \mathcal{R}_a;$$

hence the admittance is

$$y = \sqrt{g^2 + b^2} = \frac{a}{N} (\mathcal{R}_i + \mathcal{R}_a).$$

Therefore, in a circuit containing iron, the admittance is the sum of the admittance due to the iron part of the circuit, $y_i = a / N \mathcal{R}_i$, and of the admittance due to the air part of the circuit, $y_a = a / N \mathcal{R}_a$, if the iron and the air are in series in the magnetic circuit.

The conductance, g , represents the loss of energy in the iron, and, since air has no magnetic hysteresis, is not changed by the introduction of an air-gap. Hence the angle of hysteretic advance of phase is

$$\sin \alpha = \frac{g}{y} = \frac{g}{y_i + y_a} = \frac{g}{y_i} \frac{\mathcal{R}_i}{\mathcal{R}_i + \mathcal{R}_a},$$

and a maximum, g/y_i , for the ironclad circuit, but decreases with increasing width of the air-gap. The introduction of the air-gap of reluctance, \mathfrak{R}_a , decreases $\sin \alpha$ in the ratio,

$$\frac{\mathfrak{R}_i}{\mathfrak{R}_i + \mathfrak{R}_a}$$

In the range of practical application, from $\mathfrak{B} = 2,000$ to $\mathfrak{B} = 12,000$, the permeability of iron varies between 900 and 2,000 approximately, while $\sin \alpha$ in an ironclad circuit varies in this range from .51 to .69. In air, $\mu = 1$.

If, consequently, one per cent of the length of the iron is replaced by an air-gap, the total reluctance only varies in the proportion of $1\frac{1}{5}$ to $1\frac{1}{20}$, or about 6 per cent, that is, remains practically constant; while the angle of hysteretic advance varies from $\sin \alpha = .035$ to $\sin \alpha = .064$. Thus g is negligible compared with b , and b is practically equal to y .

Therefore, in an electric circuit containing iron, but forming an open magnetic circuit whose air-gap is not less than $\frac{1}{100}$ the length of the iron, the susceptance is practically constant and equal to the admittance, so long as saturation is not yet approached, or,

$$b = \frac{\mathfrak{R}a}{N}, \text{ or: } x = \frac{N}{\mathfrak{R}a}$$

The angle of hysteretic advance is small, below 4° , and the hysteretic conductance is,

$$g = \frac{A}{E^4 N^6}$$

The current wave is practically a sine wave.

As an instance, in Fig. 71, Curve II., the current curve of a circuit is shown, containing an air-gap of only $\frac{1}{100}$ of the length of the iron, giving a current wave much resembling the sine shape, with an hysteretic advance of 9° .

84. To determine the electric constants of a circuit containing iron, we shall proceed in the following way:

Let —

E = counter E.M.F. of self-induction ;

then from the equation,

$$E = \sqrt{2} \pi n N \Phi 10^{-8},$$

where,

N = frequency,

n = number of turns,

we get the magnetism, Φ , and by means of the magnetic cross section, S , the maximum magnetic induction: $\mathfrak{B} = \Phi / S$.

From \mathfrak{B} , we get, by means of the magnetic characteristic of the iron, the M.M.F., = \mathfrak{F} ampere-turns per cm length, where

$$\mathfrak{F} = \frac{10}{4\pi} \mathfrak{C},$$

if \mathfrak{C} = M.M.F. in C.G.S. units.

Hence,

if L_i = length of iron circuit, $\mathfrak{F}_i = L_i \mathfrak{F}$ = ampere-turns required in the iron;

if L_a = length of air circuit, $\mathfrak{F}_a = \frac{10 L_a \mathfrak{B}}{4\pi}$ = ampere-turns required in the air;

hence, $\mathfrak{F} = \mathfrak{F}_i + \mathfrak{F}_a$ = total ampere-turns, maximum value, and $\mathfrak{F} / \sqrt{2}$ = effective value. The exciting current is

$$I = \frac{\mathfrak{F}}{n\sqrt{2}},$$

and the absolute admittance,

$$y = \sqrt{g^2 + b^2} = \frac{I}{E}.$$

If \mathfrak{F}_i is not negligible as compared with \mathfrak{F}_a , this admittance, y , is variable with the E.M.F., E .

If —

V = volume of iron,

η = coefficient of hysteresis,

the loss of energy by hysteresis due to molecular magnetic friction is,

$$W = \eta N V \mathfrak{B}^{1.6};$$

hence the hysteretic conductance is $g = W / E^2$, and variable with the E.M.F., E .

The angle of hysteretic advance is, —

$$\sin \alpha = \frac{g}{y};$$

the susceptance,

$$b = \sqrt{y^2 - g^2};$$

the effective resistance,

$$r = \frac{g}{y^2};$$

and the reactance,

$$x = \frac{b}{y^2}$$

85. As conclusions, we derive from this chapter the following:—

1.) In an alternating-current circuit surrounded by iron, the current produced by a sine wave of E.M.F. is not a true sine wave, but is distorted by hysteresis.

2.) This distortion is excessive only with a closed magnetic circuit transferring no energy into a secondary circuit by mutual inductance.

3.) The distorted wave of current can be replaced by the equivalent sine wave—that is a sine wave of equal effective intensity and equal power—and the superposed higher harmonic, consisting mainly of a term of triple frequency, may be neglected except in resonating circuits.

4.) Below saturation, the distorted curve of current and its equivalent sine wave have approximately the same maximum value.

5.) The angle of hysteretic advance,—that is, the phase difference between the magnetic flux and equivalent sine wave of M.M.F.,—is a maximum for the closed magnetic circuit, and depends there only upon the magnetic constants of the iron, upon the permeability, μ , the coefficient of hysteresis, η , and the maximum magnetic induction, as shown in the equation,

$$\sin \alpha = \frac{4 \mu \eta}{B^4}.$$

6.) The effect of hysteresis can be represented by an admittance, $Y = g + jb$, or an impedance, $Z = r - jx$.

7.) The hysteretic admittance, or impedance, varies with the magnetic induction; that is, with the E.M.F., etc.

8.) The hysteretic conductance, g , is proportional to the coefficient of hysteresis, η , and to the length of the magnetic circuit, L , inversely proportional to the 4th power of the E.M.F., E , to the 6th power of frequency, N , and of the cross-section of the magnetic circuit, S , and to the 1.6th power of the number of turns of the electric circuit, n , as expressed in the equation,

$$g = \frac{58 \eta L 10^8}{E^4 N^6 S^6 n^{1.6}}.$$

9.) The absolute value of hysteretic admittance, —

$$y = \sqrt{g^2 + b^2},$$

is proportional to the magnetic reluctance: $\mathcal{R} = \mathcal{R}_i + \mathcal{R}_a$, and inversely proportional to the frequency, N , and to the square of the number of turns, n , as expressed in the equation,

$$y = \frac{(\mathcal{R}_i + \mathcal{R}_a) 10^8}{2 \pi N n^2}.$$

10.) In an ironclad circuit, the absolute value of admittance is proportional to the length of the magnetic circuit, and inversely proportional to cross-section, S , frequency, N , permeability, μ , and square of the number of turns, n , or

$$y_i = \frac{127 L 10^6}{n^2 S N \mu}.$$

11.) In an open magnetic circuit, the conductance, g , is the same as in a closed magnetic circuit of the same iron part.

12.) In an open magnetic circuit, the admittance, y , is practically constant, if the length of the air-gap is at least $\frac{1}{10}$ of the length of the magnetic circuit, and saturation be not approached.

13.) In a closed magnetic circuit, conductance, susceptance, and admittance can be assumed as constant through a limited range only.

14.) From the shape and the dimensions of the circuits, and the magnetic constants of the iron, all the electric constants, g , b , y ; r , x , z , can be calculated.

CHAPTER XI.

FOUCAULT OR EDDY CURRENTS.

86. While magnetic hysteresis or molecular friction is a magnetic phenomenon, eddy currents are rather an electrical phenomenon. When iron passes through a magnetic field, a loss of energy is caused by hysteresis, which loss, however, does not react magnetically upon the field. When cutting an electric conductor, the magnetic field induces a current therein. The M.M.F. of this current reacts upon and affects the magnetic field, more or less; consequently, an alternating magnetic field cannot penetrate deeply into a solid conductor, but a kind of screening effect is produced, which makes solid masses of iron unsuitable for alternating fields, and necessitates the use of laminated iron or iron wire as the carrier of magnetic flux.

Eddy currents are true electric currents, though flowing in minute circuits; and they follow all the laws of electric circuits.

Their E.M.F. is proportional to the intensity of magnetization, \mathcal{B} , and to the frequency, N .

Eddy currents are thus proportional to the magnetization, \mathcal{B} , the frequency, N , and to the electric conductivity, γ , of the iron; hence, can be expressed by

$$i = \beta \gamma \mathcal{B} N.$$

The power consumed by eddy currents is proportional to their square, and inversely proportional to the electric conductivity, and can be expressed by

$$P = \beta \gamma \mathcal{B}^2 N^2;$$

or, since, \mathcal{N} is proportional to the induced E.M.F., E , in the equation

$$E = \sqrt{2} \pi S n N \mathcal{N} 10^{-8},$$

it follows that, *The loss of power by eddy currents is proportional to the square of the E.M.F., and proportional to the electric conductivity of the iron*; or,

$$W = a E^2 \gamma.$$

Hence, that component of the effective conductance which is due to eddy currents, is

$$g = \frac{W}{E^2} = a \gamma;$$

that is, *The equivalent conductance due to eddy currents in the iron is a constant of the magnetic circuit; it is independent of E.M.F., frequency, etc., but proportional to the electric conductivity of the iron, γ .*

87. Eddy currents, like magnetic hysteresis, cause an advance of phase of the current by an *angle of advance*, β ; but, unlike hysteresis, eddy currents in general do not distort the current wave.

The angle of advance of phase due to eddy currents is,

$$\sin \beta = \frac{g}{y},$$

where y = absolute admittance of the circuit, g = eddy current conductance.

While the equivalent conductance, g , due to eddy currents, is a constant of the circuit, and independent of E.M.F., frequency, etc., the loss of power by eddy currents is proportional to the square of the E.M.F. of self-induction, and therefore proportional to the square of the frequency and to the square of the magnetization.

Only the energy component, gE , of eddy currents, is of interest, since the wattless component is identical with the wattless component of hysteresis, discussed in a preceding chapter.

88. To calculate the loss of power by eddy currents —

Let V = volume of iron ;

\mathcal{B} = maximum magnetic induction ;

N = frequency ;

γ = electric conductivity of iron ;

ϵ = coefficient of eddy currents.

The loss of energy per cm^3 , in ergs per cycle, is

$$W = \epsilon \gamma N \mathcal{B}^2 ;$$

hence, the total loss of power by eddy currents is

$$W = \epsilon \gamma V N^2 \mathcal{B}^2 10^{-7} \text{ watts,}$$

and the equivalent conductance due to eddy currents is

$$g = \frac{W}{E^2} = \frac{10 \epsilon \gamma l}{2 \pi^2 S n^2} = \frac{.507 \epsilon \gamma l}{S n^2},$$

where :

l = length of magnetic circuit,

S = section of magnetic circuit,

n = number of turns of electric circuit.

The coefficient of eddy currents, ϵ , depends merely upon the shape of the constituent parts of the magnetic circuit ; that is, whether of iron plates or wire, and the thickness of plates or the diameter of wire, etc.

The two most important cases are :

(a). Laminated iron.

(b). Iron wire.

89. (a). *Laminated Iron.*

Let, in Fig. 79,

d = thickness of the iron plates ;

\mathcal{B} = maximum magnetic induction ;

N = frequency ;

γ = electric conductivity of the iron.

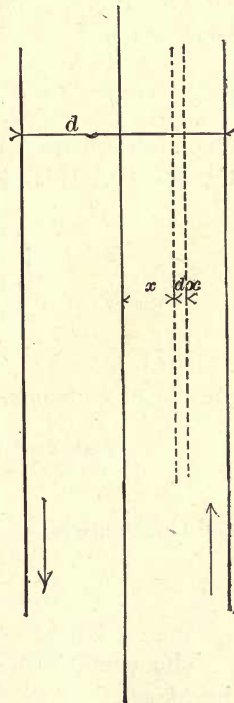


Fig. 79.

Then, if x is the distance of a zone, $d x$, from the center of the sheet, the conductance of a zone of thickness, $d x$, and of one cm length and width is $\gamma d x$; and the magnetic flux cut by this zone is $\mathfrak{B} x$. Hence, the E.M.F. induced in this zone is

$$\delta E = \sqrt{2} \pi N \mathfrak{B} x, \text{ in C.G.S. units.}$$

This E.M.F. produces the current :

$$d I = \delta E \gamma d x = \sqrt{2} \pi N \mathfrak{B} \gamma x d x, \text{ in C.G.S. units,}$$

provided the thickness of the plate is negligible as compared with the length, in order that the current may be assumed as flowing parallel to the sheet, and in opposite directions on opposite sides of the sheet.

The power consumed by the induced current in this zone, $d x$, is

$$d P = \delta E d I = 2 \pi^2 N^2 \mathfrak{B}^2 \gamma x^2 d x, \text{ in C.G.S. units or ergs per second,}$$

and, consequently, the total power consumed in one cm^2 of the sheet of thickness, d , is

$$\begin{aligned} \delta P &= \int_{-\frac{d}{2}}^{+\frac{d}{2}} d P = 2 \pi^2 N^2 \mathfrak{B}^2 \gamma \int_{-\frac{d}{2}}^{+\frac{d}{2}} x^2 d x \\ &= \frac{\pi^2 N^2 \mathfrak{B}^2 \gamma d^3}{6}, \text{ in C.G.S. units; } \end{aligned}$$

the power consumed per cm^3 of iron is, therefore,

$$p = \frac{\delta P}{d} = \frac{\pi^2 N^2 \mathfrak{B}^2 \gamma d^2}{6}, \text{ in C.G.S. units or erg-seconds,}$$

and the energy consumed per cycle and per cm^3 of iron is

$$h = \frac{p}{N} = \frac{\pi^2 \gamma d^2 N \mathfrak{B}^2}{6} \text{ ergs.}$$

The coefficient of eddy currents for laminated iron is, therefore,

$$\epsilon = \frac{\pi^2 d^2}{6} = 1.645 d^2,$$

where γ is expressed in C.G.S. units. Hence, if γ is expressed in practical units or 10^{-9} C.G.S. units,

$$\epsilon = \frac{\pi^2 d^2 10^{-9}}{6} = 1.645 d^2 10^{-9}.$$

Substituting for the conductivity of sheet iron the approximate value,

$$\gamma = 10^5,$$

we get as the coefficient of eddy currents for laminated iron,

$$\epsilon = \frac{\pi^2}{6} d^2 10^{-9} = 1.645 d^2 10^{-9}.$$

loss of energy per cm^3 and cycle,

$$W = \epsilon \gamma N \mathcal{B}^2 = \frac{\pi^2}{6} d^2 \gamma N \mathcal{B}^2 10^{-9} = 1.645 d^2 \gamma N \mathcal{B}^2 10^{-9} \text{ ergs}$$

$$= 1.645 d^2 N \mathcal{B}^2 10^{-4} \text{ ergs};$$

or, $W = \epsilon \gamma N \mathcal{B}^2 10^{-7} = 1.645 d^2 N \mathcal{B}^2 10^{-11} \text{ joules};$

loss of power per cm^3 at frequency, N ,

$$p = NW = \epsilon \gamma N^2 \mathcal{B}^2 10^{-7} = 1.645 d^2 N^2 \mathcal{B}^2 10^{-11} \text{ watts};$$

total loss of power in volume, V ,

$$P = Vp = 1.645 V d^2 N^2 \mathcal{B}^2 10^{-11} \text{ watts.}$$

As an example,

$$d = 1 \text{ mm} = .1 \text{ cm}; N = 100; \mathcal{B} = 5000; V = 1000 \text{ cm}^3.$$

$$\epsilon = 1,645 \times 10^{-11};$$

$$W = 4110 \text{ ergs}$$

$$= .000411 \text{ joules};$$

$$p = .0411 \text{ watts};$$

$$P = 41.1 \text{ watts.}$$

90. (b). *Iron Wire.*

Let, in Fig. 80, d = diameter of a piece of iron wire; then if x is the radius of a circular zone of thickness, $d x$, and one cm in length, the conductance of this

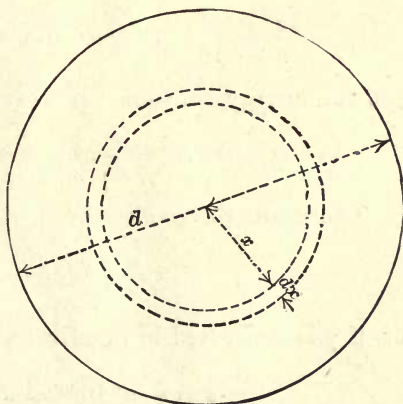


Fig. 80.

zone is, $\gamma \frac{d^2 x}{2 \pi x}$, and the magnetic flux inclosed by the zone is $\mathcal{B} x^2 \pi$.

Hence, the E.M.F. induced in this zone is :

$$\delta E = \sqrt{2} \pi^2 N \mathcal{B} x^2, \text{ in C.G.S. units,}$$

and the current produced thereby is,

$$\begin{aligned} dI &= \frac{\gamma dx}{2 \pi x} \times \sqrt{2} \pi^2 N \mathcal{B} x^2 \\ &= \frac{\sqrt{2} \pi}{2} \gamma N \mathcal{B} x dx, \text{ in C.G.S. units.} \end{aligned}$$

The power consumed in this zone is, therefore,

$$dP = \delta E dI = \pi^3 \gamma N^2 \mathcal{B}^2 x^3 dx, \text{ in C.G.S. units}$$

consequently, the total power consumed in one cm length of wire is

$$\begin{aligned} \delta P &= \int_0^d dW = \pi^3 \gamma N^2 \mathcal{B}^2 \int_0^d x^3 dx \\ &= \frac{\pi^3}{6^4} \gamma N^2 \mathcal{B}^2 d^4, \text{ in C.G.S. units.} \end{aligned}$$

Since the volume of one cm length of wire is

$$v = \frac{d^2 \pi}{4},$$

the power consumed in one cm^3 of iron is

$$p = \frac{\delta P}{v} = \frac{\pi^2}{16} \gamma N^2 \mathcal{B}^2 d^2, \text{ in C.G.S. units or erg-seconds,}$$

and the energy consumed per cycle and cm^3 of iron is

$$W = \frac{p}{N} = \frac{\pi^2}{16} \gamma N \mathcal{B}^2 \text{ ergs.}$$

Therefore, the coefficient of eddy currents for iron wire is

$$\epsilon = \frac{\pi^2}{16} d^2 = .617 d^2;$$

or, if γ is expressed in practical units, or 10^{-9} C.G.S. units,

$$\epsilon = \frac{\pi^2}{16} d^2 10^{-9} = .617 d^2 10^{-9}.$$

Substituting $\gamma = 10^5$,

we get as the coefficient of eddy currents for iron wire,

$$\epsilon = \frac{\pi^2}{16} d^2 10^{-9} = .617 d^2 10^{-9}.$$

The loss of energy per cm^3 of iron, and per cycle becomes

$$\begin{aligned} W &= \epsilon \gamma N \mathcal{B}^2 = \frac{\pi^2}{16} d^2 \gamma N \mathcal{B}^2 10^9 = .617 d^2 \gamma N \mathcal{B}^2 10^{-9} \\ &= .617 d^2 N \mathcal{B}^2 10^{-4} \text{ ergs,} \\ &= \epsilon \gamma N \mathcal{B}^2 10^{-7} = .617 d^2 N \mathcal{B}^2 10^{-11} \text{ joules;} \end{aligned}$$

loss of power per cm^3 , at frequency, N ,

$$p = Nh = \epsilon \gamma N^2 \mathcal{B}^2 10^{-7} = .617 d^2 N^2 \mathcal{B}^2 10^{-11} \text{ watts;}$$

total loss of power in volume, V ,

$$P = Vp = .617 V d^2 N^2 \mathcal{B}^2 10^{-11} \text{ watts.}$$

As an example,

$$d = 1 \text{ mm,} = 1 \text{ cm;} \quad N = 100; \quad \mathcal{B}^2 = 5,000; \quad V = 1,000 \text{ cm}^3.$$

Then,

$$\begin{aligned} \epsilon &= .617 \times 10^{-11}, \\ W &= 1540 \text{ ergs} = .000154 \text{ joules,} \\ p &= .0154 \text{ watts,} \\ P &= 15.4 \text{ watts,} \end{aligned}$$

hence very much less than in sheet iron of equal thickness.

91. Comparison of sheet iron and iron wire.

If

d_1 = thickness of lamination of sheet iron, and

d_2 = diameter of iron wire,

the eddy-coefficient of sheet iron being

$$\epsilon_1 = \frac{\pi^2}{6} d_1^2 10^{-9},$$

and the eddy coefficient of iron wire

$$\epsilon_2 = \frac{\pi^2}{16} d_2^2 10^{-9},$$

the loss of power is equal in both — other things being equal — if $\epsilon_1 = \epsilon_2$; that is, if,

$$d_2^3 = \frac{8}{3} d_1^3,$$

or,

$$d_2 = 1.63 d_1.$$

It follows that the diameter of iron wire can be 1.63 times, or, roughly, $1\frac{2}{3}$ as large as the thickness of laminated iron, to give the same loss of energy through eddy currents.

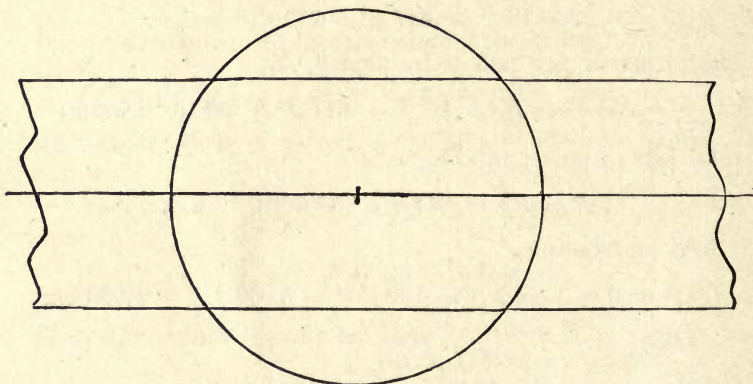


Fig. 81.

92. Demagnetizing, or screening effect of eddy currents.

The formulas derived for the coefficient of eddy currents in laminated iron and in iron wire, hold only when the eddy currents are small enough to neglect their magnetizing force. Otherwise the phenomenon becomes more complicated; the magnetic flux in the interior of the lamina, or the wire, is not in phase with the flux at the surface, but lags behind it. The magnetic flux at the surface is due to the impressed M.M.F., while the flux in the interior is due to the resultant of the impressed M.M.F. and to the M.M.F. of eddy currents; since the eddy currents lag 90° behind the flux producing them, their resultant with the impressed M.M.F., and therefore the magnetism in the

interior, is made lagging. Thus, progressing from the surface towards the interior, the magnetic flux gradually lags more and more in phase, and at the same time decreases in intensity. While the complete analytical solution of this phenomenon is beyond the scope of this book, a determination of the magnitude of this demagnetization, or screening effect, sufficient to determine whether it is negligible, or whether the subdivision of the iron has to be increased to make it negligible, can be made by calculating the maximum magnetizing effect, which cannot be exceeded by the eddys.

Assuming the magnetic density as uniform over the whole cross-section, and therefore all the eddy currents in phase with each other, their total M.M.F. represents the maximum possible value, since by the phase difference and the lesser magnetic density in the center the resultant M.M.F. is reduced.

In laminated iron of thickness l , the current in a zone of thickness, dx at distance x from center of sheet, is :

$$\begin{aligned} dI &= \sqrt{2} \pi N \mathcal{G} j x dx \text{ units (C.G.S.)} \\ &= \sqrt{2} \pi N \mathcal{G} j x dx 10^{-8} \text{ amperes ;} \end{aligned}$$

hence the total current in sheet is

$$\begin{aligned} I &= \int_0^{\frac{l}{2}} dI = \sqrt{2} \pi N \mathcal{G} j 10^{-8} \int_0^{\frac{l}{2}} x dx \\ &= \frac{\sqrt{2} \pi}{8} N \mathcal{G} j l^2 10^{-8} \text{ amperes.} \end{aligned}$$

Hence, the maximum possible demagnetizing ampere-turns acting upon the center of the lamina, are

$$\begin{aligned} I &= \frac{\sqrt{2} \pi}{8} N \mathcal{G} j l^2 10^{-8} = .555 N \mathcal{G} j l^2 10^{-8} \\ &= .555 N \mathcal{G} l^2 10^{-8} \text{ ampere-turns per cm.} \end{aligned}$$

Example : $d = .1$ cm, $N = 100$, $\mathcal{G} = 5,000$,
or $I = 2.775$ ampere-turns per cm.

93. In iron wire of diameter l , the current in a tubular zone of dx thickness and x radius is

$$dI = \frac{\sqrt{2}}{2} \pi N \mathfrak{B} j x dx 10^{-8} \text{ amperes;}$$

hence, the total current is

$$\begin{aligned} I &= \int_0^{\frac{l}{2}} dI \frac{\sqrt{2}}{2} \pi N \mathfrak{B} j 10^{-8} \int_0^{\frac{l}{2}} x dx \\ &= \frac{\sqrt{2}}{16} \pi N \mathfrak{B} j l^2 10^{-8} \text{ amperes.} \end{aligned}$$

Hence, the maximum possible demagnetizing ampere-turns, acting upon the center of the wire, are

$$\begin{aligned} I &= \frac{\sqrt{2} \pi}{16} N \mathfrak{B} j l^2 10^{-8} = .2775 N \mathfrak{B} j l^2 10^{-8} \\ &= .2775 N \mathfrak{B} l^2 10^{-8} \text{ ampere-turns per cm.} \end{aligned}$$

For example, if $l = .1$ cm, $N = 100$, $\mathfrak{B} = 5,000$, then $I = 1,338$ ampere-turns per cm; that is, half as much as in a lamina of the thickness l .

94. Besides the eddy, or Foucault, currents proper, which flow as parasitic circuits in the interior of the iron lamina or wire, under certain circumstances eddy currents also flow in larger orbits from lamina to lamina through the whole magnetic structure. Obviously a calculation of these eddy currents is possible only in a particular structure. They are mostly surface currents, due to short circuits existing between the laminæ at the surface of the magnetic structure.

Furthermore, eddy currents are induced outside of the magnetic iron circuit proper, by the magnetic stray field cutting electric conductors in the neighborhood, especially when drawn towards them by iron masses behind, in electric conductors passing through the iron of an alternating field, etc. All these phenomena can be calculated only in particular cases, and are of less interest, since they can easily be avoided.

Eddy Currents in Conductor, and Unequal Current Distribution.

95. If the electric conductor has a considerable size, the alternating magnetic field, in cutting the conductor, may set up differences of potential between the different parts thereof, thus giving rise to local or eddy currents in the copper. This phenomenon can obviously be studied only with reference to a particular case, where the shape of the conductor and the distribution of the magnetic field are known.

Only in the case where the magnetic field is produced by the current flowing in the conductor can a general solution be given. The alternating current in the conductor produces a magnetic field, not only outside of the conductor, but inside of it also; and the lines of magnetic force which close themselves inside of the conductor induce E.M.F.s. in their interior only. Thus the counter E.M.F. of self-inductance is largest at the axis of the conductor, and least at its surface; consequently, the current density at the surface will be larger than at the axis, or, in extreme cases, the current may not penetrate at all to the center, or a reversed current flow there. Hence it follows that only the exterior part of the conductor may be used for the conduction of the current, thereby causing an increase of the ohmic resistance due to unequal current distribution.

The general solution of this problem for round conductors leads to complicated equations, and can be found in Maxwell.

In practice, this phenomenon is observed only with very high frequency currents, as lightning discharges; in power distribution circuits it has to be avoided by either keeping the frequency sufficiently low, or having a shape of conductor such that unequal current distribution does not take place, as by using a tubular or a stranded conductor, or several conductors in parallel.

96. It will, therefore, be sufficient to determine the largest size of round conductor, or the highest frequency, where this phenomenon is still negligible.

In the interior of the conductor, the current density is not only less than at the surface, but the current lags behind the current at the surface, due to the increased effect of self-inductance. This lag of the current causes the magnetic fluxes in the conductor to be out of phase with each other, making their resultant less than their sum, while the lesser current density in the center reduces the total flux inside of the conductor. Thus, by assuming, as a basis for calculation, a uniform current density and no difference of phase between the currents in the different layers of the conductor, the unequal distribution is found larger than it is in reality. Hence this assumption brings us on the safe side, and at the same time simplifies the calculation greatly.

Let Fig. 82 represent a cross-section of a conductor of radius R , and a uniform current density,

$$i = \frac{I}{R^2 \pi},$$

where I = total current in conductor.

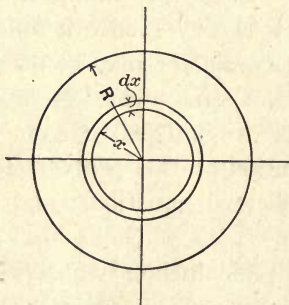


Fig. 82.

The magnetic reluctance of a tubular zone of unit length and thickness dx , of radius x , is

$$\mathcal{R}_x = \frac{2 x \pi}{dx}.$$

The current inclosed by this zone is $I_x = ix^2\pi$, and therefore, the M.M.F. acting upon this zone is

$$\mathcal{F}_x = \frac{4\pi}{10} I_x = \frac{4\pi^2 ix^2}{10},$$

and the magnetic flux in this zone is

$$d\Phi = \frac{\mathcal{F}_x}{\mathcal{R}_x} = \frac{2\pi ix dx}{10}.$$

Hence, the total magnetic flux inside the conductor is

$$\Phi = \int_0^{\mathcal{R}} d\Phi = \frac{2\pi}{10} i \int_0^{\mathcal{R}} x dx = \frac{\pi i \mathcal{R}^2}{10} = \frac{I}{10}.$$

From this we get, as the excess of counter E.M.F. at the axis of the conductor over that at the surface —

$$\begin{aligned} \Delta E &= \sqrt{2} \pi N \Phi 10^{-9} = \sqrt{2} \pi N I 10^{-9}, \text{ per unit length,} \\ &= \sqrt{2} \pi^2 N i \mathcal{R}^2 10^{-9}; \end{aligned}$$

and the reactivity, or specific reactance at the center of the conductor, becomes

$$k = \frac{\Delta E}{i} = \sqrt{2} \pi^2 N \mathcal{R}^2 10^{-9}.$$

Let ρ = resistivity, or specific resistance, of the material of the conductor.

We have then,

$$\frac{b}{\rho} = \frac{\sqrt{2} \pi^2 N \mathcal{R}^2 10^{-9}}{\rho};$$

and

$$\frac{k}{\sqrt{k^2 + \rho^2}},$$

the percentage decrease of current density at center over that at periphery;

also,

$$\frac{r}{\sqrt{k^2 + \rho^2}},$$

the ratio of current densities at center and at periphery.

For example, if, in copper, $\rho = 1.7 \times 10^{-6}$, and the percentage decrease of current density at center shall not exceed 5 per cent, that is —

$$r \div \sqrt{k^2 + \rho^2} = .95 \div 1,$$

we have,

$$k = .51 \times 10^{-6};$$

$$\text{hence } .51 \times 10^{-6} = \sqrt{2} \pi^2 N R^2 10^{-9}$$

$$\text{or } N R^2 = 36.6 ;$$

$$\text{hence, when } N = \quad 125 \quad 100 \quad 60 \quad 33.3$$

$$R = \quad .541 \quad .605 \quad .781 \quad 1.05 \text{ cm.}$$

$$D = 2 R = \quad 1.08 \quad 1.21 \quad 1.56 \quad 2.1 \text{ cm.}$$

Hence, even at a frequency of 125 cycles, the effect of unequal current distribution is still negligible at one cm diameter of the conductor. Conductors of this size are, however, excluded from use at this frequency by the external self-induction, which is several times larger than the resistance.

We thus see that unequal current distribution is usually negligible in practice.

Mutual Inductance.

97. When an alternating magnetic field of force includes a secondary electric conductor, it induces therein an E.M.F. which produces a current, and thereby consumes energy if the circuit of the secondary conductor is closed.

A particular case of such induced secondary currents are the eddy or Foucault currents previously discussed.

Another important case is the induction of secondary E.M.Fs. in neighboring circuits; that is, the interference of circuits running parallel with each other.

In general, it is preferable to consider this phenomenon of mutual inductance as not merely producing an energy component and a wattless component of E.M.F. in the primary conductor, but to consider explicitly both the secondary and the primary circuit, as will be done in the chapter on the alternating-current transformer.

Only in cases where the energy transferred into the secondary circuit constitutes a small part of the total primary energy, as in the discussion of the disturbance caused by one circuit upon a parallel circuit, may the effect on the primary circuit be considered analogously as in the chapter on eddy currents, by the introduction of an energy com-

ponent, representing the loss of power, and a wattless component, representing the decrease of self-inductance.

Let —

$x = 2 \pi N L =$ reactance of main circuit; that is, $L =$ total number of interlinkages with the main conductor, of the lines of magnetic force produced by unit current in that conductor;

$x_1 = 2 \pi N L_1 =$ reactance of secondary circuit; that is, $L_1 =$ total number of interlinkages with the secondary conductor, of the lines of magnetic force produced by unit current in that conductor;

$x_m = 2 \pi N L_m =$ mutual inductance of circuits; that is, $L_m =$ total number of interlinkages with the secondary conductor, of the lines of magnetic force produced by unit current in the main conductor, or total number of interlinkages with the main conductor of the lines of magnetic force produced by unit current in the secondary conductor.

Obviously :

$$x_m^2 \leq x x_1.*$$

* As coefficient of self-inductance L, L' , the total flux surrounding the conductor is here meant. Quite frequently in the discussion of inductive apparatus, especially of transformers, that part of the magnetic flux is denoted self-inductance of the one circuit which surrounds this circuit, but not the other circuit; that is, which passes between both circuits. Hence, the total self-inductance, L , is in this case equal to the sum of the self-inductance, L' , and the mutual inductance, L_m .

The object of this distinction is to separate the wattless part, L' , of the total self-inductance, L , from that part, L_m , which represents the transfer of E.M.F. into the secondary circuit, since the action of these two components is essentially different.

Thus, in alternating-current transformers it is customary—and will be done later in this book—to denote as the self-inductance, L , of each circuit only that part of the magnetic flux produced by the circuit which passes between both circuits, and thus acts in “choking” only, but not in transforming; while the flux surrounding both circuits is called mutual inductance, or useful magnetic flux.

With this denotation, in transformers the mutual inductance, L_m , is usually very much greater than the self-inductances, L' , and L'_1 , while, if the self-inductances, L and L_1 , represent the total flux, their product is larger than the square of the mutual inductance, L_m ; or

$$L L_1 \geq L_m^2; \quad (L' + L_m)(L'_1 + L_m) \geq L_m^2.$$

Let r_1 = resistance of secondary circuit. Then the impedance of secondary circuit is

$$Z_1 = r_1 - jx_1, \quad z_1 = \sqrt{r_1^2 + x_1^2}; \quad *$$

E.M.F. induced in the secondary circuit, $E_1 = jx_m I$,

where I = primary current. Hence, the secondary current is

$$I_1 = \frac{E_1}{z_1} = \frac{jx_m}{r_1 - jx_1} I;$$

and the E.M.F. induced in the primary circuit by the secondary current, I_1 is

$$E = jx_m I_1;$$

$$E = \frac{-x_m^2}{r_1 - jx_1} I;$$

or, expanded,

$$E = \left\{ \frac{-x_m^2 r_1}{r_1^2 + x_1^2} - \frac{jx_m^2 x_1}{r_1^2 + x_1^2} \right\} I.$$

Hence,

$$g = \frac{x_m^2 r_1}{r_1^2 + x_1^2} = \text{effective conductance of mutual inductance};$$

$$b = \frac{-x_m^2 x_1}{r_1^2 + x_1^2} = \text{effective susceptance of mutual inductance}.$$

The susceptance of mutual inductance is negative, or of opposite sign from the susceptance of self-inductance. Or,

Mutual inductance consumes energy and decreases the self-inductance.

Dielectric and Electrostatic Phenomena.

98. While magnetic hysteresis and eddy currents can be considered as the energy component of inductance, condensation has an energy component also, called dielectric hysteresis. In an alternating magnetic field, energy is consumed in hysteresis due to molecular friction, and similarly, energy is also consumed in an alternating electrostatic field in the dielectric medium, in what is called dielectric hysteresis.

While the laws of the loss of energy by magnetic hysteresis are fairly well understood, and the magnitude of the effect known, the phenomenon of dielectric hysteresis is still almost entirely unknown as concerns its laws and the magnitude of the effect.

It is quite probable that the loss of power in the dielectric in an alternating electrostatic field consists of two distinctly different components, of which the one is directly proportional to the frequency, — analogous to magnetic hysteresis, and thus a constant loss of energy per cycle, independent of the frequency; while the other component is proportional to the square of the frequency, — analogous to the loss of power by eddy currents in the iron, and thus a loss of energy per cycle proportional to the frequency.

The existence of a loss of power in the dielectric, proportional to the square of the frequency, I observed some time ago in paraffined paper in a high electrostatic field and at high frequency, by the electro-dynamometer method, and other observers under similar conditions have found the same result.

Arno of Turin found at low frequencies and low field strength in a larger number of dielectrics, a loss of energy per cycle independent of the frequency, but proportional to the 1.6th power of the field strength, — that is, following the same law as the magnetic hysteresis,

$$W_{\text{H}} = \eta B^{1.6}.$$

This loss, probably true dielectric static hysteresis, was observed under conditions such that a loss proportional to the square of density and frequency must be small, while at high densities and frequencies, as in condensers, the true dielectric hysteresis may be entirely obscured by a viscous loss, represented by $W_{\text{H}} = \epsilon N B^2$.

99. If the loss of power by electrostatic hysteresis is proportional to the square of the frequency and of the field intensity, — as it probably nearly is under the working con-

ditions of alternating-current condensers, — then it is proportional to the square of the E.M.F., that is, the effective conductance, g , due to dielectric hysteresis is a constant; and, since the condenser susceptance, $-b = b'$, is a constant also, — unlike the magnetic inductance, — the ratio of conductance and susceptance, that is, the angle of difference of phase due to dielectric hysteresis, is a constant. This I found proved by experiment.

This would mean that the dielectric hysteretic admittance of a condenser,

$$Y = g + jb = g - jc,$$

where

$$g = \text{hysteretic conductance,}$$

$$b' = \text{hysteretic susceptance;}$$

and the dielectric hysteretic impedance of a condenser,

$$Z = r - jb' = r + jx_c,$$

where:

$$r = \text{hysteretic resistance,}$$

$$x_c = \text{hysteretic condensance;}$$

and the angle of dielectric hysteretic lag,

$$\tan a = \frac{g}{b'} = \frac{r}{x_c},$$

are constants of the circuit, independent of E.M.F. and frequency. The E.M.F. is obviously inversely proportional to the frequency.

The true static dielectric hysteresis, observed by Arno as proportional to the 1.6th power of the density, will enter the admittance and the impedance as a term variable and dependent upon E.M.F. and frequency, in the same manner as discussed in the chapter on magnetic hysteresis.

To the magnetic hysteresis corresponds, in the electrostatic field, the static component of dielectric hysteresis, following, probably, the same law of 1.6th power.

To the eddy currents in the iron corresponds, in the electrostatic field, the viscous component of dielectric hysteresis, following the square law.

To the phenomenon of mutual inductance corresponds, in the electrostatic field, the electrostatic induction, or influence.

100. The alternating electrostatic field of force of an electric circuit induces, in conductors within the field of force, electrostatic charges by what is called electrostatic influence. These charges are proportional to the field strength; that is, to the E.M.F. in the main circuit.

If a flow of current is produced by the induced charges, energy is consumed proportional to the square of the charge; that is, to the square of the E.M.F.

These induced charges, reacting upon the main conductor, influence therein charges of equal but opposite phase, and hence lagging behind the main E.M.F. by the angle of lag between induced charge and inducing field. They require the expenditure of a charging current in the main conductor in quadrature with the induced charge thereon; that is, nearly in quadrature with the E.M.F., and hence consisting of an energy component in phase with the E.M.F. — representing the power consumed by electrostatic influence — and a wattless component, which increases the capacity of the conductor, or, in other words, reduces its capacity susceptance, or condensance.

Thus, the electrostatic influence introduces an effective conductance, g , and an effective susceptance, b , — of opposite sign with condenser susceptance, — into the equations of the electric circuit.

While theoretically g and b should be constants of the circuit, frequently they are very far from such, due to disruptive phenomena beginning to appear at these high densities.

Even the capacity condensance changes at very high potentials; escape of electricity into the air and over the surfaces of the supporting insulators by brush discharge or electrostatic glow takes place. As far as this electrostatic

corona reaches, the space is in electric connection with the conductor, and thus the capacity of the circuit is determined, not by the surface of the metallic conductor, but by the exterior surface of the electrostatic glow surrounding the conductor. This means that with increasing potential, the capacity increases as soon as the electrostatic corona appears; hence, the condensance decreases, and at the same time an energy component appears, representing the loss of power in the corona.

This phenomenon thus shows some analogy with the decrease of magnetic inductance due to saturation.

At moderate potentials, the condensance due to capacity can be considered as a constant, consisting of a wattless component, the condensance proper, and an energy component, the dielectric hysteresis.

The condensance of a polarization cell, however, begins to decrease at very low potentials, as soon as the counter E.M.F. of chemical dissociation is approached.

The condensance of a synchronizing alternator is of the nature of a variable quantity; that is, the synchronous reactance changes gradually, according to the relation of impressed and of counter E.M.F., from inductance over zero to condensance.

Besides the phenomena discussed in the foregoing as terms of the energy components and the wattless components of current and of E.M.F., the electric leakage is to be considered as a further energy component; that is, the direct escape of current from conductor to return conductor through the surrounding medium, due to imperfect insulating qualities. This leakage current represents an effective conductance, g , theoretically independent of the E.M.F., but in reality frequently increasing greatly with the E.M.F., owing to the decrease of the insulating strength of the medium upon approaching the limits of its disruptive strength.

101. In the foregoing, the phenomena causing loss of energy in an alternating-current circuit have been discussed; and it has been shown that the mutual relation between current and E.M.F. can be expressed by two of the four constants:

Energy component of E.M.F., in phase with current, and =
current \times effective resistance, or r ;
wattless component of E.M.F., in quadrature with current, and =
current \times effective reactance, or x ;
energy component of current, in phase with E.M.F., and =
E.M.F. \times effective conductance, or g ;
wattless component of current, in quadrature with E.M.F., and =
E.M.F. \times effective susceptance, or b .

In many cases the exact calculation of the quantities, r , x , g , b , is not possible in the present state of the art.

In general, r , x , g , b , are not constants of the circuit, but depend — besides upon the frequency — more or less upon E.M.F., current, etc. Thus, in each particular case it becomes necessary to discuss the variation of r , x , g , b , or to determine whether, and through what range, they can be assumed as constant.

In what follows, the quantities r , x , g , b , will always be considered as the coefficients of the energy and wattless components of current and E.M.F., — that is, as the *effective* quantities, — so that the results are directly applicable to the general electric circuit containing iron and dielectric losses.

Introducing now, in Chapters VII. to IX., instead of “ohmic resistance,” the term “effective resistance,” etc., as discussed in the preceding chapter, the results apply also — within the range discussed in the preceding chapter — to circuits containing iron and other materials producing energy losses outside of the electric conductor.

CHAPTER XII.

DISTRIBUTED CAPACITY, INDUCTANCE, RESISTANCE, AND LEAKAGE.

102. As far as capacity has been considered in the foregoing chapters, the assumption has been made that the condenser or other source of negative reactance is shunted across the circuit at a definite point. In many cases, however, the capacity is distributed over the whole length of the conductor, so that the circuit can be considered as shunted by an infinite number of infinitely small condensers infinitely near together, as diagrammatically shown in Fig. 83.

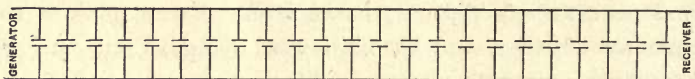


Fig. 83. *Distributed Capacity.*

In this case the intensity as well as phase of the current, and consequently of the counter E.M.F. of inductance and resistance, vary from point to point; and it is no longer possible to treat the circuit in the usual manner by the vector diagram.

This phenomenon is especially noticeable in long-distance lines, in underground cables, especially concentric cables, and to a certain degree in the high-potential coils of alternating-current transformers. It has the effect that not only the E.M.Fs., but also the currents, at the beginning, end, and different points of the conductor, are different in intensity and in phase.

Where the capacity effect of the line is small, it may with sufficient approximation be represented by one con-

denser of the same capacity as the line, shunted across the line. Frequently it makes no difference either, whether this condenser is considered as connected across the line at the generator end, or at the receiver end, or at the middle.

The best approximation is to consider the line as shunted at the generator and at the motor end, by two condensers of $\frac{1}{2}$ the line capacity each, and in the middle by a condenser of $\frac{2}{3}$ the line capacity. This approximation, based on Simpson's rule, assumes the variation of the electric quantities in the line as parabolic.

If, however, the capacity of the line is considerable, and the condenser current is of the same magnitude as the main current, such an approximation is not permissible, but each line element has to be considered as an infinitely small condenser, and the differential equations based thereon integrated.

103. It is thus desirable to first investigate the limits of applicability of the approximate representation of the line by one or by three condensers.

Assuming, for instance, that the line conductors are of 1 cm diameter, and at a distance from each other of 50 cm, and that the length of transmission is 50 km, we get the capacity of the transmission line from the formula —

$$c = \frac{1.11 \times 10^{-6} \epsilon l}{4 \log \text{nat} \frac{2d}{\delta}} \text{ microfarads,}$$

where

κ = dielectric constant of the surrounding medium = 1 in air;

l = length of conductor = 5×10^6 cm.;

d = distance of conductors from each other = 50 cm.;

δ = diameter of conductor = 1 cm.

Since

$$C = .3 \text{ microfarads,}$$

the capacity reactance is

$$x = \frac{10^6}{2 \pi N C} \text{ ohms,}$$

where N = frequency ; hence, at $N = 60$ cycles,

$$x = 8,900 \text{ ohms ;}$$

and the charging current of the line, at $E = 20,000$ volts, becomes,

$$i_o = \frac{E}{x} = 2.25 \text{ amperes.}$$

The resistance of 100 km of line of 1 cm diameter is 22 ohms ; therefore, at 10 per cent = 2,000 volts loss in the line, the main current transmitted over the line is

$$I = \frac{2,000}{22} = 91 \text{ amperes,}$$

representing about 1,800 kw.

In this case, the condenser current thus amounts to less than $2\frac{1}{2}$ per cent., and hence can still be represented by the approximation of one condenser shunted across the line.

If, however, the length of transmission is 150 km and the voltage 30,000,

capacity reactance at 60 cycles,	$x = 2,970$ ohms ;
charging current,	$i_o = 10.1$ amperes ;
line resistance,	$r = 66$ ohms ;
main current at 10 per cent loss,	$I = 45.5$ amperes.

The condenser current is thus about 22 per cent. of the main current.

At 300 km length of transmission it will, at 10 per cent. loss and with the same size of conductor, rise to nearly 90 per cent. of the main current, thus making a more explicit investigation of the phenomena in the line necessary.

In most cases of practical engineering, however, the capacity effect is small enough to be represented by the approximation of one ; viz., three condensers shunted across the line.

104. A.) *Line capacity represented by one condenser shunted across middle of line.*

Let —

$Y = g + jb$ = admittance of receiving circuit ;

$z = r - jx$ = impedance of line ;

b_c = condenser susceptance of line.

Denoting, in Fig. 84,

the E.M.F., viz., current in receiving circuit by E, I ,
 the E.M.F. at middle of line by E' ,
 the E.M.F., viz., current at generator by E_o, I_o ;

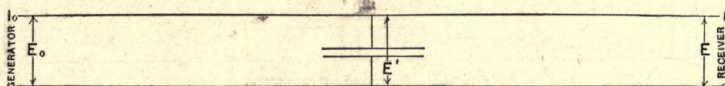


Fig. 84. Capacity Shunted across Middle of Line.

We have,

$$I = E (g + jb);$$

$$E' = E + \frac{r - jx}{2} I$$

$$= E \left\{ 1 + \frac{(r - jx)(g + jb)}{2} \right\};$$

$$I_o = I - jb_c E'$$

$$= E \left\{ g + jb - jx \left[1 + \frac{(r - jx)(g + jb)}{2} \right] \right\}$$

$$E_o = E' + \frac{r - jx}{2} I_o$$

$$= E \left\{ 1 + \frac{(r - jx)(g + jb)}{2} + \frac{(r - jx)(g + jb)}{2} - \frac{jb_c(r - jx)}{2} - jb_c \frac{(r - jx)^2(g + jb)}{4} \right\};$$

or, expanding,

$$I_o = E \{ [g + b_c(rb - xg)] + j[(b - b_c) - (rg + xb)] \};$$

$$E_o = E \left\{ 1 + (r - jx)(g + jb) - \frac{jb_c}{2}(r - jx) \right.$$

$$\left. \left[1 + \frac{(r - jx)(g + jb)}{2} \right] \right\}$$

$$= E \left\{ 1 + (r - jx) \left(g + jb - \frac{jb_c}{2} \right) - \frac{jb_c}{4}(r - jx)^2 (g + jb) \right\}.$$

105. B.) Line capacity represented by three condensers, in the middle and at the ends of the line.

Denoting, in Fig. 85,

the E.M.F. and current in receiving circuit by E, I ,
 the E.M.F. at middle of line by E' ,

the current on receiving side of line by I' ,
 the current on generator side of line by I'' ,
 the E.M.F., viz., current at generator by E_o , I_o ,

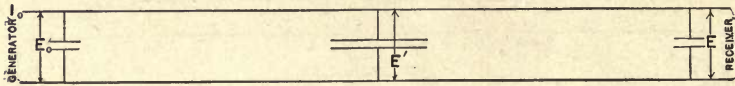


Fig. 85. Distributed Capacity.

otherwise retaining the same denotations as in A),

We have,

$$I = E(g + jb);$$

$$I' = I - \frac{jb_c E}{6}$$

$$= E \left\{ g + jb - \frac{jb_c}{6} \right\};$$

$$E' = E + \frac{r - jx}{2} I'$$

$$= E \left\{ 1 + \frac{r - jx}{2} \left(g + jb - \frac{jb_c}{6} \right) \right\};$$

$$I'' = I' - \frac{4jb_c E'}{6}$$

$$= E \left\{ g + jb - \frac{5jb_c}{6} - \frac{jb_c}{3} (r - jx) \left(g + jb - \frac{jb_c}{6} \right) \right\};$$

$$E_o = E' + \frac{r - jx}{2} I'';$$

$$E_o = E \left\{ 1 + (r - jx) \left(g + jb - \frac{jb_c}{2} \right) - \frac{jb_c}{6} (r - jx)^2 \left(g + jb - \frac{jb_c}{6} \right) \right\};$$

$$I_o = I'' - \frac{jb_c E_o}{6};$$

$$I_o = E \left\{ \left(g + jb - \frac{jb_c}{6} \right) - \frac{jb_c}{6} (r - jx) \left(3g + 3jb - \frac{5jb_c}{6} \right) - \frac{b_c^2}{36} (r - jx)^2 \left(g + jb - \frac{jb_c}{6} \right) \right\}.$$

As will be seen, the first terms in the expression of E_o and of I_o are the same in A) and in B).

106. C.) *Complete investigation of distributed capacity, inductance, leakage, and resistance.*

In some cases, especially in very long circuits, as in lines conveying alternating power currents at high potential over extremely long distances by overhead conductors or underground cables, or with very feeble currents at extremely high frequency, such as telephone currents, the consideration of the *line resistance* — which consumes E.M.Fs. in phase with the current — and of the *line reactance* — which consumes E.M.Fs. in quadrature with the current — is not sufficient for the explanation of the phenomena taking place in the line, but several other factors have to be taken into account.

In long lines, especially at high potentials, the *electrostatic capacity* of the line is sufficient to consume noticeable currents. The charging current of the line condenser is proportional to the difference of potential, and is one-fourth period ahead of the E.M.F. Hence, it will either increase or decrease the main current, according to the relative phase of the main current and the E.M.F.

As a consequence, the current will change in intensity as well as in phase, in the line from point to point; and the E.M.Fs. consumed by the resistance and inductance will therefore also change in phase and intensity from point to point, being dependent upon the current.

Since no insulator has an infinite resistance, and as at high potentials not only leakage, but even direct *escape of electricity* into the air, takes place by "silent discharge," we have to recognize the existence of a current approximately proportional and in phase with the E.M.F. of the line. This current represents consumption of energy, and is therefore analogous to the E.M.F. consumed by resistance, while the condenser current and the E.M.F. of inductance are wattless.

Furthermore, the alternate current passing over the line induces in all neighboring conductors secondary currents,

which react upon the primary current, and thereby introduce E.M.Fs. of *mutual inductance* into the primary circuit. Mutual inductance is neither in phase nor in quadrature with the current, and can therefore be resolved into an *energy component* of mutual inductance in phase with the current, which acts as an increase of resistance, and into a *wattless component* in quadrature with the current, which decreases the self-inductance.

This mutual inductance is by no means negligible, as, for instance, its disturbing influence in telephone circuits shows.

The alternating potential of the line induces, by *electrostatic influence*, electric charges in neighboring conductors outside of the circuit, which retain corresponding opposite charges on the line wires. This electrostatic influence requires the expenditure of a current proportional to the E.M.F., and consisting of an *energy component*, in phase with the E.M.F., and a *wattless component*, in quadrature thereto.

The alternating electromagnetic field of force set up by the line current produces in some materials a loss of energy by magnetic hysteresis, or an expenditure of E.M.F. in phase with the current, which acts as an increase of resistance. This electromagnetic hysteretic loss may take place in the conductor proper if iron wires are used, and will then be very serious at high frequencies, such as those of telephone currents.

The effect of *eddy currents* has already been referred to under "mutual inductance," of which it is an energy component.

The alternating electrostatic field of force expends energy in dielectrics by what is called *dielectric hysteresis*. In concentric cables, where the electrostatic gradient in the dielectric is comparatively large, the dielectric hysteresis may at high potentials consume far greater amounts of energy than the resistance does. The dielectric hysteresis

appears in the circuit as consumption of a current, whose component in phase with the E.M.F. is the *dielectric energy current*, which may be considered as the power component of the capacity current.

Besides this, there is the increase of ohmic resistance due to *unequal distribution of current*, which, however, is usually not large enough to be noticeable.

107. This gives, as the most general case, and per unit length of line :

E.M.Fs. consumed in phase with the current I , and $= rI$, representing consumption of energy, and due to :

Resistance, and its increase by unequal current distribution; to the energy component of *mutual inductance*; to *induced currents*; to the energy component of *self-inductance*; or to *electromagnetic hysteresis*.

E.M.Fs. consumed in quadrature with the current I , and $= xI$, wattless, and due to :

Self-inductance, and *Mutual inductance*.

Currents consumed in phase with the E.M.F., E , and $= gE$, representing consumption of energy, and due to :

Leakage through the insulating material, including silent discharge; energy component of *electrostatic influence*; energy component of *capacity*, or of *dielectric hysteresis*.

Currents consumed in quadrature to the E.M.F., E , and $= bE$, being wattless, and due to :

Capacity and *Electrostatic influence*.

Hence we get four constants :—

Effective resistance, r ,

Effective reactance, x ,

Effective conductance, g ,

Effective susceptance, $b = -b_c$.

per unit length of line, which represent the coefficients, per unit length of line, of

- E.M.F. consumed in phase with current ;
- E.M.F. consumed in quadrature with current ;
- Current consumed in phase with E.M.F. ;
- Current consumed in quadrature with E.M.F.

108. This line we may assume now as feeding into a *receiver circuit of any description*, and determine the current and E.M.F. at any point of the circuit.

That is, an E.M.F. and current (differing in phase by any desired angle) may be given at the terminals of receiving circuit. To be determined are the E.M.F. and current at any point of the line ; for instance, at the generator terminals.

Or, $Z_1 = r_1 - jx_1$;

the impedance of receiver circuit, or admittance,

$$Y_1 = g_1 + jb_1,$$

and E.M.F., E_o , at generator terminals are given. Current and E.M.F. at any point of circuit to be determined, etc.

109. Counting now the distance, x , from a point, 0, of the line which has the E.M.F.,

$$E_1 = e_1 + je_1', \text{ and the current: } I_1 = i_1 + ji_1',$$

and counting x positive in the direction of rising energy, and negative in the direction of decreasing energy, we have at any point, x , in the line differential, dx :

$$\text{Leakage current: } Egd x;$$

$$\text{Capacity current: } -jEb_c dx;$$

hence, the total current consumed by the line element, dx , is

$$\begin{aligned} dI &= E(g - jb_c) dx, \text{ or,} \\ \frac{dI}{dx} &= E(g - jb_c). \end{aligned} \quad (1)$$

E.M.F. consumed by resistance, $Ir dx$;

E.M.F. consumed by reactance, $-jIx dx$;

hence, the total E.M.F. consumed in the line element, dx , is

$$\begin{aligned} dE &= I(r - jx) dx, \text{ or,} \\ \frac{dE}{dx} &= I(r - jx). \end{aligned} \quad (2)$$

These *fundamental differential equations*:

$$\left. \begin{aligned} \frac{dI}{dx} &= E(g - j\sigma_c), \\ \frac{dE}{dx} &= I(r - jx), \end{aligned} \right\} \quad (1)$$

are symmetrical with respect to I and E .

Differentiating these equations:

$$\left. \begin{aligned} \frac{d^2 I}{dx^2} &= \frac{dE}{dx} (g - j b_c), \\ \frac{d^2 E}{dx^2} &= \frac{dI}{dx} (r - j b_c); \end{aligned} \right\} \quad (3)$$

and substituting (3) in (1) and (2), we get:

$$\left. \begin{aligned} \frac{d^2 E}{dx^2} &= E(g - j b_c)(r - jx), \\ \frac{d^2 I}{dx^2} &= I(g - j b_c)(r - jx), \end{aligned} \right\} \quad (4)$$

$$\left. \begin{aligned} \frac{d^2 E}{dx^2} &= E(g - j b_c)(r - jx), \\ \frac{d^2 I}{dx^2} &= I(g - j b_c)(r - jx), \end{aligned} \right\} \quad (5)$$

the *differential equations of E and I* .

110. *These differential equations are identical, and consequently I and E are functions differing by their limiting conditions only.*

These equations, (4) and (5), are of the form:

$$\frac{d^2 w}{dx^2} = w(g - j b_c)(r - jx), \quad (6)$$

and are integrated by

$$w = a \epsilon^{vx},$$

where ϵ is the basis of natural logarithms; for, differentiating this, we get,

$$\frac{d^2 w}{dx^2} = v^2 a \epsilon^{vx} = v^2 w;$$

hence,
$$v^2 = (g - j b_c)(r - j x); \quad (7)$$

or,
$$v = \pm \sqrt{(g - j b_c)(r - j x)};$$

hence, the general integral is :

$$w = a \epsilon^{+vx} + b \epsilon^{-vx}, \quad (8)$$

where a and b are the two constants of integration ; substituting

$$v = \alpha - j\beta \quad (9)$$

into (7), we have,

$$(\alpha - j\beta)^2 = (g - j b_c)(r - j x);$$

or,

$$\left. \begin{aligned} \alpha^2 - \beta^2 &= g r - x b_c; \\ 2 \alpha \beta &= g x + b_c r; \end{aligned} \right\} \quad (b)$$

therefore,

$$\alpha^2 + \beta^2 = \sqrt{(g^2 + b_c^2)(r^2 + x^2)}; \quad (10)$$

$$\left. \begin{aligned} \alpha &= \sqrt{1/2 \{ \sqrt{(g^2 + b_c^2)(r^2 + x^2)} + (g r - b_c x) \}}; \\ \beta &= \sqrt{1/2 \{ \sqrt{(g^2 + b_c^2)(r^2 + x^2)} - (g r - b_c x) \}}; \end{aligned} \right\} \quad (11)$$

substituting (9) into (8) :

$$\begin{aligned} w &= a \epsilon^{(\alpha - j\beta)x} + b \epsilon^{-(\alpha - j\beta)x} \\ &= a \epsilon^{\alpha x} (\cos \beta x - j \sin \beta x) + b \epsilon^{-\alpha x} (\cos \beta x + j \sin \beta x); \\ w &= (a \epsilon^{\alpha x} + b \epsilon^{-\alpha x}) \cos \beta x - j (a \epsilon^{\alpha x} - b \epsilon^{-\alpha x}) \sin \beta x \end{aligned} \quad (12)$$

which is the general solution of differential equations (4) and (5)

Differentiating (8) gives :

$$dw/dx = y (a \epsilon^{vx} - b \epsilon^{-vx});$$

hence, substituting, (9) :

$$\begin{aligned} dw/dx &= (\alpha - j\beta) \{ (a \epsilon^{\alpha x} - b \epsilon^{-\alpha x}) (\cos \beta x - j) \\ &\quad (a \epsilon^{\alpha x} + b \epsilon^{-\alpha x}) \sin \beta x \}. \end{aligned} \quad (13)$$

Substituting now I for w , and substituting (13) in (1), and writing,

$$\begin{aligned} (\alpha - j\beta) a &= A, \\ (\alpha - j\beta) b &= B, \end{aligned}$$

we get :

$$\left\{ \begin{aligned} I &= \frac{1}{a-j\beta} \{ (A\epsilon^{ax} + B\epsilon^{-ax}) \cos \beta x - j(A\epsilon^{ax} - B\epsilon^{-ax}) \sin \beta x \}; \\ E &= \frac{1}{g-jb_c} \{ (A\epsilon^{ax} - B\epsilon^{-ax}) \cos \beta x - j(A\epsilon^{ax} + B\epsilon^{-ax}) \sin \beta x \}; \end{aligned} \right\} \quad (14)$$

where A and B are the constants of integration.

These are the general integral equations of the problem.

111. If —

$$\left. \begin{aligned} I_1 &= i_1 + j i_1' \text{ is the current} \\ E_1 &= e_1 + j e_1' \text{ is the E.M.F.} \end{aligned} \right\} \text{ at point, } x = 0, \quad (15)$$

by substituting (15) in (14), we get :

$$\left. \begin{aligned} 2A &= \{ (a i_1 + \beta i_1') + (g e_1 + b_c e_1') \} \\ &\quad + j \{ (a i_1' - \beta i_1) + (g e_1' - b_c e_1) \}, \\ 2B &= \{ (a i_1 + \beta i_1') - (g e_1 + b_c e_1') \} \\ &\quad + j \{ (a i_1' - \beta i_1) - (g e_1' - b_c e_1) \}, \end{aligned} \right\} \quad (16)$$

a and β being determined by equations (11).

112. If $Z = R - jX$ is the impedance of the receiver circuit, $E_o = e_o + j e_o'$ is the E.M.F. at dynamo terminals (17), and $l =$ length of line, we get

at $x = 0,$

$$I = \frac{A + B}{a - j\beta},$$

$$E = \frac{A - B}{g - j b_c};$$

hence $Z = \frac{E}{I} = \frac{A - B}{A + B} \frac{a - j\beta}{g - j b_c};$

or $\frac{A - B}{A + B} = D \frac{g - j b_c}{a - j\beta}.$ (18)

At $x = l,$

$$E_o = \frac{1}{g - j b_c} \{ (A\epsilon^{al} - B\epsilon^{-al}) \cos \beta l - j(A\epsilon^{al} + B\epsilon^{-al}) \sin \beta l \}. \quad (19)$$

Equations (18) and (19) determine the constants A and B , which, substituted in (14), give the final integral equations.

The length, $x_0 = 2\pi/\beta$ is a complete wave length (20), which means, that in the distance $2\pi/\beta$ the phases of current and E.M.F. repeat, and that in half this distance, they are just opposite.

Hence the remarkable condition exists that, in a very long line, at different points the currents at the same time flow in opposite directions, and the E.M.Fs. are opposite.

113. The difference of phase, $\hat{\omega}$, between current, I , and E.M.F., E , at any point, x , of the line, is determined by the equation,

$$D (\cos \hat{\omega} + j \sin \hat{\omega}) = \frac{E}{I},$$

where D is a constant.

Hence, $\hat{\omega}$ varies from point to point, oscillating around a medium position, $\hat{\omega}_x$, which it approaches at infinity.

This difference of phase, $\hat{\omega}_x$, towards which current and E.M.F. tend at infinity, is determined by the expression,

$$D (\cos \hat{\omega}_x + j \sin \hat{\omega}_x) = \left. \frac{E}{I} \right|_{z=\infty}$$

or, substituting for E and I their values, and since $\epsilon^{-\alpha x} = 0$, and $A \epsilon^{\alpha x} (\cos \beta x - j \sin \beta x)$, α cancels, and

$$\begin{aligned} D (\cos \hat{\omega}_x + j \sin \hat{\omega}_x) &= \frac{a - j\beta}{g - j b_c} \\ &= \frac{(ag + \beta b_c) - j(a b_c - \beta g)}{b_c^2 + g^2}; \end{aligned}$$

hence,
$$\tan \hat{\omega}_x = \frac{-a b_c + \beta g}{ag + \beta b_c}. \quad (21)$$

This angle, $\hat{\omega}_x$, = 0; that is, current and E.M.F. come more and more in phase with each other, when

$$\begin{aligned} a b_c - \beta g &= 0; \text{ that is,} \\ a \div \beta &= g \div b_c, \text{ or,} \\ \frac{a^2 - \beta^2}{2 a \beta} &= \frac{g^2 - b_c^2}{2 g b_c}; \end{aligned}$$

substituting (10), gives,

$$\frac{gr - b_c x}{gx + b_c r} = \frac{g^2 - b_c^2}{2gb_c};$$

hence, expanding, $r \div x = g \div b_c$; (22)

that is, *the ratio of resistance to inductance equals the ratio of leakage to capacity.*

This angle, $\omega_\infty = 45^\circ$; that is, current and E.M.F. differ by $\frac{1}{4}$ th period, if $-ab_c + \beta g = ag + \beta b_c$; or,

$$\frac{\alpha}{\beta} = \frac{b_c + g}{b_c + g};$$

which gives: $rg + x b_c = 0$. (23)

That is, *two of the four line constants must be zero; either g and x, or g and b_c.*

114. As an instance, in Fig. 86 a line diagram is shown, with the distances from the receiver end as abscissæ. The diagram represents one and one-half complete waves, and gives total effective current, total E.M.F., and difference of phase between both as function of the distance from receiver circuit; under the conditions,

E.M.F. at receiving end, 10,000 volts; hence, $E_1 = e_1 = 10,000$;
current at receiving end, 65 amperes, with an energy coefficient of .385,

that is, $I = i_1 + j i_1' = 25 + 60 j$;

line constants per unit length,

$$\left. \begin{aligned} r &= 1, & g &= 2 \times 10^{-5}, \\ k &= 4, & b_c &= 20 \times 10^{-5}; \end{aligned} \right\}$$

hence,

$$\left. \begin{aligned} \alpha &= 4.95 \times 10^{-3}, \\ \beta &= 28.36 \times 10^{-3}, \\ \alpha^2 + \beta^2 &= .829 \times 10^{-3}; \end{aligned} \right\}$$

$$x_o = L = \frac{2\pi}{\beta} = 221.5 = \left\{ \begin{array}{l} \text{length of line corresponding to} \\ \text{one complete period of the wave} \\ \text{of propagation.} \end{array} \right.$$

$$\left. \begin{aligned} A &= 1.012 - 1.206 j, \\ B &= .812 + .794 j. \end{aligned} \right\}$$

These values, substituted, give,

$$I = \left\{ \epsilon^{ax} (47.3 \cos \beta x + 27.4 \sin \beta x) - \epsilon^{-ax} (22.3 \cos \beta x + 32.6 \sin \beta x) \right\}$$

$$+ j \left\{ \epsilon^{ax} (27.4 \cos \beta x - 47.3 \sin \beta x) + \epsilon^{-ax} (32.6 \cos \beta x - 22.3 \sin \beta x) \right\};$$

$$E = \left\{ \epsilon^{ax} (6450 \cos \beta x + 4410 \sin \beta x) + \epsilon^{-ax} (3530 \cos \beta x - 4410 \sin \beta x) \right\}$$

$$+ j \left\{ \epsilon^{ax} (4410 \cos \beta x - 6450 \sin \beta x) - \epsilon^{-ax} (4410 \cos \beta x + 3530 \sin \beta x) \right\};$$

$$\tan \hat{\omega}_x = \frac{-ab_c + \beta g}{ag + \beta b_c} = -.073, \quad \hat{\omega}_x = -4.2^\circ.$$

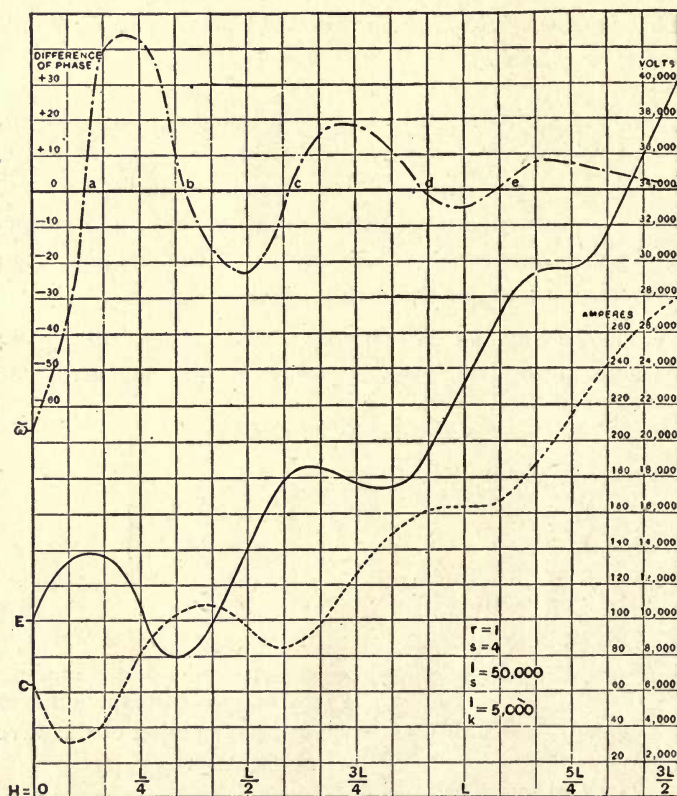


Fig. 86.

115. The following are some particular cases:

A.) *Open circuit at end of lines:*

$$x = 0: I_1 = 0.$$

$$A = (g e_1 + b_c e_1') + j(g e_1' - b_c e_1) = -R;$$

hence,

$$\left. \begin{aligned} E &= \frac{1}{g - j b_c} A \{ (\epsilon^{ax} + \epsilon^{-ax} \cos \beta x - j(\epsilon^{ax} - \epsilon^{-ax}) \sin \beta x); \\ C &= \frac{1}{a - j \beta} A \{ (\epsilon^{ax} - \epsilon^{-ax}) \cos \beta x - j(\epsilon^{ax} + \epsilon^{-ax}) \sin \beta x \}. \end{aligned} \right\}$$

B.) *Line grounded at end:*

$$x = 0: E_1 = 0.$$

$$A = (\alpha i_1 + \beta i_1') + j(\alpha i_1' - \beta i_1) = B$$

$$\left. \begin{aligned} E &= \frac{1}{g - j b_c} A \{ (\epsilon^{ax} - \epsilon^{-ax}) \cos \beta x - j(\epsilon^{ax} + \epsilon^{-ax}) \sin \beta x \}; \\ I &= \frac{1}{a - j \beta} A \{ (\epsilon^{ax} + \epsilon^{-ax}) \cos \beta x - j(\epsilon^{ax} - \epsilon^{-ax}) \sin \beta x \}. \end{aligned} \right\}$$

C.) *Infinitely long conductor:*

Replacing x by $-x$, that is, counting the distance positive in the direction of decreasing energy, we have,

$$x = \infty: I = 0, E = 0;$$

hence

$$B = 0,$$

and

$$\left. \begin{aligned} E &= \frac{1}{g - j b_c} A \epsilon^{-ax} (\cos \beta x + j \sin \beta x); \\ I &= \frac{1}{a - j \beta} A \epsilon^{-ax} (\cos \beta x + j \sin \beta x), \end{aligned} \right\}$$

involving decay of the electric wave.

The total impedance of the infinitely long conductor is

$$\begin{aligned} Z &= \frac{E}{I} \\ &= \frac{a - j \beta}{g - j b_c} \\ &= \frac{(a - j \beta)(g + j b_c)}{g^2 + b_c^2} = \frac{(ag + \beta b_c) - j(\beta g - ab_c)}{g^2 + b_c^2}. \end{aligned}$$

The infinitely long conductor acts like an impedance

$$Z = \frac{ag + \beta b_c}{g^2 + b_c^2} - j \frac{\beta g - ab_c}{g^2 + b_c^2};$$

that is, like a resistance

$$R = \frac{ag + \beta b_c}{g^2 + b_c^2},$$

combined with a reactance

$$X = \frac{\beta g - ab_c}{g^2 + b_c^2}.$$

We thus get the difference of phase between E.M.F. and current,

$$\tan \hat{\omega} = \frac{X}{R} = \frac{\beta g - ab_c}{ag + \beta b_c},$$

which is constant at all points of the line.

If $g = 0$, $x = 0$, we have,

$$a = \beta = \sqrt{\frac{b^2 r}{2}};$$

hence,

$$\begin{aligned} \tan \hat{\omega} &= 1, \text{ or,} \\ \hat{\omega} &= 45^\circ; \end{aligned}$$

that is, current and E.M.F. differ by $\frac{1}{4}$ th period.

D.) Generator feeding into closed circuit :

Let $x = 0$ be the center of cable ; then,

$$\begin{aligned} E_x &= -E_{-x}; & \text{hence: } E &= 0 \text{ at } x = 0; \\ I_x &= I_{-x}; \end{aligned}$$

which equations are the same as in *B*, where the line is grounded at $x = 0$.

CHAPTER XIII.

THE ALTERNATING-CURRENT TRANSFORMER.

116. The simplest alternating-current apparatus is the transformer. It consists of a magnetic circuit interlinked with two electric circuits, a primary and a secondary. The primary circuit is excited by an impressed E.M.F., while in the secondary circuit an E.M.F. is induced. Thus, in the primary circuit power is consumed, and in the secondary a corresponding amount of power is produced.

Since the same magnetic circuit is interlinked with both electric circuits, the E.M.F. induced per turn must be the same in the secondary as in the primary circuit; hence, the primary induced E.M.F. being approximately equal to the impressed E.M.F., the E.M.F.s. at primary and at secondary terminals have approximately the ratio of their respective turns. Since the power produced in the secondary is approximately the same as that consumed in the primary, the primary and secondary currents are approximately in inverse ratio to the turns.

117. Besides the magnetic flux interlinked with both electric circuits — which flux, in a closed magnetic circuit transformer, has a circuit of low reluctance — a magnetic cross-flux passes between the primary and secondary coils, surrounding one coil only, without being interlinked with the other. This magnetic cross-flux is proportional to the current flowing in the electric circuit, or rather, the ampere-turns or M.M.F. increase with the increasing load on the transformer, and constitute what is called the self-inductance of the transformer; while the flux surrounding both

coils may be considered as mutual inductance. This cross-flux of self-induction does not induce E.M.F. in the secondary circuit, and is thus, in general, objectionable, by causing a drop of voltage and a decrease of output; and, therefore, in the constant potential transformer the primary and secondary coils are brought as near together as possible, or even interspersed, to reduce the cross-flux.

As will be seen, by the self-inductance of a circuit, not the total flux produced by, and interlinked with, the circuit is understood, but only that (usually small) part of the flux which surrounds one circuit without interlinking with the other circuit.

118. The alternating magnetic flux of the magnetic circuit surrounding both electric circuits is produced by the combined magnetizing action of the primary and of the secondary current.

This magnetic flux is determined by the E.M.F. of the transformer, by the number of turns, and by the frequency.

If

$$\begin{aligned}\Phi &= \text{maximum magnetic flux,} \\ N &= \text{frequency,} \\ n &= \text{number of turns of the coil;}\end{aligned}$$

the E.M.F. induced in this coil is

$$\begin{aligned}E &= \sqrt{2} \pi N n \Phi 10^{-8} \text{ volts,} \\ &= 4.44 N n \Phi 10^{-8} \text{ volts;}\end{aligned}$$

hence, if the E.M.F., frequency, and number of turns are determined, the maximum magnetic flux is

$$\Phi = \frac{E 10^8}{\sqrt{2} \pi N n}.$$

To produce the magnetism, Φ , of the transformer, a M.M.F. of \mathcal{F} ampere-turns is required, which is determined by the shape and the magnetic characteristic of the iron, in the manner discussed in Chapter X.

For instance, in the closed magnetic circuit transformer, the maximum magnetic induction is

$$\mathfrak{B} = \frac{\Phi}{S},$$

where S = the cross-section of magnetic circuit.

119. To induce a magnetic density, \mathfrak{B} , a M.M.F. of \mathfrak{F}_m ampere-turns maximum is required, or, $\mathfrak{F}_m / \sqrt{2}$ ampere-turns effective, per unit length of the magnetic circuit; hence, for the total magnetic circuit, of length, l ,

$$\mathfrak{F} = \frac{l\mathfrak{F}_m}{\sqrt{2}} \text{ ampere-turns};$$

or

$$I = \frac{\mathfrak{F}}{n} = \frac{l\mathfrak{F}_m}{n\sqrt{2}} \text{ amps. eff.},$$

where n = number of turns.

At no load, or open secondary circuit, this M.M.F., \mathfrak{F} , is furnished by the *exciting current*, I_{oo} , improperly called the *leakage-current*, of the transformer; that is, that small amount of primary current which passes through the transformer at open secondary circuit.

In a transformer with open magnetic circuit, such as the "hedgehog" transformer, the M.M.F., \mathfrak{F} , is the sum of the M.M.F. consumed in the iron and in the air part of the magnetic circuit (see Chapter X.).

The energy of the exciting current is the energy consumed by hysteresis and eddy currents and the small ohmic loss.

The exciting current is not a sine wave, but is, at least in the closed magnetic circuit transformer, greatly distorted by hysteresis, though less so in the open magnetic circuit transformer. It can, however, be represented by an equivalent sine wave, I_{oo} , of equal intensity and equal power with the distorted wave, and a wattless higher harmonic, mainly of triple frequency.

Since the higher harmonic is small compared with the

that is, counting the time from the moment where the rising magnetism passes its zero value.

Then the resultant M.M.F. is represented by the vector $\overline{O\mathfrak{F}}$, leading $\overline{O\Phi}$ by the angle $\mathfrak{F}O\Phi = \omega$.

The induced E.M.F.s. have the phase 180° , that is, are plotted towards the left, and represented by the vectors $\overline{OE'_o}$ and $\overline{OE'_1}$.

If, now, $\hat{\omega}'_1 =$ angle of lag in the secondary circuit, due to the total (internal and external) secondary reactance, the secondary current I_1 , and hence the secondary M.M.F., $\mathfrak{F}_1 = n_1 I_1$, will lag behind E'_1 by an angle β' , and have the phase, $180^\circ + \beta'$, represented by the vector $\overline{O\mathfrak{F}_1}$. Constructing a parallelogram of M.M.F.s., with $\overline{O\mathfrak{F}}$ as a diagonal and $\overline{O\mathfrak{F}_1}$ as one side, the other side or $\overline{O\mathfrak{F}_o}$ is the primary M.M.F., in intensity and phase, and hence, dividing by the number of primary turns, n_o , the primary current is $I_o = \mathfrak{F}_o / n_o$.

To complete the diagram of E.M.F.s., we have now, —

In the primary circuit :

E.M.F. consumed by resistance is $I_o r_o$, in phase with I_o , and represented by the vector $\overline{OE_{or}}$;

E.M.F. consumed by reactance is $I_o x_o$, 90° ahead of I_o , and represented by the vector $\overline{OE_{ox}}$;

E.M.F. consumed by induced E.M.F. is E_o , equal and opposite thereto, and represented by the vector $\overline{OE'_o}$.

Hence, the total primary impressed E.M.F. by combination of $\overline{OE_{or}}$, $\overline{OE_{ox}}$, and $\overline{OE'_o}$ by means of the parallelogram of E.M.F.s. is,

$$E_o = \overline{OE_o},$$

and the difference of phase between the primary impressed E.M.F. and the primary current is

$$\beta_o = E_o O\mathfrak{F}_o.$$

In the secondary circuit :

Counter E.M.F. of resistance is $I_1 r_1$ in opposition with I_1 , and represented by the vector $\overline{OE'_1 r'}$;

magnitude as not to be easily represented on the same scale; or the primary circuit may be reduced to the secondary in the same way. In either case, the vectors representing the two induced E.M.Fs. coincide, or $\overline{OE}_1' = \overline{OE}_o'$.

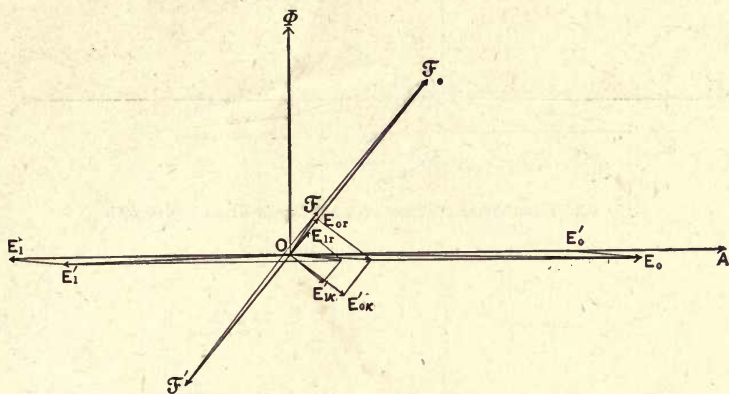


Fig. 89. Transformer Diagram with 50° Lag in Secondary Circuit.

Figs. 88 to 94 give the polar diagram of a transformer having the constants —

- | | |
|----------------------|---------------------|
| $r_o = .2$ ohms, | $b_o = .0173$ mhos, |
| $x_o = .33$ ohms, | $E_1' = 100$ volts, |
| $r_1 = .00167$ ohms, | $I_1 = 60$ amperes, |
| $x_1 = .0025$ ohms, | $a = 10.$ |
| $g_o = .0100$ mhos, | |

for the conditions of secondary circuit,

- | | | | |
|---------------------------|-------------|----------------------------|-------------|
| $\beta_1' = 80^\circ$ lag | in Fig. 88. | $\beta_1' = 20^\circ$ lead | in Fig. 92. |
| 50° lag | “ 89. | 50° lead | “ 93. |
| 20° lag | “ 90. | 80° lead | “ 94. |
| O , or in phase, | “ 91. | | |

As shown with a change of β_1' , E_o , g_1 , g_o , etc., change in intensity and direction. The locus described by them are circles, and are shown in Fig. 95, with the point corresponding to non-inductive load marked. The part of the locus corresponding to a lagging secondary current is

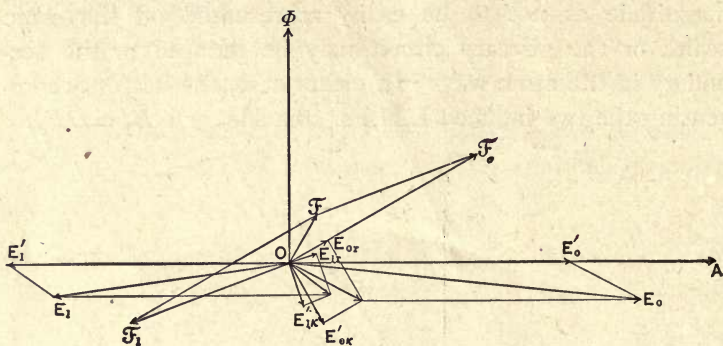


Fig. 90. Transformer Diagram with 20° Lag in Secondary Circuit.

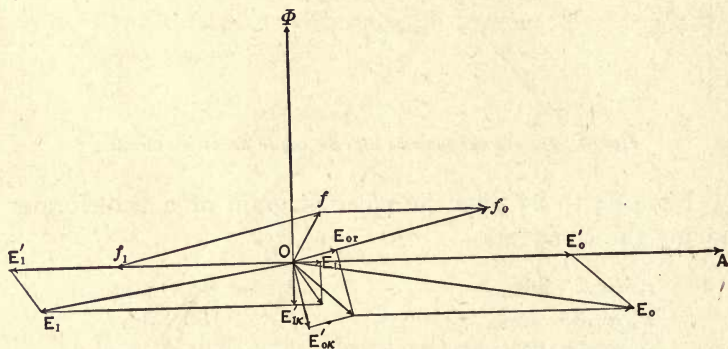


Fig. 91. Transformer Diagram with Secondary Current in Phase with E.M.F.

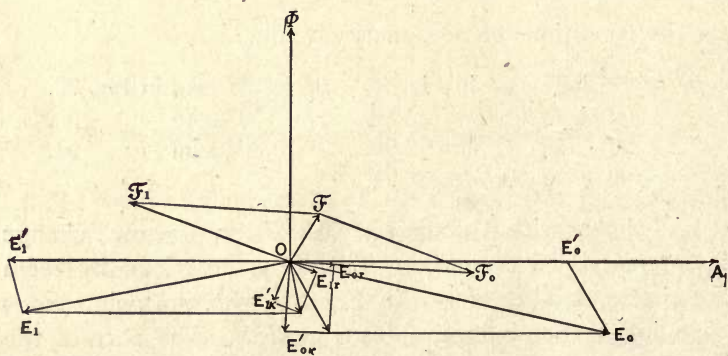


Fig. 92. Transformer Diagram with 20° Lead in Secondary Current.

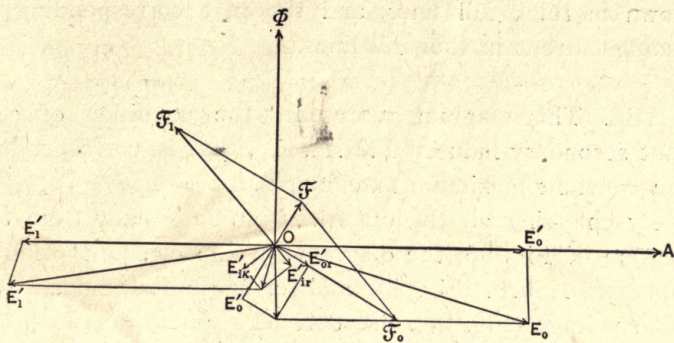


Fig. 93. Transformer Diagram with 50° Lead in Secondary Circuit.

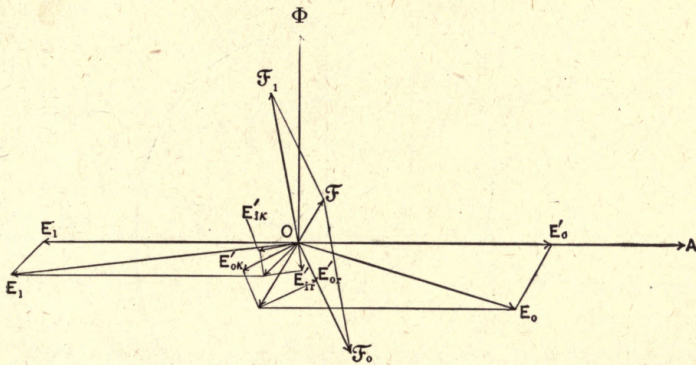


Fig. 94. Transformer Diagram with 80° Lead in Secondary Circuit.

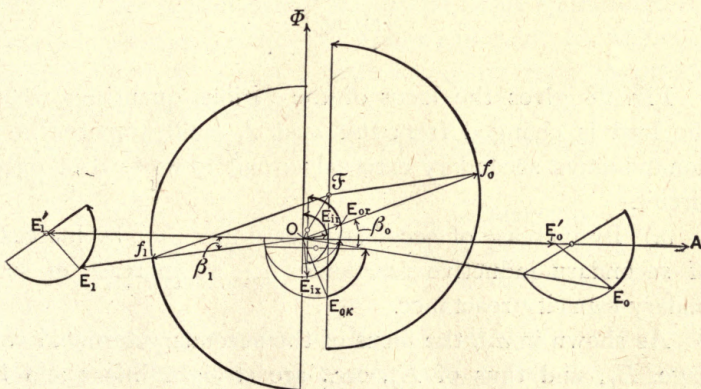


Fig. 95.

shown in thick full lines, and the part corresponding to leading current in thin full lines.

122. This diagram represents the condition of constant secondary induced E.M.F., E_1' , that is, corresponding to a constant maximum magnetic flux.

By changing all the quantities proportionally from the diagram of Fig. 95, the diagram for the constant primary impressed E.M.F. (Fig. 96), and for constant secondary terminal voltage (Fig. 97), are derived. In these cases, the locus gives curves of higher order.

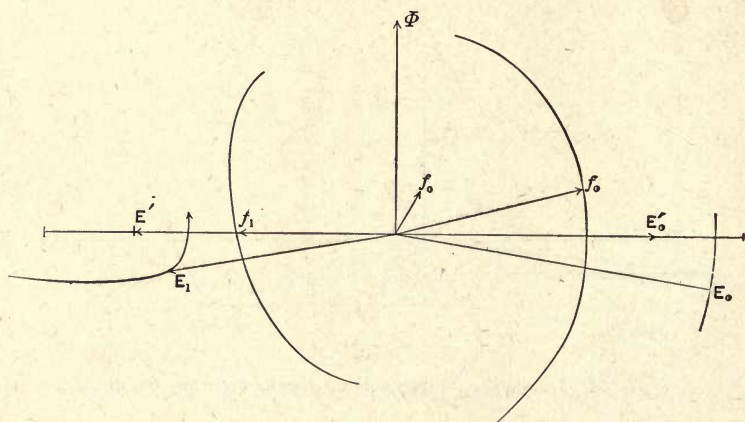


Fig. 96.

Fig. 98 gives the locus of the various quantities when the load is changed from full load, $I_1 = 60$ amperes in a non-inductive secondary external circuit to no load or open circuit.

a.) By increase of secondary resistance; *b.*) by increase of secondary inductive reactance; *c.*) by increase of secondary capacity reactance.

As shown in *a.*), the locus of the secondary terminal voltage, E_1 , and thus of E_0 , etc., are straight lines; and in *b.*) and *c.*), parts of one and the same circle *a.*) is shown

in full lines, *b.*) in heavy full lines, and *c.*) in light full lines. This diagram corresponds to constant maximum magnetic flux; that is, to constant secondary induced E.M.F. The diagrams representing constant primary impressed E.M.F. and constant secondary terminal voltage can be derived from the above by proportionality.

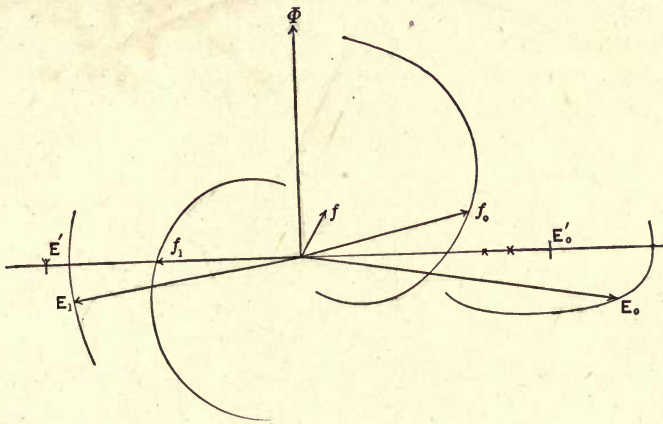


Fig. 97.

123. It must be understood, however, that for the purpose of making the diagrams plainer, by bringing the different values to somewhat nearer the same magnitude, the constants chosen for these diagrams represent, not the magnitudes found in actual transformers, but refer to greatly exaggerated internal losses.

In practice, about the following magnitudes would be found:

$r_o = .01$ ohms;	$x_1 = .00025$ ohms;
$x_o = .033$ ohms;	$g_o = .001$ ohms;
$r_1 = .00008$ ohms;	$b_o = .00173$ ohms;

that is, about one-tenth as large as assumed. Thus the changes of the values of E_o , E_1 , etc., under the different conditions will be very much smaller.

Symbolic Method.

124. In symbolic representation by complex quantities the transformer problem appears as follows :

The exciting current, I_{00} , of the transformer depends upon the primary E.M.F., which dependence can be represented by an admittance, the "primary admittance," $Y_o = g_o + jb_o$, of the transformer.

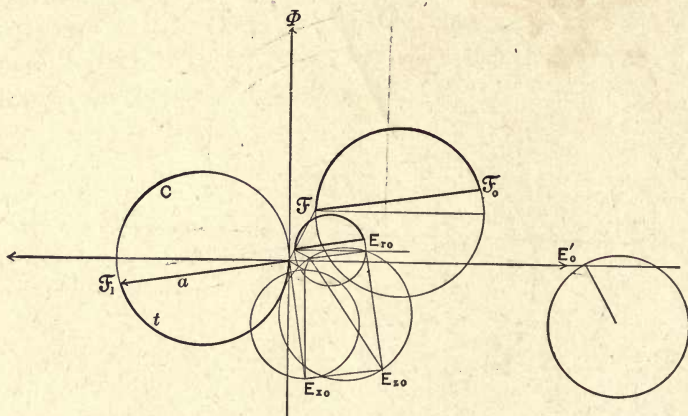


Fig. 98.

The resistance and reactance of the primary and the secondary circuit are represented in the impedance by

$$Z_o = r_o - jx_o, \quad \text{and} \quad Z_1 = r_1 - jx_1.$$

Within the limited range of variation of the magnetic density in a constant potential transformer, admittance and impedance can usually, and with sufficient exactness, be considered as constant.

Let

n_o = number of primary turns in series ;

n_1 = number of secondary turns in series ;

$a = \frac{n_o}{n_1}$ = ratio of turns ;

$Y_o = g_o - jb_o$ = primary admittance

$$= \frac{\text{Exciting current}}{\text{Primary counter E.M.F.}} ;$$

$$Z_o = r_o - jx_o = \text{primary impedance}$$

$$= \frac{\text{E.M.F. consumed in primary coil by resistance and reactance;}}{\text{Primary current}}$$

$$Z_1 = r_1 - jx_1 = \text{secondary impedance}$$

$$= \frac{\text{E.M.F. consumed in secondary coil by resistance and reactance;}}{\text{Secondary current}}$$

where the reactances, x_o and x_1 , refer to the true self-inductance only, or to the cross-flux passing between primary and secondary coils; that is, interlinked with one coil only.

Let also

$$Y = g + jb = \text{total admittance of secondary circuit, including the internal impedance;}$$

$$E_o = \text{primary impressed E.M.F. ;}$$

$$E_o' = \text{E.M.F. consumed by primary counter E.M.F. ;}$$

$$E_1 = \text{secondary terminal voltage;}$$

$$E_1' = \text{secondary induced E.M.F. ;}$$

$$I_o = \text{primary current, total;}$$

$$I_{oo} = \text{primary exciting current ;}$$

$$I_1 = \text{secondary current.}$$

Since the primary counter E.M.F., E_o' , and the secondary induced E.M.F., E_1' , are proportional by the ratio of turns, a ,

$$E_o' = -a E_1'. \tag{1}$$

The secondary current is :

$$I_1 = Y E_1', \tag{2}$$

consisting of an energy component, $g E_1'$, and a reactive component, $j E_1'$.

To this secondary current corresponds the component of primary current,

$$I_o' = \frac{-Y E_1'}{a} = \frac{Y E_o'}{a^2}. \tag{3}$$

The primary exciting current is —

$$I_{oo} = Y_o E_o'. \tag{4}$$

Hence, the total primary current is :

$$I_o = I_o' + I_{oo}$$

$$= \frac{Y E_o'}{a^2} + Y_o E_o', \tag{5}$$

$$\begin{aligned} \text{or, } I_o &= \frac{E_o'}{a^2} \{Y + a^2 Y_o\} \\ &= -\frac{E_1'}{a} \{Y + a^2 Y_o\} \end{aligned} \quad (6)$$

The E.M.F. consumed in the secondary coil by the internal impedance is $Z_1 I_1$.

The E.M.F. induced in the secondary coil by the magnetic flux is E_1' .

Therefore, the secondary terminal voltage is

$$E_1 = E_1' - Z_1 I_1,$$

or, substituting (2), we have

$$E_1 = E_1' \{1 - Z_1 Y\} \quad (7)$$

The E.M.F. consumed in the primary coil by the internal impedance is $Z_o I_o$.

The E.M.F. consumed in the primary coil by the counter E.M.F. is E_o' .

Therefore, the primary impressed E.M.F. is

$$E_o = E_o' + Z_o I_o,$$

or, substituting (6),

$$\left. \begin{aligned} E_o &= E_o' \left\{ 1 + Z_o Y_o + \frac{Z_o Y}{a^2} \right\} \\ &= -a E_1' \left\{ 1 + Z_o Y_o + \frac{Z_o Y}{a^2} \right\}. \end{aligned} \right\} \quad (8)$$

125. We thus have,

$$\text{primary E.M.F., } E_o = -a E_1' \left\{ 1 + Z_o Y_o + \frac{Z_o Y}{a^2} \right\}, \quad (8)$$

$$\text{secondary E.M.F., } E_1 = E_1' \{1 - Z_1 Y\}, \quad (7)$$

$$\text{primary current, } I_o = -\frac{E_1'}{a} \{Y + a^2 Y_o\}, \quad (6)$$

$$\text{secondary current, } I_1 = Y E_1', \quad (2)$$

as functions of the secondary induced E.M.F., E_1' , as parameter.

From the above we derive

Ratio of transformation of E.M.Fs. :

$$\frac{E_o}{E_1} = -a \frac{1 + Z_o Y_o + \frac{Z_o Y}{a^2}}{1 - Z_1 Y} \quad (9)$$

Ratio of transformations of currents :

$$\frac{I_o}{I_1} = -\frac{1}{a} \left\{ 1 + a^2 \frac{Y_o}{Y} \right\} \quad (10)$$

From this we get, at constant primary impressed E.M.F.,

$$E_o = \text{constant};$$

secondary induced E.M.F.,

$$E_1' = -\frac{E_o}{a} \frac{1}{1 + Z_o Y_o + \frac{Z_o Y}{a^2}};$$

E.M.F. induced per turn,

$$\delta E = -\frac{E_o}{n_o} \frac{1}{1 + Z_o Y_o + \frac{Z_o Y}{a^2}};$$

secondary terminal voltage,

$$E_1 = -\frac{E_o}{a} \frac{1 - Z_o Y}{1 + Z_o Y_o + \frac{Z_o Y}{a^2}};$$

primary current,

$$I_o = \frac{E_o}{a^2} \frac{Y + a^2 Y_o}{1 + Z_o Y_o + \frac{Z_o Y}{a^2}} = E_o \frac{\frac{Y}{a^2} + Y_o}{1 + Z_o Y_o + \frac{Z_o Y}{a^2}};$$

secondary current,

$$I_1 = -\frac{E_o}{a} \frac{Y}{1 + Z_o Y_o + \frac{Z_o Y}{a^2}}.$$

At constant secondary terminal voltage,

$$E_1 = \text{const.};$$

secondary induced E.M.F.,

$$E_1' = \frac{E_1}{1 - Z_1 Y};$$

E.M.F. induced per turn,

$$\delta E = \frac{E_1}{n_1} \frac{1}{1 - Z_1 Y};$$

primary impressed E.M.F.,

$$E_o = -aE_1 \frac{1 + Z_o Y_o + \frac{Z_o Y}{a^2}}{1 - Z_1 Y};$$

primary current,

$$I_o = -\frac{E_1}{a} \frac{Y + a^2 Y_o}{1 - Z_1 Y};$$

secondary current,

$$I_1 = E_1 \frac{Y}{1 - Z_1 Y}.$$

(12)

126. Some interesting conclusions can be drawn from these equations.

The apparent impedance of the total transformer is

$$Z_t = \frac{E_o}{I_o} = a^2 \frac{1 + Z_o Y_o + \frac{Z_o Y}{a^2}}{Y + a^2 Y_o} \quad (13)$$

$$= \frac{1 + Z_o \left(Y_o + \frac{Y}{a^2} \right)}{Y_o + \frac{Y}{a^2}};$$

$$Z_t = \frac{1}{Y_o + \frac{Y}{a^2}} + Z_o. \quad (14)$$

Substituting now, $\frac{Y}{a^2} = Y'$, the total secondary admittance, reduced to the primary circuit by the ratio of turns, it is

$$Z_t = \frac{1}{Y_o + Y'} + Z_o. \quad (15)$$

$Y_o + Y'$ is the total admittance of a divided circuit with the exciting current, of admittance Y_o , and the secondary

current, of admittance Y' (reduced to primary), as branches. Thus :

$$\frac{1}{Y_o + Y'} = Z_o' \tag{16}$$

is the impedance of this divided circuit, and

$$Z_o = Z_o' + Z_o. \tag{17}$$

That is :

The alternate-current transformer, of primary admittance Y_o , total secondary admittance Y , and primary impedance Z_o , is equivalent to, and can be replaced by, a divided circuit with the branches of admittance Y_o , the exciting current, and admittance $Y' = Y/a^2$, the secondary current, fed over mains of the impedance Z_o , the internal primary impedance.

This is shown diagrammatically in Fig. 99.

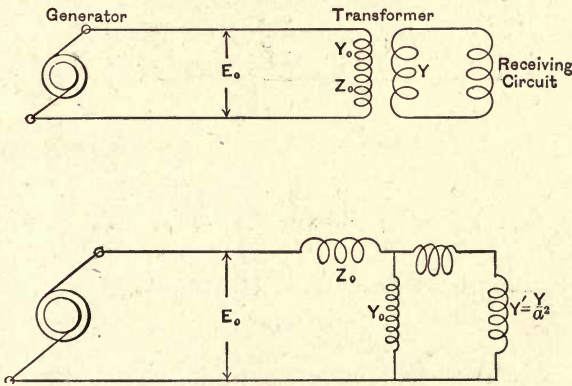


Fig. 99.

127. Separating now the internal secondary impedance from the external secondary impedance, or the impedance of the consumer circuit, it is

$$\frac{1}{Y} = Z_1 + Z; \tag{18}$$

where Z = external secondary impedance,

$$Z = \frac{E_1}{I_1}. \tag{19}$$

Reduced to primary circuit, it is

$$\begin{aligned} \frac{1}{Y'} &= \frac{a^2}{Y} = a^2 Z_1 + a^2 Z \\ &= Z_1' + Z'. \end{aligned} \quad (20)$$

That is :

An alternate-current transformer, of primary admittance Y_0 , primary impedance Z_0 , secondary impedance Z_1 , and ratio of turns a , can, when the secondary circuit is closed by an impedance Z (the impedance of the receiver circuit), be replaced, and is equivalent to a circuit of impedance $Z' = a^2 Z$, fed over mains of the impedance $Z_0 + Z_1'$, where $Z_1' = a^2 Z_1$, shunted by a circuit of admittance Y_0 , which latter circuit branches off at the points $a - b$, between the impedances Z_0 and Z_1' .

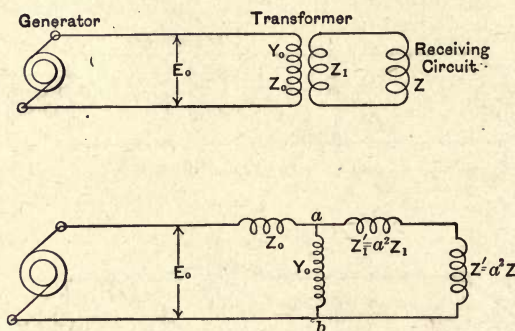


Fig. 100.

This is represented diagrammatically in Fig. 100.

It is obvious therefore, that if the transformer contains several independent secondary circuits they are to be considered as branched off at the points $a - b$, in diagram Fig. 100, as shown in diagram Fig. 101.

It therefore follows :

An alternate-current transformer, of x secondary coils, of the internal impedances $Z_1^I, Z_1^{II}, \dots, Z_1^x$, closed by external secondary circuits of the impedances Z^I, Z^{II}, \dots, Z^x , is equivalent to a divided circuit of $x + 1$ branches, one branch of

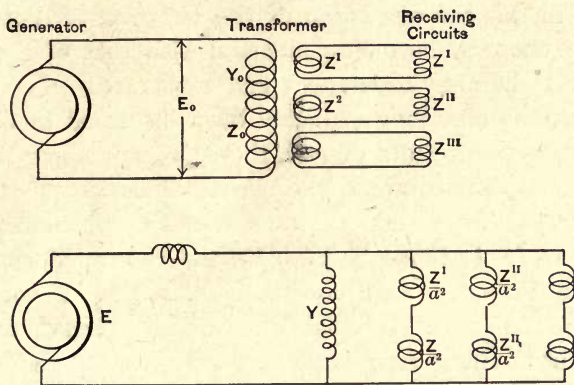


Fig. 101.

admittance Y_0 , the exciting current, the other branches of the impedances $Z_1^I + Z^I$, $Z_1^{II} + Z^{II}$, . . . $Z_1^x + Z^x$, the latter impedances being reduced to the primary circuit by the ratio of turns, and the whole divided circuit being fed by the primary impressed E.M.F. E_0 , over mains of the impedance Z_0 .

Consequently, transformation of a circuit merely changes all the quantities proportionally, introduces in the mains the impedance $Z_0 + Z_1'$, and a branch circuit between Z_0 and Z_1' , of admittance Y_0 .

Thus, double transformation will be represented by diagram, Fig. 102.

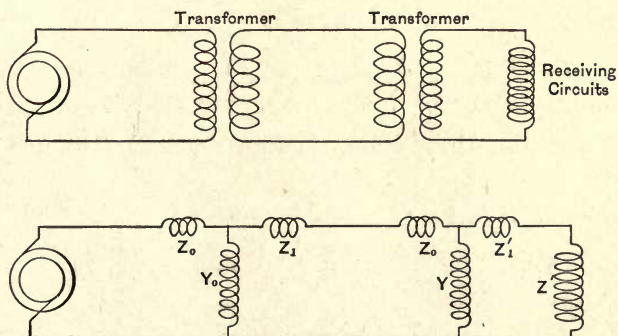


Fig. 102.

With this the discussion of the alternate-current transformer ends, by becoming identical with that of a divided circuit containing resistances and reactances.

Such circuits have explicitly been discussed in Chapter VIII., and the results derived there are now directly applicable to the transformer, giving the variation and the control of secondary terminal voltage, resonance phenomena, etc.

Thus, for instance, if $Z_1' = Z_o$, and the transformer contains a secondary coil, constantly closed by a condenser reactance of such size that this auxiliary circuit, together with the exciting circuit, gives the reactance $-x_o$, with a non-inductive secondary circuit $Z_1 = r_1$, we get the condition of transformation from constant primary potential to constant secondary current, and inversely, as previously discussed.

Non-inductive Secondary Circuit.

128. In a non-inductive secondary circuit, the external secondary impedance is,

$$Z = R_1,$$

or, reduced to primary circuit,

$$\frac{Z}{a^2} = \frac{R_1}{a^2} = R.$$

Assuming the secondary impedance, reduced to primary circuit, as equal to the primary impedance,

$$a^2 Z_1 = Z_o = r_o - jx_o,$$

it is,

$$\frac{Y}{a^2} = \frac{1}{a^2(Z + Z_1)} = \frac{1}{R + r_o - jx_o}.$$

Substituting these values in Equations (9), (10), and (13), we have

Ratio of E.M.Fs. :

$$\frac{E_o}{E_1} = -a \frac{1 + \frac{r_o - jx_o}{R + r_o - jx_o} + (r_o - jx_o)(g_o + jb_o)}{1 - \frac{(r_o - jx_o)}{R + r_o - jx_o}}$$

$$= -a \left\{ 1 + \frac{r_o - jx_o}{R + r_o - jx_o} + (r_o - jx_o)(g_o + jb_o) \right\} \left\{ 1 + \frac{r_o - jx_o}{R + r_o - jx_o} + \left(\frac{r_o - jx_o}{R + r_o - jx_o} \right)^2 + \dots \right\};$$

or, expanding, and neglecting terms of higher than third order,

$$\frac{E_o}{E_1} = -a \left\{ 1 + 2 \frac{r_o - jx_o}{R + r_o - jx_o} + 2 \left(\frac{r_o - jx_o}{R + r_o - jx_o} \right)^2 + (r_o - jx_o)(g_o + jb_o) \right\};$$

or, expanded,

$$\frac{E_o}{E_1} = -a \left\{ 1 + 2 \frac{r_o - jx_o}{R} + (r_o - jx_o)(g_o + jb_o) \right\}$$

Neglecting terms of tertiary order also,

$$\frac{E_o}{E_1} = -a \left\{ 1 + 2 \frac{r_o - jx_o}{R} \right\}.$$

Ratio of currents :

$$\frac{I_o}{I_1} = -\frac{1}{a} \{ 1 + (g_o + jb_o)(R + r_o - jx_o) \};$$

or, expanded,

$$\frac{I_o}{I_1} = -\frac{1}{a} \{ 1 + R(g_o + jb_o) + (r_o - jx_o)(g_o + jb_o) \}.$$

Neglecting terms of tertiary order also,

$$\frac{I_o}{I_1} = -\frac{1}{a} \{ 1 + R(g_o + jb_o) \}.$$

Total apparent primary admittance :

$$Z_t \equiv \frac{E_o}{I_o} = \frac{1 + \frac{r_o - jx_o}{R + r_o - jx_o} + (r_o - jx_o)(g_o + jb_o)}{\frac{1}{R + r_o - jx_o} + g_o + jb_o}$$

$$= \{ R + (r_o - jx_o) + R(r_o - jx_o)(g_o + jb_o) \} \{ 1 - (g_o + jb_o)(R + r_o - jx_o) + (g_o + jb_o)^2(R + r_o - jx_o)^2 + \dots \}$$

$$= \{ R + 2(r_o - jx_o) - R^2(g_o + jb_o) - 2R(r_o - jx_o)(g_o + jb_o) + R^3(g_o + jb_o)^2 \};$$

or,

$$Z_t = R \left\{ 1 + 2 \frac{r_o - jx_o}{R} - R(g_o + jb_o) - 2(r_o - jx_o)(g_o + jb_o) + R^2(g_o + jb_o)^2 \right\}.$$

Neglecting terms of tertiary order also :

$$Z_t = R \left\{ 1 + 2 \frac{r_o - jx_o}{R} - R(g_o + jb_o) \right\}.$$

Angle of lag in primary circuit :

$$\tan \hat{\omega}_o = \frac{x_t}{r_t}, \text{ hence,}$$

$$\tan \hat{\omega}_o = \frac{2 \frac{x_o}{R} + Rb_o + 2r_ob_o - 2x_og_o - 2R^2g_ob_o}{1 + 2 \frac{r_o}{R} - Rg_o - 2r_og_o - 2x_ob_o + R^2g_o^2 + R_1^2b_o^2}.$$

Neglecting terms of tertiary order also :

$$\tan \hat{\omega}_o = \frac{2 \frac{x_o}{R} + Rb_o}{1 + 2 \frac{r_o}{R} - Rg_o}.$$

129. If, now, we represent the external resistance of the secondary circuit at full load (reduced to the primary circuit) by R_o , and denote,

$$\frac{2r_o}{R_o} = p = \text{ratio} \frac{\text{Internal resistance of transformer}}{\text{External resistance of secondary circuit}} = \text{percentage internal resistance,}$$

$$\frac{2x_o}{R_o} = q = \text{ratio} \frac{\text{Internal reactance of transformer}}{\text{External resistance of secondary circuit}} = \text{percentage internal reactance,}$$

$$R_og_o = h = \text{ratio} \frac{\text{Hysteretic energy current}}{\text{Total secondary current}} = \text{percentage hysteresis,}$$

$$R_ob_o = g = \text{ratio} \frac{\text{Magnetizing current}}{\text{Total secondary current}} = \text{percentage magnetizing current,}$$

and if d represents the load of the transformer, as fraction of full load, we have

$$R = \frac{R_o}{d},$$

$$\text{and,} \quad \begin{aligned} \frac{2 r_o}{R} &= p d, \\ \frac{2 x_o}{R} &= q d, \\ R g_o &= \frac{h}{d}, \\ R b_o &= \frac{g}{d}. \end{aligned}$$

Substituting these values we get, as the equations of the transformer on non-inductive load,

Ratio of E.M.Fs. :

$$\begin{aligned} \frac{E_o}{E_1} &= -a \left\{ 1 + d(p - jq) + \frac{(p - jq)(h + jg)}{2} \right\} \\ &\cong -a \{ 1 + d(p - jq) \} \end{aligned}$$

or, eliminating imaginary quantities,

$$\begin{aligned} \frac{e_o}{e_1} &= a \sqrt{\left(1 + dp + \frac{ph + qg'}{2} \right)^2 + \left(dq - \frac{pg - qh}{2} \right)^2} \\ &\cong a \sqrt{(1 + dp)^2 + d^2 q^2} \\ &\cong a \left\{ 1 + dp + \frac{ph + qg' + d^2 q^2}{2} \right\} \\ &\cong a \{ 1 + dp \}. \end{aligned}$$

Ratio of currents :

$$\begin{aligned} \frac{I_o}{I_1} &= -\frac{1}{a} \left\{ 1 + \frac{(h + jg)}{d} + \frac{(p - jq)(h + jg)}{2} \right\} \\ &\cong -\frac{1}{a} \left\{ 1 + \left(\frac{h + jg}{d} \right) \right\}; \end{aligned}$$

or, eliminating imaginary quantities,

$$\begin{aligned} \frac{i_o}{i_1} &= \frac{1}{a} \sqrt{\left(1 + \frac{h}{d} + \frac{ph + qg}{2} \right)^2 + \left(\frac{g}{d} + \frac{pg - qh}{2} \right)^2} \\ &\cong \frac{1}{a} \sqrt{\left(1 + \frac{h}{d} \right)^2 + \left(\frac{g}{d} \right)^2} \\ &\cong \frac{1}{a} \left\{ 1 + \frac{h}{d} + \frac{ph + qg + g^2}{2d^2} \right\} \\ &\cong \frac{1}{a} \left\{ 1 + \frac{h}{d} \right\}. \end{aligned}$$

Total apparent primary impedance :

$$\begin{aligned} Z_t &= \frac{R_o}{d} \left\{ 1 + d(p - jg) - \frac{h + jg}{d} - (p - jg)(h + jg) + \left(\frac{h + jg}{d^2} \right)^2 \right\} \\ &\approx \frac{R_o}{d} \left\{ 1 + d(p - jg) - \frac{h + jg'}{d} \right\} \end{aligned}$$

or, eliminating imaginary quantities,

$$\begin{aligned} Z_t &= \frac{R_o}{d} \sqrt{\left(1 + dp - \frac{h}{d} - ph - qg + \frac{h^2 - g^2}{d^2} \right)^2 + \left(dq - \frac{g}{d} - pg + gh + 2 \frac{hg}{d^2} \right)^2} \\ &\approx \frac{R_o}{d} \sqrt{\left(1 + dp - \frac{h}{d} \right)^2 + \left(dq - \frac{g}{d} \right)^2} \\ &\approx \frac{R_o}{d} \left\{ 1 + dp - \frac{h}{d} - ph - 2qg + \frac{h^2 - g^2}{d^2} + \frac{d^2 q^2}{2} + \frac{g^2}{2d^2} \right. \\ &\quad \left. + \frac{d^2 p^2}{2} + \frac{h^2}{2d^2} \right\} \\ &\approx \frac{R_o}{d} \left\{ 1 + dp - \frac{h}{d} \right\} . \end{aligned}$$

Angle of lag in primary circuit :

$$\begin{aligned} \tan \hat{\omega}_o &= \frac{dq + \frac{g}{d} + pg - gh - 2 \frac{hg}{d^2}}{1 + dp - \frac{h}{d} - ph - qg + \frac{hg}{d} \frac{h^2 + g^2}{d^2}} \\ &\approx \frac{dg + \frac{g}{d}}{1 + dp - \frac{h}{d}} . \end{aligned}$$

That is,

An alternate-current transformer, feeding into a non-inductive secondary circuit, is represented by the constants :

- R_o = secondary external resistance at full load ;
- p = percentage resistance ;
- q = percentage reactance ;
- h = percentage hysteresis ;
- g = percentage magnetizing current ;
- d = secondary percentage load.

All these qualities being considered as reduced to the primary circuit by the square of the ratio of turns, a^2 .

130. As an instance, a transformer of the following constants may be given:

$$\begin{array}{lll}
 e_o = 1,000; & R_o = 120; & q = .06; \\
 a = 10; & p = .02 & h = .02; \\
 & & g = .04.
 \end{array}$$

Substituting these values, gives:

$$\begin{aligned}
 e_1 &= \frac{100}{\sqrt{(1.0014 + .02 d)^2 + (.0002 + .06 d)^2}}; \\
 c_1 &= \frac{e_1 d a^2}{R_o} = \frac{e_1 d}{1.2}; \\
 c_o &= .1 c_1 \sqrt{\left(1.0014 + \frac{.02}{d}\right)^2 + \left(\frac{.04}{d} - .0002\right)^2}; \\
 \tan \hat{\omega}_o &= \frac{.06 d + \frac{.04}{d} - .0004 - \frac{.0016}{d^2}}{1.9972 + .02 d + \frac{.002}{d^2} - \frac{.02}{d}}.
 \end{aligned}$$

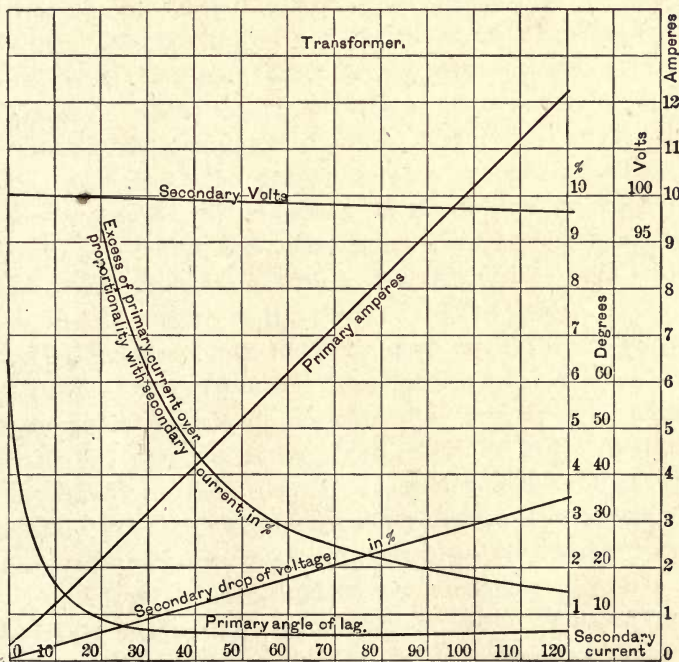


Fig. 103. Load Diagram of Transformer.

In diagram Fig. 103 are shown, for the values from $d = 0$ to $d = 1.5$, with the secondary current c_1 as abscissæ, the values :

- secondary terminal voltage, in volts,
- secondary drop of voltage, in per cent,
- primary current, in amps,
- excess of primary current over proportionality with secondary, in per cent,
- primary angle of lag.

The power-factor of the transformer, $\cos \hat{\omega}_0$, is .45 at open secondary circuit, and is above .99 from 25 amperes, upwards, with a maximum of .995 at full load.

CHAPTER XIV.

THE GENERAL ALTERNATING-CURRENT TRANSFORMER.

131. THE simplest alternating-current apparatus is the alternating-current transformer. It consists of a magnetic circuit, interlinked with two electric circuits or sets of electric circuits. The one, the primary circuit, is excited by an impressed E.M.F., while in the other, the secondary circuit, an E.M.F. is induced. Thus, in the primary circuit, power is consumed, in the secondary circuit a corresponding amount of power produced; or in other words, power is transferred through space, from primary to secondary circuit. This transfer of power finds its mechanical equivalent in a repulsive thrust acting between primary and secondary. Thus, if the secondary coil is not held rigidly as in the stationary transformer, it will be repelled and move away from the primary. This mechanical effect is made use of in the induction motor, which represents a transformer whose secondary is mounted movably with regard to the primary in such a way that, while set in rotation, it still remains in the primary field of force.

The condition that the secondary circuit, while moving with regard to the primary, does not leave the primary field of magnetic force, requires that this field is not undirectional, but that an active field exists in every direction. One way of producing such a magnetic field is by exciting different primary circuits angularly displaced in space with each other by currents of different phase. Another way is to excite the primary field in one direction only, and get the cross magnetization, or the angularly displaced magnetic field, by the reaction of the secondary current.

We see, consequently, that the stationary transformer and the induction motor are merely different applications of the same apparatus, comprising a magnetic circuit interlinked with two electric circuits. Such an apparatus can properly be called a "*general alternating-current transformer.*"

The equations of the stationary transformer and those of the induction motor are merely specializations of the general alternating-current transformer equations.

Quantitatively the main differences between induction motor and stationary transformer are those produced by the air-gap between primary and secondary, which is required to give the secondary mechanical movability. This air-gap greatly increases the magnetizing current over that in the closed magnetic circuit transformer, and requires an ironclad construction of primary and secondary to keep the magnetizing current within reasonable limits. An ironclad construction again greatly increases the self-induction of primary and secondary circuit. Thus the induction motor is a transformer of large magnetizing current and large self-induction; that is, comparatively large primary susceptance and large reactance.

The general alternating-current transformer transforms between electrical and mechanical power, and changes not only E.M.F.s. and currents, but frequencies also.

132. Besides the magnetic flux interlinked with both primary and secondary electric circuit, a magnetic cross-flux passes in the transformer between primary and secondary, surrounding one coil only, without being interlinked with the other. This magnetic cross-flux is proportional to the current flowing in the electric circuit, and constitutes what is called the self-induction of the transformer. As seen, as self-induction of a transformer circuit, not the total flux produced by and interlinked with this circuit is understood, but only that—usually small—part of the flux

which surrounds the one circuit without interlinking with the other, and is thus produced by the M.M.F. of one circuit only.

133. The common magnetic flux of the transformer is produced by the resultant M.M.F. of both electric circuits. It is determined by the counter E.M.F., the number of turns, and the frequency of the electric circuit, by the equation :

$$E = \sqrt{2} \pi N n \Phi 10^{-8}.$$

Where E = effective E.M.F.
 N = frequency.
 n = number of turns.
 Φ = maximum magnetic flux.

The M.M.F. producing this flux, or the resultant M.M.F. of primary and secondary circuit, is determined by shape and magnetic characteristic of the material composing the magnetic circuit, and by the magnetic induction. At open secondary circuit, this M.M.F. is the M.M.F. of the primary current, which in this case is called the exciting current, and consists of an energy component, the magnetic energy current, and a reactive component, the magnetizing current.

134. In the general alternating-current transformer, where the secondary is movable with regard to the primary, the rate of cutting of the secondary electric circuit with the mutual magnetic flux is different from that of the primary. Thus, the frequencies of both circuits are different, and the induced E.M.Fs. are not proportional to the number of turns as in the stationary transformer, but to the product of number of turns into frequency.

135. Let, in a general alternating-current transformer :

$$s = \text{ratio } \frac{\text{secondary}}{\text{primary}} \text{ frequency, or "slip" ;}$$

thus, if

$$N = \text{primary frequency, or frequency of impressed E.M.F.,}$$

$$s N = \text{secondary frequency ;}$$

and the E.M.F. induced per secondary turn by the mutual flux has to the E.M.F. induced per primary turn the ratio s ,

$s = 0$ represents synchronous motion of the secondary ;

$s < 0$ represents motion above synchronism—driven by external mechanical power, as will be seen ;

$s = 1$ represents standstill ;

$s > 1$ represents backward motion of the secondary

that is, motion against the mechanical force acting between primary and secondary (thus representing driving by external mechanical power).

Let

n_0 = number of primary turns in series per circuit ;

n_1 = number of secondary turns in series per circuit ;

$a = \frac{n_0}{n_1}$ = ratio of turns ;

$Y_0 = g_0 + j b_0$ = primary admittance per circuit ;

where

g_0 = effective conductance ;

b_0 = susceptance ;

$Z_0 = r_0 - j x_0$ = internal primary impedance per circuit,

where

r_0 = effective resistance of primary circuit ;

x_0 = reactance of primary circuit ;

$Z_{11} = r_1 - j x_1$ = internal secondary impedance per circuit at standstill, or for $s = 1$,

where

r_1 = effective resistance of secondary coil ;

x_1 = reactance of secondary coil at standstill, or full frequency, $s = 1$.

Since the reactance is proportional to the frequency, at the slip s , or the secondary frequency sN , the secondary impedance is ;

$$Z_1 = r_1 - j s x_1.$$

Let the secondary circuit be closed by an external resistance r , and an external reactance, and denote the latter

by x at frequency N , then at frequency sN , or slip s , it will be $= sx$, and thus :

$$Z = r - jsx = \text{external secondary impedance.}^*$$

Let

- E_0 = primary impressed E.M.F. per circuit,
- E_0' = E.M.F. consumed by primary counter E.M.F.,
- E_1 = secondary terminal E.M.F.,
- E_1' = secondary induced E.M.F.,
- e = E.M.F. induced per turn by the mutual magnetic flux, at full frequency N ,
- I_0 = primary current,
- I_{00} = primary exciting current,
- I_1 = secondary current.

It is then :

Secondary induced E.M.F.

$$E_1' = sn_1e.$$

Total secondary impedance

$$Z_1 + Z = (r_1 + r) - js(x_1 + x);$$

hence, secondary current

$$I_1 = \frac{E_1'}{Z_1 + Z} = \frac{kn_1e}{(r_1 + r) - js(x_1 + x)};$$

Secondary terminal voltage

$$E_1 = E_1' - I_1Z_1 = I_1Z$$

$$= sn_1e \left\{ 1 - \frac{r_1 - jsx_1}{(r_1 + r) - js(x_1 + x)} \right\} = \frac{sn_1e(r - jsx)}{(r_1 + r) - js(x_1 + x)}.$$

* This applies to the case where the secondary contains inductive reactance only ; or, rather, that kind of reactance which is proportional to the frequency. In a condenser the reactance is inversely proportional to the frequency in a synchronous motor under circumstances independent of the frequency. Thus, in general, we have to set, $x = x' + x'' + x'''$, where x' is that part of the reactance which is proportional to the frequency, x'' that part of the reactance independent of the frequency, and x''' that part of the reactance which is inversely proportional to the frequency; and have thus, at slip s , or frequency sN , the external secondary reactance $sx' + x'' + \frac{x'''}{s}$.

E.M.F. consumed by primary counter E.M.F.

$$E_0' = -n_0 e;$$

hence, primary exciting current:

$$I_{00} = E_0' Y_0 = -n_0 e (g_0 + j b_0).$$

Component of primary current corresponding to secondary current I_1 :

$$\begin{aligned} I_1' &= -\frac{I_1}{a} \\ &= -\frac{n_0 s e}{a^2 \{(r_1 + r) - j s (x_1 + x)\}}, \end{aligned}$$

hence, total primary current,

$$\begin{aligned} I_0 &= I_{00} + I_1' \\ &= -s n_0 e \left\{ \frac{1}{a^2 (r_1 + r) - j s (x_1 + x)} + \frac{g_0 + j s b_0}{s} \right\}. \end{aligned}$$

Primary impressed E.M.F.,

$$\begin{aligned} E_0 &= E_0' + I_0 Z_0 \\ &= -n_0 e \left\{ 1 + \frac{s}{a^2} \frac{r_0 - j x_0}{(r_1 + r) - j s (x_1 + x)} + (r_0 - j x_0) (g_0 + j b_0) \right\} \end{aligned}$$

We get thus, as the

Equations of the General Alternating-Current Transformer:

Of ratio of turns, a ; and ratio of frequencies, s ; with the E.M.F. induced per turn at full frequency, e , as parameter, the values:

Primary impressed E.M.F.,

$$E_0 = -n_0 e \left\{ 1 + \frac{s}{a^2} \frac{r_0 - j x_0}{(r_1 + r) - j s (x_1 + x)} + (r_0 - j x_0) (g_0 + j b_0) \right\}.$$

Secondary terminal voltage,

$$E_1 = s n_1 e \left\{ 1 - \frac{r_1 - j s x_1}{(r_1 + r) - j s (x_1 + x)} \right\} = s n_1 e \frac{r - j s x}{(r_1 + r) - j s (x_1 + x)}.$$

Primary current,

$$I_0 = -s n_0 e \left\{ \frac{1}{a^2 (r_1 + r) - j s (x_1 + x)} + \frac{g_0 + j s b_0}{s} \right\}.$$

Secondary current,

$$I_1 = \frac{s n_1 e}{(r_1 + r) - j s (x_1 + x)}$$

Therefrom, we get :

Ratio of currents,

$$\frac{I_0}{I_1} = -\frac{1}{a} \left\{ 1 + \frac{a^2}{s} (g_0 + j b_0) [(r_1 + r) - j (x_1 + x)] \right\}.$$

Ratio of E.M.Fs.,

$$\frac{E_0}{E_1} = -\frac{a}{s} \left\{ \frac{1 + \frac{s}{a^2} \frac{r_0 - j x_0}{(r_1 + r) - j s (x_1 + x)} + (r_0 - j x_0)(g_0 + j b_0)}{1 - \frac{r_1 - j s x_1}{(r_1 + r) - j s (x_1 + x)}} \right\}.$$

Total apparent primary impedance,

$$Z_t = \frac{E_0}{I_0} = \frac{a^2}{s} \{ (r_1 + r) - j (x_1 + x) \} \left\{ \frac{1 + \frac{s}{a^2} \frac{r_0 - j x_0}{(r_1 + r) - j s (x_1 + x)} + (r_0 - j x_0)(g_0 + j b_0)}{1 + \frac{a^2}{s} (g_0 + j b_0) [(r_1 + r) - j s (x_1 + x)]} \right\}$$

where $x = x' + \frac{x''}{s} + \frac{x'''}{s^2}$

in the general secondary circuit as discussed in foot-note, page 4.

Substituting in these equations:

$$s = 1,$$

gives the

General Equations of the Stationary Alternating-Current Transformer :

$$E_0 = -n_0 e \left\{ 1 + \frac{1}{a^2} \frac{Z_0}{Z_1 + Z} + Z_0 Y_0 \right\}.$$

$$E_1 = n_1 e \left\{ 1 - \frac{Z_1}{Z_1 + Z} \right\} = n_1 e \frac{Z}{Z_1 + Z}.$$

$$I_0 = -n_0 e \left\{ \frac{1}{a^2 (Z_1 + Z)} + Y_0 \right\}.$$

$$I_1 = \frac{n_1 e}{Z_1 + Z}$$

$$\frac{I_0}{I_1} = -\frac{1}{a} \{1 + a^2 Y_0 (Z_1 + Z)\}.$$

$$\frac{E_0}{E_1} = -a \left\{ \frac{1 + \frac{Z_0}{a^2 (Z_1 + Z)} + Z_0 Y_0}{1 - \frac{Z_1}{Z_1 + Z}} \right\}.$$

$$Z_t = \frac{E_0}{I_0} = a^2 (Z_1 + Z) \left\{ \frac{1 + \frac{Z_0}{a^2 (Z_1 + Z)} + Z_0 Y_0}{1 + a^2 Y_0 (Z_1 + Z)} \right\}$$

Substituting in the equations of the general alternating-current transformer,

$$Z = 0,$$

gives the

General Equations of the Induction Motor:

$$E_0 = -n_0 e \left\{ 1 + \frac{s}{a^2} \frac{r_0 - jx_0}{r_1 - jsx_1} + (r_0 + jx_0)(g_0 + jb_0) \right\}.$$

$$E_1 = 0.$$

$$I_0 = -sn_0 e \left\{ \frac{1}{a^2 (r_1 - jsx_1)} + \frac{g_0 + jb_0}{s} \right\}.$$

$$I_1 = \frac{sn_1 e}{r_1 - jsx_1}.$$

$$\frac{I_0}{I_1} = -\frac{1}{a} \left\{ 1 + \frac{a^2}{s} (g_0 + jb_0) (r_1 - jsx_1) \right\}.$$

$$Z_t = \frac{a^2}{s} (r_1 - jsx_1) \left\{ \frac{1 + \frac{s}{a^2} \frac{r_0 - jx_0}{r_1 - jsx_1} + (r_0 - jx_0)(g_0 + jb_0)}{1 + \frac{a^2}{s} (r_1 - jsx_1) (g_0 + jb_0)} \right\}.$$

Returning now to the general alternating-current transformer, we have, by substituting

$$(r_1 + r)^2 + s^2 (x_1 + x)^2 = z_k^2,$$

and separating the real and imaginary quantities,

$$E_0 = -n_0 e \left\{ \left[1 + \frac{s}{a^2 z_k^2} (r_0 (r_1 + r) + sx_0 (x_1 + x)) \right] \right.$$

$$\left. \begin{aligned} &+ (r_0 g_0 + x_0 b_0) \\ &+ (r_0 g_0 - x_0 b_0) \end{aligned} \right\} + j \left[\frac{s}{a^2 z_k^2} (s r_0 (x_1 + x) - x_0 (r_1 + r)) \right]$$

$$I_0 = -s n_0 e \left\{ \left[\frac{r_1 + r}{a^2 z_k^2} + \frac{g_0}{s} \right] + j \left[\frac{s(x_1 + x)}{a^2 z_k^2} + \frac{b_0}{s} \right] \right\}.$$

$$I_1 = \frac{s n_1 e}{z_k^2} \left\{ (r_1 + r) + j s (x_1 + x) \right\}.$$

Neglecting the exciting current, or rather considering it as a separate and independent shunt circuit outside of the transformer, as can approximately be done, and assuming the primary impedance reduced to the secondary circuit as equal to the secondary impedance,

$$\begin{aligned} Y_0 &= 0, \\ \frac{Z_0}{a^2} &= Z_{11}. \end{aligned}$$

Substituting this in the equations of the general transformer, we get,

$$\begin{aligned} E_0 &= -n_0 e \left\{ 1 + \frac{s}{z_k^2} [r_1 (r_1 + r) + s x_1 (x_1 + x)] \right. \\ &\quad \left. + \frac{j s}{z_k^2} [s r_1 (x_1 + x) - x_1 (r_1 + r)] \right\}. \end{aligned}$$

$$E_1 = \frac{s n_1 e}{z_k^2} \{ [r (r_1 + r) + s^2 x (x_1 + x)] + i s [r x_1 - x r_1] \}.$$

$$I_0 = -\frac{s n_1 e}{a z_k^2} \{ (r_1 + r) j s (x_1 + x) \}.$$

$$I_1 = \frac{s n_1 e}{z_k^2} \{ (r_1 + r) j s (x_1 + x) \}.$$

136. If

$E = a + j\beta =$ E.M.F., in complex quantities,
and

$I = c + jd =$ current in complex quantities,

the power is,

$$P = |E, I| = E I \cos (E, I) = ac + \beta d.$$

Making use of this, and denoting,

$$\frac{s n_1^2 e^2}{z_k^2} = w$$

gives:

Secondary output of the transformer

$$P_1 = |E_1, I_1| = \left(\frac{s n_1 e}{z_k} \right)^2 r = s r w.$$

Internal loss in secondary circuit,

$$P_1^1 = i_1^2 r_1 = \left(\frac{s n_1 e}{z_k} \right)^2 r_1 = s r_1 w.$$

Total secondary power,

$$P_1 + P_1^1 = \left(\frac{s n_1 e}{z_k} \right)^2 (r + r_1) = s w (r + r_1).$$

Internal loss in primary circuit,

$$P_0^1 = i_0^2 r_1 = \left(\frac{s n_1 e}{z_k} \right)^2 r_1 = s r_1 w$$

Total electrical output, plus loss,

$$P^1 = P_1 + P_1^1 + P_0^1 = \left(\frac{s n_1 e}{z_k} \right)^2 (r + 2 r_1) = s w (r + 2 r_1).$$

Total electrical input of primary,

$$P_0 = |E_0 I_0| = s \left(\frac{n_1 e}{z_k} \right)^2 (r + r_1 + s r_1) = w (r + r_1 + s r_1).$$

Hence, mechanical output of transformer,

$$P = P_0 - P^1 = w (1 - s) (r + r_1).$$

Ratio,

$$\frac{\text{mechanical output}}{\text{total secondary power}} = \frac{P}{P_1 + P_1^1} = \frac{1 - s}{s} = \frac{\text{speed}}{\text{slip}}.$$

137. Thus,

In a general alternating transformer of ratio of turns, a , and ratio of frequencies, s , neglecting exciting current, it is:

Electrical input in primary,

$$P_0 = \frac{s n_1^2 e^2 (r + r_1 + s r_1)}{(r_1 + r)^2 + s^2 (x_1 + x)^2}$$

Mechanical output,

$$P = \frac{s(1-s)n_1^2 e^2 (r+r_1)}{(r_1+r)^2 + s^2(x_1+x)^2}.$$

Electrical output of secondary,

$$P_1 = \frac{s^2 n_1^2 e^2 r}{(r_1+r)^2 + s^2(x_1+x)^2}.$$

Losses in transformer,

$$P_0^1 + P_1^1 = P^1 = \frac{2s^2 n_1^2 e^2 r_1}{(r_1+r)^2 + s^2(x_1+x)^2}.$$

Of these quantities, P^1 and P_1 are always positive; P_0 and P can be positive or negative, according to the value of s . Thus the apparatus can either produce mechanical power, acting as a motor, or consume mechanical power; and it can either consume electrical power or produce electrical power, as a generator.

138. At

$$s = 0, \text{ synchronism, } P_0 = 0, P = 0, P_1 = 0.$$

At $0 < s < 1$, between synchronism and standstill.

P_1 , P and P_0 are positive; that is, the apparatus consumes electrical power P_0 in the primary, and produces mechanical power P and electrical power $P_1 + P_1^1$ in the secondary, which is partly, P_1^1 , consumed by the internal secondary resistance, partly, P_1 , available at the secondary terminals.

In this case it is:

$$\frac{P_1 + P_1^1}{P} = \frac{s}{1-s};$$

that is, of the electrical power consumed in the primary circuit, P_0 , a part P_0^1 is consumed by the internal primary resistance, the remainder transmitted to the secondary, and divides between electrical power, $P_1 + P_1^1$, and mechanical power, P , in the proportion of the slip, or drop below synchronism, s , to the speed: $1 - s$.

In this range, the apparatus is a motor.

At $s > 1$; or, backwards driving,

$P < 0$, or negative; that is, the apparatus requires mechanical power for driving.

It is then: $P_0 - P_0^1 - P_1^1 < P_1$;

that is: the secondary electrical power is produced partly by the primary electrical power, partly by the mechanical power, and the apparatus acts simultaneously as transformer and as alternating-current generator, with the secondary as armature.

The ratio of mechanical input to electrical input is the ratio of speed to synchronism.

In this case, the secondary frequency is higher than the primary.

At $P < 0$, beyond synchronism,

$P < 0$; that is, the apparatus has to be driven by mechanical power.

$P_0 < 0$; that is, the primary circuit produces electrical power from the mechanical input.

At $r + r_1 + sr_1 = 0$, or, $s < -\frac{r + r_1}{r}$;

the electrical power produced in the primary becomes less than required to cover the losses of power, and P_0 becomes positive again.

We have thus:

$$s < -\frac{r + r_1}{r}$$

consumes mechanical and primary electric power; produces secondary electric power.

$$-\frac{r + r_1}{r} < s < 0$$

consumes mechanical, and produces electrical power in primary and in secondary circuit.

$$0 < s < 1$$

consumes primary electric power, and produces mechanical and secondary electrical power.

$$1_1 < s$$

consumes mechanical and primary electrical power; produces secondary electrical power.

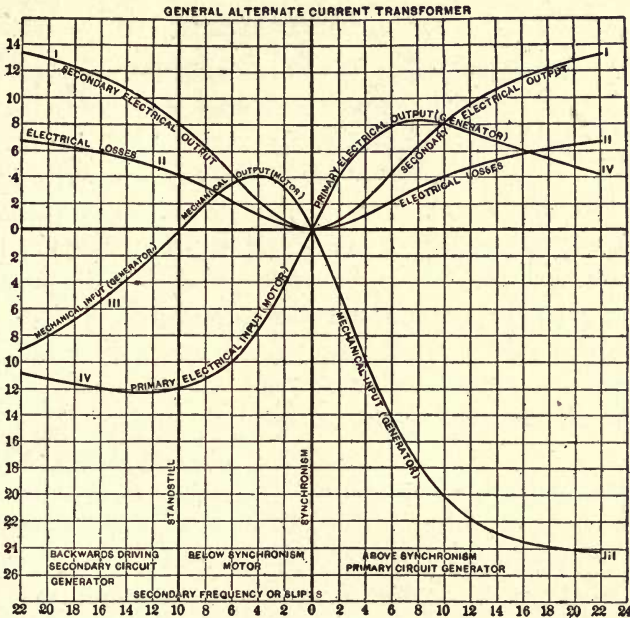


Fig. 104.

139. As an instance, in Fig. 1 are plotted, with the slip s as abscissæ, the values of :

- Secondary electrical output as Curve I. ;
- Total internal loss as Curve II. ;
- Mechanical output as Curve III. ;
- Primary electrical input as Curve IV. ;

for the values :

$$\begin{aligned}
 n_1 c &= 100.0 ; & r &= .4 ; \\
 r_1 &= .1 ; & s &= .3 ; \\
 k_1 &= .2 ;
 \end{aligned}$$

hence,

$$P_1 = \frac{16,000 s^2}{1 + s^2};$$

$$P_0^1 + P_1^1 = \frac{8,000 s^2}{1 + s^2};$$

$$P_0 = \frac{4,000 s + (5 + s)}{1 + s^2};$$

$$P = \frac{20,000 s (1 - s)}{1 + s^2}.$$

CHAPTER XV.

INDUCTION MOTOR.

140. A specialization of the general alternating-current transformer is the induction motor. It differs from the stationary alternating-current transformer in so far as the two sets of electric circuits — the primary or excited, and the secondary or induced, circuits — are movable with regard to each other; and that in general a number of primary and a number of secondary circuits are used, angularly displaced around the periphery of the motor, and containing E.M.Fs. displaced in phase by the same angle. This multi-circuit arrangement has the object always to retain secondary circuits in inductive relation to primary circuits, in spite of their relative motion.

The result of the relative motion between primary and secondary is, that the E.M.Fs. induced in the secondary or the motor armature are not of the same frequency as the E.M.F. impressed upon the primary, but of a frequency which is the difference between the impressed frequency and the frequency of rotation, or equal to the “slip,” that is, the difference between synchronism and speed (in cycles).

Hence, if

N = frequency of main or primary E.M.F.,
 and s = percentage slip;
 sN = frequency of armature or secondary E.M.F.,
 and $(1 - s)N$ = frequency of rotation of armature.

In its reaction upon the primary circuit, however, the armature current is of the same frequency as the primary

current, since it is carried around mechanically, with such a frequency as always to have the same phase relation, in the same position, with regard to the primary current.

141. Let the primary system consist of p equal circuits, displaced angularly in space by $1/p$ of a period, that is, $1/p$ of the width of two poles, and excited by p E.M.Fs. displaced in phase by $1/p$ of a period; that is, in other words, let the field circuits consist of a symmetrical p -phase system.

Analogously, let the armature or secondary circuits consist of a symmetrical p_1 -phase system.

Let

n = number of primary turns per circuit or phase ;

n_1 = number of secondary turns per circuit or phase ;

$a = \frac{n p}{n_1 p_1}$ = ratio of total primary turns to total secondary turns
or ratio of transformation.

Since the number of secondary circuits and number of turns of the secondary circuits, in the induction motor — like in the stationary transformer — is entirely unessential, it is preferable to reduce all secondary quantities to the primary system, by the ratio of transformation, a ; thus

if E_1' = secondary E.M.F. per circuit, $E_1 = a E_1'$
= secondary E.M.F. per circuit reduced to primary system ;

if I_1' = secondary current per circuit, $I_1 = \frac{I_1'}{a}$
= secondary current per circuit reduced to primary system ;

if r_1' = secondary resistance per circuit, $r_1 = a^2 r_1'$
= secondary resistance per circuit reduced to primary system ;

if x_1' = secondary reactance per circuit, $x_1 = a^2 x_1'$
= secondary reactance per circuit reduced to primary system ;

if z_1' = secondary impedance per circuit, $z_1 = a^2 z_1'$
 = secondary impedance per circuit reduced to primary system ;

that is, the number of secondary circuits and of turns per secondary circuit is assumed the same as in the primary system.

In the following discussion, as secondary quantities exclusively, the values reduced to the primary system shall be used, so that, to derive the true secondary values, these quantities have to be reduced backwards again by the factor

$$a = \frac{n\phi}{n_1\phi_1}.$$

142. Let

Φ = total maximum flux of the magnetic field per motor pole.

It is then

$E = \sqrt{2} \pi n N \Phi 10^{-8}$ = effective E.M.F. induced by the magnetic field per primary circuit.

Counting the time from the moment where the rising magnetic flux of mutual induction Φ (flux interlinked with both electric circuits, primary and secondary) passes through zero, in complex quantities, the magnetic flux is denoted by

$$\Phi = j\phi,$$

and the primary induced E.M.F.,

$$E = -e;$$

where

$e = \sqrt{2} \pi n N \phi 10^{-8}$ may be considered as the "Active E.M.F. of the motor."

Since the secondary frequency is sN , the secondary induced E.M.F. (reduced to primary system) is

$$E_1 = -se.$$

Let

I_o = exciting current, or current passing through the motor, per primary circuit, when doing no work (at synchronism),

and

$$Y = g + jb = \text{primary admittance per circuit} = \frac{I_o}{e}.$$

It is thus

ge = magnetic energy current, ge^2 = loss of power by hysteresis (and eddy currents) per primary coil.

Hence

pge^2 = total loss of energy by hysteresis and eddys, as calculated according to Chapter X.

be = magnetizing current,

and

nbe = effective M.M.F. per primary circuit ;

hence

$$\frac{p}{2} nbe = \text{total effective M.M.F. ;}$$

and

$\frac{p}{\sqrt{2}} nbe$ = total maximum M.M.F., as resultant of the M.M.Fs. of the p -phases, combined by the parallelogram of M.M.Fs.*

If \mathcal{R} = reluctance of magnetic circuit per pole, as discussed in Chapter X., it is

$$\frac{\phi}{\sqrt{2}} nbe = \mathcal{R} \phi.$$

Thus, from the hysteretic loss, and the reluctance, the constants, g and b , and thus the admittance, Y , are derived.

Let

r = resistance per primary circuit ;

z = reactance per primary circuit ;

thus,

$Z = r - jx$ = impedance per primary circuit ;

* Complete discussion hereof, see Chapter XXIII.

r_1 = resistance per secondary circuit reduced to primary system;

x_1 = reactance per secondary circuit reduced to primary system, at full frequency, N ;

hence,

$s x_1$ = reactance per secondary circuit at slip s ;

and

$Z_1 = r_1 - j s x_1$ = secondary internal impedance.

143. It is now,

Primary induced E.M.F.,

$$E = -e.$$

Secondary induced E.M.F.,

$$E_1 = -s e.$$

Hence,

Secondary current,

$$I_1 = \frac{E_1}{Z_1} = - \frac{s e}{r_1 - j s x_1}$$

Component of primary current, corresponding thereto,

$$I_1' = - I_1 = \frac{s e}{r_1 - j s x_1};$$

Primary exciting current,

$$I_o = e Y = e (g + j b);$$

hence,

Total primary current,

$$\begin{aligned} I &= I_1' + I_o \\ &= e \left\{ \frac{s}{r_1 - j s x_1} + (g + j b) \right\}; \end{aligned}$$

E.M.F. consumed by primary impedance,

$$\begin{aligned} E_z &= Z I \\ &= e (r - j x) \left\{ \frac{s}{r_1 - j s x} + (g + j b) \right\}; \end{aligned}$$

E.M.F. required to overcome the primary induced E.M.F.,

$$- E = e;$$

hence,

Primary terminal voltage,

$$\begin{aligned} E_o &= e + E_z \\ &= e \left\{ 1 + \frac{s(r-jx)}{r_1 - jsx_1} + (r-jx)(g+jb) \right\}. \end{aligned}$$

We get thus, in an induction motor, at slip s and active E.M.F. e , it is

Primary terminal voltage,

$$E_o = e \left\{ 1 + \frac{s(r-jx)}{r_1 - jsx_1} + (r-jx)(g+jb) \right\};$$

Primary current,

$$I = e \left\{ \frac{s}{r_1 - jsx_1} + (g+jb) \right\};$$

or, in complex expression,

Primary terminal voltage,

$$E_o = e \left\{ 1 + s \frac{Z}{Z_1} + ZY \right\};$$

Primary current,

$$I = e \left\{ \frac{s}{Z_1} + Y \right\}.$$

To eliminate e , we divide, and get,

Primary current, at slip s , and impressed E.M.F., E_o :

$$I = \frac{s + Z_1 Y}{Z_1 + sZ + ZZ_1 Y} E_o;$$

or,

$$I = \frac{s + (r_1 - jsx_1)(g + jb)}{(r_1 - jsx_1) + s(r - jx) + (r - jx)(r_1 - jsx_1)(g + jb)} E_o.$$

Neglecting, in the denominator, the small quantity $ZZ_1 Y$, it is

Denoting the magnetism by the vertical vector $\overline{O\Phi}$ in Fig. 105, the M.M.F. in ampere-turns per circuit is represented by vector \overline{OF} , leading the magnetism $\overline{O\Phi}$ by the angle of hysteretic advance α . The E.M.F. induced in the secondary is proportional to the slip s , and represented by $\overline{OE_1}$ at the amplitude of 180° . Dividing $\overline{OE_1}$ by α in the proportion of $r_1 \div s x_1$, and connecting α with the middle b of the upper arc of the circle $\overline{OE_1}$, this line intersects the lower arc of the circle at the point $\overline{I_1 r_1}$. Thus, $\overline{OI_1 r_1}$ is the E.M.F. consumed by the secondary resistance, and $\overline{OI_1 x_1}$ equal and parallel to $\overline{E_1 I_1 r_1}$ is the E.M.F. consumed by the secondary reactance. The angle, $E_1 O I_1 r_1 = \hat{\omega}_1$ is the angle of secondary lag.

The secondary M.M.F. $\overline{OG_1}$ is in the direction of the vector $\overline{OI_1 r_1}$. Completing the parallelogram of M.M.Fs. with \overline{OF} as diagonal and $\overline{OG_1}$ as one side, gives the primary M.M.F. \overline{OG} as other side. The primary current and the E.M.F. consumed by the primary resistance, represented by $\overline{OI r}$, is in line with \overline{OG} , the E.M.F. consumed by the primary reactance 90° ahead of \overline{OG} , and represented by $\overline{OI x}$, and their resultant $\overline{OI z}$ is the E.M.F. consumed by the primary impedance. The E.M.F. induced in the primary circuit is $\overline{OE_1}$, and the E.M.F. required to overcome this counter E.M.F. is \overline{OE} equal and opposite to $\overline{OE_1}$. Combining \overline{OE} with $\overline{OI z}$ gives the primary terminal voltage represented by vector $\overline{OE_0}$, and the angle of primary lag, $E_0 O G = \hat{\omega}_0$.

145. Thus far the diagram is essentially the same as the diagram of the stationary alternating-current transformer.

Regarding dependence upon the slip of the motor, the locus of the different quantities for different values of the slip s is determined thus :

It is

$$E_1 = s E_1'$$

$$OA \div I_1 r_1 = E_1 \div I_1 s x_1$$

$$OA = \frac{I_1 r_1 \times E_1}{I_1 s x_1} = \frac{I_1 r_1 \times s E_1'}{I_1 s x_1} = \frac{r_1}{x_1} E_1' = \text{constant.}$$

That is, $I_1 r_1$ lies on a half-circle with $\frac{r_1}{x_1} E_1'$ as diameter.

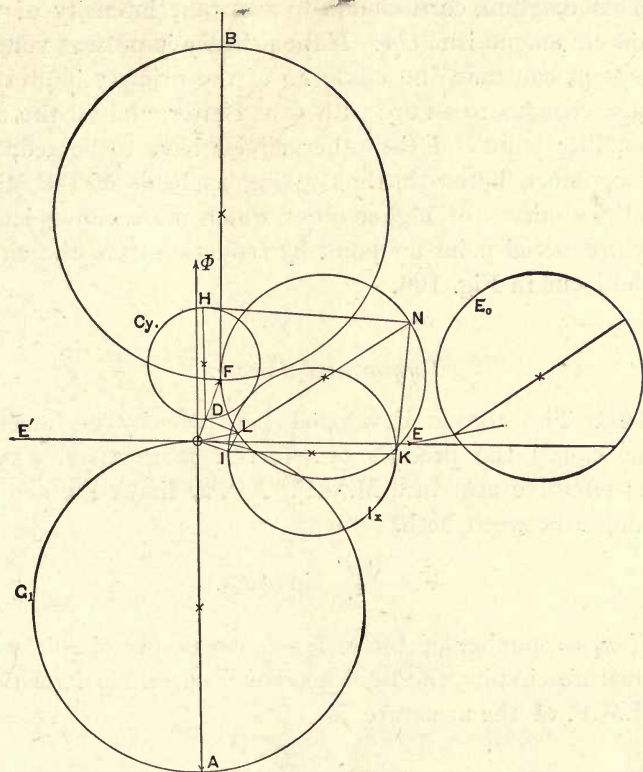


Fig. 106.

That means G_1 lies on a half-circle g_1 in Fig. 106 with \overline{OA} as diameter. In consequence hereof, G_o lies on half-circle g_o with \overline{FB} equal and parallel to \overline{OA} as diameter.

Thus I_r lies on a half-circle with \overline{DH} as diameter, which circle is perspective to the circle \overline{FB} , and I_x lies on a half-circle with \overline{IK} as diameter, and I_z on a half-circle with \overline{LN} as diameter, which circle is derived by the combination of the circles I_r and I_x .

The primary terminal voltage E_o lies thus on a half-circle eo equal to the half-circle Iz , and having to point E the same relative position as the half-circle Iz has to point 0.

This diagram corresponds to constant intensity of the maximum magnetism, $\overline{O\Phi}$. If the primary impressed voltage E_o is kept constant, the circle eo of the primary impressed voltage changes to an arc with O as center, and all the corresponding points of the other circles have to be reduced in accordance herewith, thus giving as locus of the other quantities curves of higher order which most conveniently are constructed point for point by reduction from the circle of the locus in Fig. 106.

Torque and Power.

146. The torque developed per pole by an electric motor equals the product of effective magnetism, $\phi/\sqrt{2}$, times effective armature M.M.F., $F/\sqrt{2}$, times the sine of the angle between both,

$$\tau' = \frac{\phi F}{2} \sin(\phi F_1).$$

If n_1 = number of turns, I_1 = current, per circuit, with p -armature circuits, the total maximum current polarization, or M.M.F. of the armature, is

$$F_1 = \frac{pn_1 I_1}{\sqrt{2}}.$$

Hence the torque per pole,

$$\tau' = \frac{pn_1 \phi I_1}{2\sqrt{2}} \sin(\phi I_1).$$

If d = the number of poles of the motor, the total torque of the motor is,

$$\tau = \frac{d pn_1 \phi I_1}{2\sqrt{2}} \sin(\phi I_1).$$

The secondary induced E.M.F., E_1 , lags 90° behind the inducing magnetism, hence reaches a maximum displaced in space by 90° from the position of maximum magnetization. Thus, if the secondary current, I_1 , lags behind its E.M.F., E_1 , by angle, $\hat{\omega}_1$, the space displacement between armature current and field magnetism is

$$\angle (I_1 \phi) = 90^\circ + \hat{\omega}_1$$

hence, $\sin (\phi I_1) = \cos \hat{\omega}_1$

It is, however,

$$\cos \hat{\omega}_1 = \frac{r_1}{\sqrt{r_1^2 + s^2 x_1^2}},$$

$$I_1 = \frac{e s}{\sqrt{r_1^2 + s^2 x_1^2}},$$

$$e = \sqrt{2} \pi n_1 \phi N 10^{-8},$$

thus, $\phi = \frac{e 10^8}{\sqrt{2} \pi N};$

substituting these values in the equation of the torque, it is

$$\tau = \frac{d p s r_1 e^2 10^8}{4 \pi N (r_1^2 + s^2 x_1^2)};$$

or, in practical (C.G.S.) units,

$$\tau = \frac{d p s r_1 e^2}{4 \pi N (r_1^2 + s^2 x_1^2)}.$$

The Torque of the Induction Motor.

At the slip s , the frequency N , and the number of poles d , the linear speed at unit radius is

$$v = \frac{4 \pi N}{d} (1 - s);$$

hence the output of the motor,

$$P = T S$$

or, substituted,

$$P = \frac{p r_1 e^2 s (1 - s)}{r_1^2 + s^2 x_1^2}.$$

The Power of the Induction Motor.

147. We can arrive at the same results in a different way:

By the counter E.M.F. e of the primary circuit with current $I = I_0 + I_1$ the power is consumed, $eI = eI_0 + eI_1$. The power eI_0 is that consumed by the primary hysteresis and eddys. The power eI_1 disappears in the primary circuit by being transmitted to the secondary system.

Thus the total power impressed upon the secondary system, per circuit, is

$$P_1 = eI_1$$

Of this power a part, E_1I_1 , is consumed in the secondary circuit by resistance. The remainder,

$$P' = I_1(e - E_1),$$

disappears as electrical power altogether; hence, by the law of conservation of energy, must reappear as some other form of energy, in this case as mechanical power, or as the output of the motor (included mechanical and secondary magnetic friction).

Thus the mechanical output per motor circuit is

$$P' = I_1(e - E_1).$$

Substituting,

$$E_1 = se;$$

$$I_1 = \frac{se}{r_1 - jsx_1};$$

it is

$$\begin{aligned} P' &= \frac{e^2s(1-s)}{r_1 - jsx_1} \\ &= \frac{e^2s(1-s)(r_1 + jsx_1)}{r_1^2 + s^2x_1^2}; \end{aligned}$$

hence, since the imaginary part has no meaning as power,

$$P' = \frac{r_1e^2s(1-s)}{r_1^2 + s^2x_1^2};$$

and the total power of the motor,

$$P = \frac{p r_1 e^2 s (1 - s)}{r_1^2 + s^2 x_1^2}.$$

At the linear speed,

$$v = \frac{4 \pi N}{d} (1 - s)$$

at unit radius the torque is

$$\tau = \frac{d p r_1 e^2 s}{4 \pi N (r_1^2 + s^2 x_1^2)}.$$

In the foregoing, we found

$$E_o = e \left\{ 1 + s \frac{Z}{Z_1} + Z Y \right\},$$

or, approximately,

$$E_o = e \left\{ 1 + s \frac{Z}{Z_1} \right\};$$

or,

$$e = \frac{E_o Z_1}{s Z + Z_1};$$

expanded,

$$e = E_o \frac{r_1 - j s x_1}{(r_1 + s r) - j s (x_1 + x)};$$

or, eliminating imaginary quantities :

$$e = E_o \sqrt{\frac{r_1^2 + s^2 x_1^2}{(r_1 + s r)^2 + s^2 (x_1 + x)^2}}.$$

Substituting this value in the equations of torque and of power, it is,

$$\text{torque : } \tau = \frac{d p r_1 E_o^2 s}{4 \pi N \{(r_1 + s r)^2 + s^2 (x_1 + x)^2\}};$$

$$\text{power : } P = \frac{p r_1 E_o^2 s (1 - s)}{(r_1 + s r)^2 + s^2 (x_1 + x)^2}.$$

Maximum Torque.

148. The torque of the induction motor is a maximum for that value of slip s , where

$$\frac{d\tau}{ds} = 0,$$

or, since
$$\tau = \frac{d\phi r_1 E_o^2 \kappa}{4 \pi N \{ (r_1 + s r)^2 + s^2 (x_1 + x)^2 \}},$$

for,
$$\frac{d}{ds} \left\{ \frac{(r_1 + s r)^2 + s^2 (x_1 + x)^2}{s} \right\} = 0;$$

expanded, this gives,

$$-\frac{r_1^2}{s^2} + r^2 + (x_1 + x)^2 = 0,$$

or,
$$s_t = \frac{r_1}{\sqrt{r^2 + (x_1 + x)^2}}.$$

Substituting this in the equation of torque, we get the value of maximum torque,

$$\tau_t = \frac{d\phi E_o^2}{8 \pi N \{ r + \sqrt{r^2 + (x_1 + x)^2} \}}.$$

That is, independent of the secondary resistance, r_1 .

The power corresponding hereto is, by substitution of s_t in P ,

$$P_t = \frac{\phi E_o^2 \{ \sqrt{r^2 + (x_1 + x)^2} - r_1 \}}{2 \sqrt{r^2 + (x_1 + x)^2} \{ \sqrt{r^2 + (x_1 + x)^2} + r \}}.$$

This power is not the maximum output of the motor, but already below the maximum output. The maximum output is found at a lesser slip, or higher speed, while at the maximum torque point the output is already on the decrease, due to the decrease of speed.

With increasing slip, or decreasing speed, the torque of the induction motor increases; or inversely, with increasing load, the speed of the motor decreases, and thereby the torque increases, so as to carry the load down to the slip s_t , corresponding to the maximum torque. At this point of load and slip the torque begins to decrease again; that is, as soon as with increasing load, and thus increasing slip, the motor passes the maximum torque point s_t , it "falls out of step," and comes to a standstill.

Inversely, the torque of the motor, when starting from rest, will increase with increasing speed, until the maximum

torque point is reached. From there towards synchronism the torque decreases again.

In consequence hereof, the part of the torque-speed curve below the maximum torque point is in general unstable, and can be observed only by loading the motor with an apparatus, whose countertorque increases with the speed faster than the torque of the induction motor.

In general, the maximum torque point, s_t , is between synchronism and standstill, rather nearer to synchronism. Only in motors of very large armature resistance, that is low efficiency, $s_t > 1$, that is, the maximum torque falls below standstill, and the torque constantly increases from synchronism down to standstill.

It is evident that the position of the maximum torque point, s_t , can be varied by varying the resistance of the secondary circuit, or the motor armature. Since the slip at the maximum torque point, s_t , is directly proportional to the armature resistance, r_1 , it follows that very constant speed and high efficiency will bring the maximum torque point near synchronism, and give small starting torque, while good starting torque means a maximum torque point at low speed; that is, a motor with poor speed regulation and low efficiency.

Thus, to combine high efficiency and close speed regulation with large starting torque, the armature resistance has to be varied during the operation of the motor, and the motor started with high armature resistance, and with increasing speed this armature resistance cut out as far as possible.

$$149. \text{ If } s_t = 1,$$

$$\text{it is } r_1 = \sqrt{r^2 + (x_1 + x)^2}.$$

In this case the motor starts with maximum torque, and when overloaded does not drop out of step, but gradually slows down more and more, until it comes to rest.

$$\begin{aligned} \text{If,} & \quad s_t > 1, \\ \text{it is} & \quad r_1 > \sqrt{r^2 + (x_1 + x)^2}. \end{aligned}$$

In this case, the maximum torque point is reached only by driving the motor backwards, as counter-torque.

As seen above, the maximum torque, τ_t , is entirely independent of the armature resistance, and the same is the current corresponding thereto, independent of the armature resistance. Only the speed of the motor depends upon the armature resistance.

Hence the insertion of resistance into the motor armature does not change the maximum torque, and the current corresponding thereto, but merely lowers the speed at which the maximum torque is reached.

The effect of resistance inserted into the induction motor is merely to consume the E.M.F., which otherwise would find its mechanical equivalent in an increased speed, analogous as resistance in the armature circuit of a continuous-current shunt motor.

Further discussion on the effect of armature resistance is found under "Starting Torque."

Maximum Power.

150. The power of an induction motor is a maximum for that slip, s_p , where

$$\frac{dP}{ds} = 0;$$

or, since

$$P = \frac{\phi r_1 E_o^2 s (1-s)}{(r_1 + sr)^2 + s^2 (x_1 + x)^2},$$

$$\frac{d}{ds} \left\{ \frac{(r_1 + sr)^2 + s^2 (x_1 + x)^2}{s(1-s)} \right\} = 0;$$

expanded, this gives

$$s_p = \frac{r_1}{r_1 + \sqrt{(r_1 + r)^2 + (x_1 + x)^2}};$$

substituted in P , we get the maximum power,

$$P_p = \frac{p E_o^2}{2 \{ (r_1 + r) + \sqrt{(r_1 + r)^2 + (x_1 + x)^2} \}}$$

This result has a simple physical meaning: $(r_1 + r) = R$ is the total resistance of the motor, primary plus secondary (the latter reduced to the primary). $(x_1 + x)$ is the total reactance, and thus $\sqrt{(r_1 + r)^2 + (x_1 + x)^2} = Z$ is the total impedance of the motor. Hence it is

$$P_p = \frac{p E_o^2}{2 \{ R + Z \}},$$

the maximum output of the induction motor, at the slip,

$$s_p = \frac{r_1}{r_1 + Z}.$$

The same value has been derived in Chapter IX., as the maximum power which can be transmitted into a non-inductive receiver circuit over a line of resistance R , and impedance Z , or as the maximum output of a generator, or of a stationary transformer. Hence:

The maximum output of an induction motor is expressed by the same formula as the maximum output of a generator, or of a stationary transformer, or the maximum output which can be transmitted over an inductive line into a non-inductive receiver circuit.

The torque corresponding to the maximum output P_p is,

$$\tau_p = \frac{d p E_o^2 (r_1 + Z)}{8 \pi N Z (R + Z)}.$$

This is not the maximum torque, but the maximum torque, τ_t , takes place at a lower speed, that is, greater slip,

$$s_t = \frac{r_1}{\sqrt{r^2 + (x_1 + x)^2}},$$

since, $\frac{r_1}{\sqrt{r^2 + (x_1 + x)^2}} > \frac{r_1}{r_1 + \sqrt{(r_1 + r)^2 + (x_1 + x)^2}}$;

that is,

$$s_t > s_p.$$

It is obvious from these equations, that, to reach as large an output as possible, R and Z should be as small as possible; that is, the resistances $r_1 + r$, and the impedances, Z , and thus the reactances, $x_1 + x$, should be small. Since $r_1 + r$ is usually small compared with $x_1 + x$, it follows, that the problem of induction motor design consists in constructing the motor so as to give the minimum possible reactances, $x_1 + x$.

Starting Torque.

151. In the moment of starting an induction motor, it is

$$s = 1;$$

hence, starting current :

$$I = \frac{1 + (r_1 - jx_1)(g + jb)}{(r_1 - jx_1) + (r - jx) + (r_1 - jx_1)(r - jx)(g + jb)} E_o;$$

or, expanded, with the neglect of the last term in the denominator, as insignificant :

$$I = \frac{[(r_1 + r) + g(r_1[r_1 + r] + x_1[x_1 + x]) + b(rx_1 - xr_1)] + j[(x_1 + x) + b(r_1[r_1 + r] + x_1[x_1 + x]) - g(rx_1 - xr_1)]}{(r_1 + r)^2 + (x_1 + x)^2} E_o;$$

and, displacement of phase, or angle of lag,

$$\tan \hat{\omega}_o = \frac{(x_1 + x) + b(r_1[r_1 + r] + x_1[x_1 + x]) - g(rx_1 - xr_1)}{(r_1 + r) + g(r_1[r_1 + r] + x_1[x_1 + x]) + b(rx_1 - xr_1)}.$$

Neglecting the exciting current, $g = 0 = b$, these equations assume the form :

$$I = \frac{(r_1 + r) + j(x_1 + x)}{(r_1 + r)^2 + (x_1 + x)^2} E_o = \frac{E_o}{(r_1 + r) - j(x_1 + x)};$$

or, eliminating imaginary quantities,

$$i = \frac{E_o}{\sqrt{(r_1 + r)^2 + (x_1 + x)^2}} = \frac{E_o}{Z};$$

and

$$\tan \hat{\omega}_o = \frac{x_1 + x}{r_1 + r}.$$

That means, that in starting the induction motor without additional resistance in the armature circuit, — in which case $x_1 + x$ is large compared with $r_1 + r$, and the total impedance, Z , small, — the motor takes excessive and greatly lagging currents.

The starting torque is

$$\begin{aligned}\tau_o &= \frac{d\phi r_1 E_o^2}{4\pi N \{(r_1 + r)^2 + (x_1 + x)^2\}} \\ &= \frac{d\phi E_o^2}{4\pi N} \frac{r_1}{Z^2}.\end{aligned}$$

That is, the starting torque is proportional to the armature resistance, and inverse proportional to the square of the total impedance of the motor.

It is obvious thus, that, to secure large starting torque, the impedance should be as small, and the armature resistance as large, as possible. The former condition is the condition of large maximum output and good efficiency and speed regulation; the latter condition, however, means inefficiency and poor regulation, and thus cannot properly be fulfilled by the internal resistance of the motor, but only by an additional resistance which is short-circuited while the motor is in operation.

152. Since, necessarily,

$$r_1 < Z,$$

it is,
$$\tau_o < \frac{d\phi E_o^2}{4\pi N Z};$$

and since the starting current is, approximately,

$$I = \frac{E_o}{Z},$$

it is,
$$\tau_o < \frac{d\phi}{4\pi N} E_o I.$$

$$\tau_{oo} = \frac{d\phi}{4\pi N} E_o I$$

would be the theoretical torque developed at 100 per cent efficiency, and power factor by E.M.F., E_o , and current, I , at synchronous speed.

It is thus, $\tau_o < \tau_{oo}$,

and the ratio between the starting torque, τ_o , and the theoretical maximum torque, τ_{oo} , gives a means to judge the perfection of a motor regarding its starting torque.

This ratio, τ_o / τ_{oo} , reaches .8 to .9 in the best motors.

Substituting $I = E / Z$ in the equation of starting torque, it assumes the form,

$$\tau_o = \frac{d \dot{p}}{4 \pi N} I^2 Z r_1.$$

Since $4 \pi N / d =$ synchronous speed, it is :

The starting torque of the induction motor is equal to the resistance loss in the motor armature, divided by the synchronous speed.

The armature resistance which gives maximum starting torque is

$$\frac{d \tau_o}{d r_1} = 0;$$

or, since $\tau_o = \frac{d \dot{p} E_o^2}{4 \pi N} \frac{r_1}{(r_1 + r)^2 + (x_1 + x)^2}$,

$$\frac{d}{d r} \left\{ \frac{(r_1 + r)^2 + (x_1 + x)^2}{r_1} \right\} = 0;$$

expanded, this gives,

$$r_1 = \sqrt{r^2 + (x_1 + x)^2},$$

the same value as derived in the paragraph on "maximum torque."

Thus, adding to the internal armature resistance r_1' in starting the additional resistance,

$$r_1'' = \sqrt{r^2 + (x_1 + x)^2} - r_1',$$

makes the motor start with maximum torque, while with increasing speed the torque constantly decreases, and reaches

zero at synchronism. Under these conditions, the induction motor behaves similar to the continuous-current series motor, varying in the speed with the load, the difference being, however, that the induction motor approaches a definite speed at no-load, while with the series motor the speed indefinitely increases with decreasing load.

153. The additional armature resistance, r_1'' , required to give a certain starting torque, is found from the equation of starting torque :

Denoting the internal armature resistance by r_1' , total armature resistance is $r_1 = r_1' + r_1''$,

and thus,
$$\tau_o = \frac{d p E_o^2}{4 \pi N} \frac{r_1' + r_1''}{(r_1' + r_1'' + r)^2 + (x_1 + x)^2};$$

hence,

$$r_1'' = -r_1' - r + \frac{d p E_o^2}{8 \pi N \tau_o} \pm \sqrt{\left(\frac{d p E_o^2}{8 \pi N \tau_o}\right)^2 - \frac{d p E_o^2 r}{4 \pi N \tau_o} - (x_1 + x)^2}.$$

This gives two values, one above, the other below, the maximum torque point.

Choosing the positive sign of the root, we get a larger armature resistance, a small current in starting, but the torque constantly decreases with the speed.

Choosing the negative sign, we get a smaller resistance, a large starting current, and with increasing speed the torque first increases, reaches a maximum, and then decreases again towards synchronism.

These two points correspond to the two points of the speed-torque curve of the induction motor, in Fig. 107, giving the desired torque T_o .

The smaller value of r_1'' will give fairly good speed regulation, and thus in small motors, where the comparatively large starting current is no objection, the permanent armature resistance may be chosen to represent this value.

The larger value of r_1'' allows to start with minimum current, but requires cutting out of the resistance after the start, to secure speed regulation and efficiency.

Synchronism.

154. At synchronism, $s = 0$, it is :

$$I_s = E_o(g + jb);$$

or, rationalized :

$$I_s = E_o \sqrt{g^2 + b^2};$$

$$P = 0, \tau = 0;$$

that is, power and torque are zero. Hence, the induction motor can never reach complete synchronism, but must slip sufficiently to give the torque consumed by friction.

Running near Synchronism.

155. When running near synchronism, at a slip s above the maximum output point, where s is small, from .02 to .05 at full load, the equations can be simplified by neglecting terms with s , as of higher order.

It is, current :

$$I = \frac{s + r_2(g + jb)}{r_1} E_o;$$

or, eliminating imaginary quantities :

$$I = \sqrt{\left(\frac{s}{r_1} + g\right)^2 + b^2} E_o;$$

angle of lag :

$$\tan \phi_o = \frac{s^2(x_1 + x) + r_1^2 b}{s r_1 + r_1^2 g} = \frac{s^2 \frac{x_1 + x}{r_1} + r_1 b}{s + r_1 g};$$

$$P = \frac{p E_o^2 s}{r_1};$$

$$\tau = \frac{d p E_o^2 s}{4 \pi N r_1};$$

or, inversely :

$$s = \frac{r_1 P}{p E_o^2};$$

$$s = \frac{4 \pi N r_1 \tau}{d p E_o^2}$$

that is :

Near synchronism, the slip, s , of an induction motor, or its drop in speed, is proportional to the armature resistance r_1 and to the power, P , or torque.

Induction Generator.

156. In the foregoing, the range of speed from $s = 1$, standstill, to $s = 0$, synchronism, has been discussed. In this range the motor does mechanical work.

It consumes mechanical power, that is, acts as generator or as brake, outside of this range.

For, $s > 1$, backwards driving, P becomes negative, representing consumption of power, while s remains positive; hence, since the direction of rotation has changed, represents consumption of power also. All this power is consumed in the motor, which thus acts as brake.

For, $s < 0$, or negative, P and τ become negative, and the machine becomes an electric generator, converting mechanical into electric energy.

Substituting in this case: $s_1 = -s$, where k_1 is the acceleration, or the slip of the machine above synchronism, we derive the equations of the induction generator, which are the same as those of the induction motor, except that the sign before the "slip" is reversed.

Again a maximum torque point, and a maximum output point are found, and the torque and power increase from zero at synchronism up to a maximum point, and then decrease again, while the current constantly increases.

157. The induction generator differs from the standard alternating-current generator essentially, in so far as it has no definite frequency of its own, but can operate at any frequency above that corresponding to its speed. But it can generate electric energy only when in circuit with an alternating-current apparatus of definite frequency, as an

alternator or synchronous motor. That is, the induction generator requires a "frequency setter" for its operation.

When operating in parallel with standard alternators, the phase relation of the current issuing from the induction generator mainly depends — besides upon the slip — upon the self-induction of the induction generator, and can be varied thereby.

Hence the induction generator can be used to control the phase relation in an alternating-current circuit.

When connected in series in a circuit, the E.M.F. of the induction generator is approximately proportional to the current. Thus it can be used as booster, to add voltage to a line in proportion to the current passing therein.

Example.

158. As an instance are shown, in Fig. 107, characteristic curves of a 20 horse-power three-phase induction

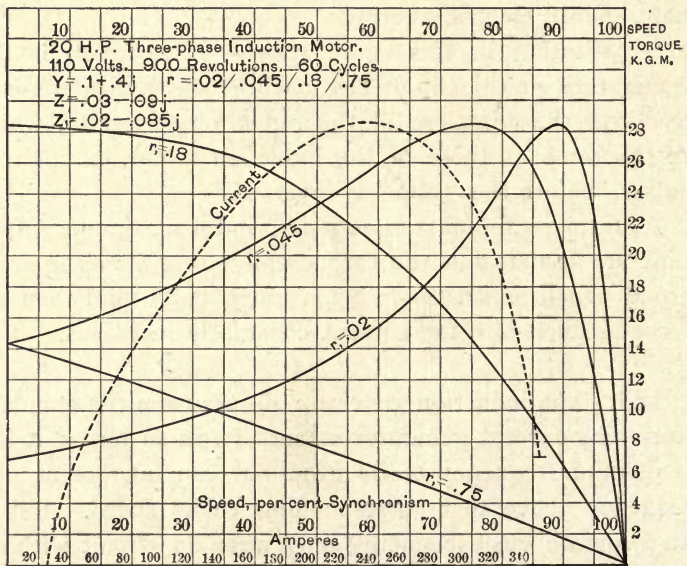


Fig. 107. Speed Characteristics of Induction Motor.

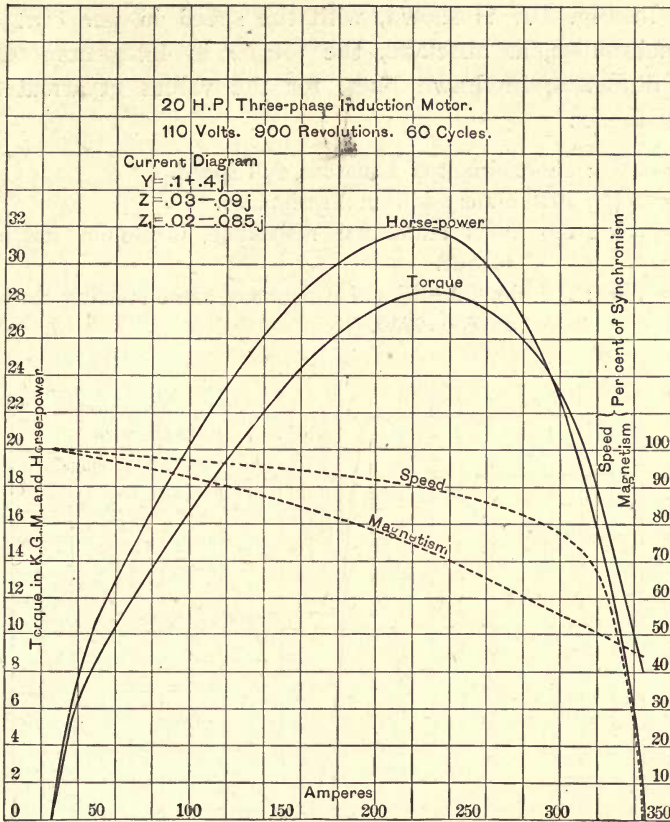


Fig. 108. Current Characteristics of Induction Motor.

motor, of 900 revolutions synchronous speed, 8 poles, frequency of 60 cycles.

The impressed E.M.F. is 110 volts between lines, and the motor star-connected, hence the E.M.F. impressed per circuit :

$$\frac{110}{\sqrt{3}} = 63.5; \text{ or } E_o = 63.5.$$

The constants of the motor are :

- Primary admittance, $Y = .1 + .4 j$.
- Primary impedance, $Z = .03 - .09 j$.
- Secondary impedance, $Z_1 = .02 - .085 j$.

In Fig. 107 is shown, with the speed in per cent of synchronism, as abscissæ, the torque in kilogrammetres, as ordinates, in drawn lines, for the values of armature resistance :

$r_1 = .02$: short circuit of armature, full speed.

$r_1 = .045$: .025 ohms additional resistance.

$r_1 = .16$: .16 ohms additional resistance, maximum starting torque.

$r_1 = .75$: .73 ohms additional resistance, same starting torque as $r_1 = .045$.

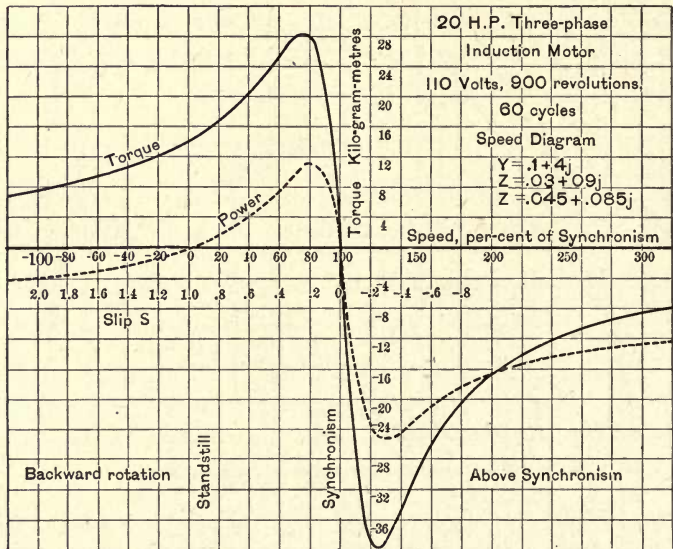


Fig. 109. Speed Characteristics of Induction Motor.

On the same Figure is shown the current per line, in dotted lines, with the verticals or torque as abscissæ, and the horizontals or amperes as ordinates. To the same torque always corresponds the same current, no matter what the speed be.

On Fig. 108 is shown, with the current input per line as abscissæ, the torque in kilogrammetres and the output

in kilowatts as ordinates in drawn lines, and the speed and the magnetism, in per cent of their synchronous values, as ordinates in dotted lines, for the armature resistance $r_1 = .02$, or short circuit.

In Fig. 109 is shown, with the speed, in per cent of synchronism, as abscissæ, the torque in drawn line, and the output in dotted line, for the value of armature resistance $r_1 = .045$, for the whole range of speed from 120 per cent backwards speed to 220 per cent beyond synchronism, showing the two maxima, the motor maximum at $s = .25$, and the generator maximum at $s = -25$.

CHAPTER XVI.

ALTERNATING-CURRENT GENERATOR.

159. In the alternating-current generator, E.M.F. is induced in the armature conductors by their relative motion through a constant or approximately constant magnetic field.

When yielding current, two distinctly different M.M.Fs. are acting upon the alternator armature — the M.M.F. of the field due to the field-exciting spools, and the M.M.F. of the armature current. The former is constant, or approximately so, while the latter is alternating, and in synchronous motion relatively to the former; hence, fixed in space relative to the field M.M.F., or uni-directional, but pulsating in a single-phase alternator. In the polyphase alternator, when evenly loaded or balanced, the resultant M.M.F. of the armature current is more or less constant.

The E.M.F. induced in the armature is due to the magnetic flux passing through and interlinked with the armature conductors. This flux is produced by the resultant of both M.M.Fs., that of the field, and that of the armature.

On open circuit, the M.M.F. of the armature is zero, and the E.M.F. of the armature is due to the M.M.F. of the field coils only. In this case the E.M.F. is, in general, a maximum at the moment when the armature coil faces the position midway between adjacent field coils, as shown in Fig. 110, and thus incloses no magnetism. The E.M.F. wave in this case is, in general, symmetrical.

An exception from this statement may take place only in those types of alternators where the magnetic reluctance of the armature is different in different directions; thereby,

during the synchronous rotation of the armature, a pulsation of the magnetic flux passing through it is produced. This pulsation of the magnetic flux induces E.M.F. in the field spools, and thereby makes the field current pulsating also. Thus, we have, in this case, even on open circuit, no

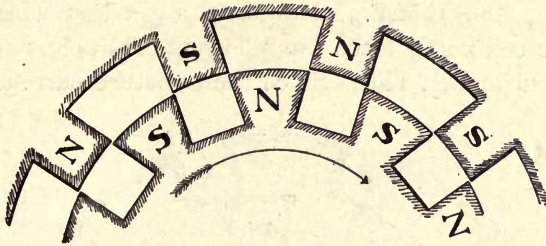


Fig. 110.

rotation through a constant magnetic field, but rotation through a pulsating field, which makes the E.M.F. wave unsymmetrical, and shifts the maximum point from its theoretical position midway between the field poles. In general this secondary reaction can be neglected, and the field M.M.F. be assumed as constant.

160. The relative position of the armature M.M.F. with respect to the field M.M.F. depends upon the phase relation existing in the electric circuit. Thus, if there is no displacement of phase between current and E.M.F., the current reaches its maximum at the same moment as the E.M.F.; or, in the position of the armature shown in Fig. 110, midway between the field poles. In this case the armature current tends neither to magnetize nor demagnetize the field, but merely distorts it; that is, demagnetizes the trailing-pole corner, *a*, and magnetizes the leading-pole corner, *b*. A change of the total flux, and thereby of the resultant E.M.F., will take place in this case only when the magnetic densities are so near to saturation that the rise of density at the leading-pole corner will be less than the decrease of

density at the trailing-pole corner. Since the internal self-inductance of the alternator alone causes a certain lag of the current behind the induced E.M.F., this condition of no displacement can exist only in a circuit with external negative reactance, as capacity, etc.

If the armature current lags, it reaches the maximum later than the E.M.F.; that is, in a position where the armature coil partly faces the following-field pole, as shown in diagram in Fig. 111. Since the armature current flows

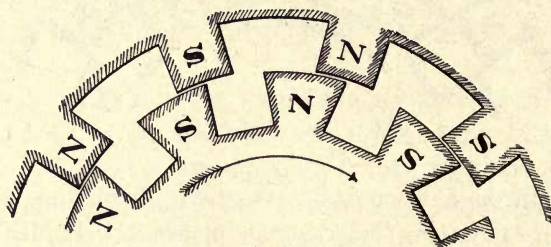


Fig. 111.

in opposite direction to the current in the following-field pole (in a generator), the armature in this case will tend to demagnetize the field.

If, however, the armature current leads,—that is, reaches its maximum while the armature coil still partly faces the

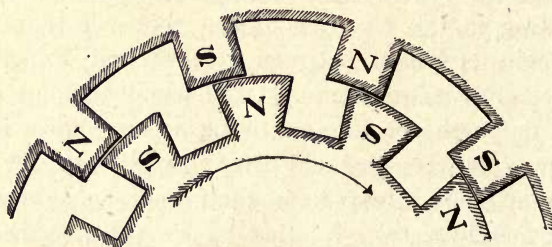


Fig. 112.

preceding-field pole, as shown in diagram Fig. 112,—it tends to magnetize this field coil, since the armature current flows in the same direction with the exciting current of the preceding-field spools.

Thus, with a leading current, the armature reaction of the alternator strengthens the field, and thereby, at constant-field excitation, increases the voltage; with lagging current it weakens the field, and thereby decreases the voltage in a generator. Obviously, the opposite holds for a synchronous motor, in which the direction of rotation is opposite; and thus a lagging current tends to magnetize, a leading current to demagnetize, the field.

161. The E.M.F. induced in the armature by the resultant magnetic flux, produced by the resultant M.M.F. of the field and of the armature, is not the terminal voltage of the machine; the terminal voltage is the resultant of this induced E.M.F. and the E.M.F. of self-inductance and the E.M.F. representing the energy loss by resistance in the alternator armature. That is, in other words, the armature current not only opposes or assists the field M.M.F. in creating the resultant magnetic flux, but sends a second magnetic flux in a local circuit through the armature, which flux does not pass through the field spools, and is called the magnetic flux of armature self-inductance.

• Thus we have to distinguish in an alternator between armature reaction, or the magnetizing action of the armature upon the field, and armature self-inductance, or the E.M.F. induced in the armature conductors by the current flowing therein. This E.M.F. of self-inductance is (if the magnetic reluctance, and consequently the reactance, of the armature circuit is assumed as constant) in quadrature behind the armature current, and will thus combine with the induced E.M.F. in the proper phase relation. This means that, if the armature current lags, the E.M.F. of self-inductance will be more than 90° behind the induced E.M.F., and therefore in partial opposition, and will reduce the terminal voltage. On the other hand, if the armature current leads, the E.M.F. of self-inductance will be less than 90° behind the induced E.M.F., or in partial conjunc-

tion therewith, and increase the terminal voltage. This means that the E.M.F. of self-inductance increases the terminal voltage with a leading, and decreases it with a lagging current, or, in other words, acts in the same manner as the armature reaction.

For this reason both actions can be combined in one, and represented by what is called the *synchronous reactance* of the alternator.

In the following, we shall represent the total reaction of the armature of the alternator by the one term, *synchronous reactance*. While this is not exact, as stated above, since the reactance should be resolved into the magnetic reaction due to the magnetizing action of the armature current, and the electric reaction due to the self-induction of the armature current, it is in general sufficiently near for practical purposes, and well suited to explain the phenomena taking place in the alternator under the various conditions of load.

162. This synchronous reactance, x , is frequently not constant, but is pulsating, owing to the synchronously varying reluctance of the armature magnetic circuit, and the field magnetic circuit; it may, however, be considered in what follows as constant; that is, the E.M.Fs. induced thereby may be represented by their equivalent sine waves. A specific discussion of the distortions of the wave shape due to the pulsation of the synchronous reactance is found in Chapter XX. The synchronous reactance, x , is not a true reactance in the ordinary sense of the word, but an *equivalent* or *effective* reactance.

163. Let E_0 = induced E.M.F. of the alternator, or the E.M.F. induced in the armature coils by their rotation through the constant magnetic field produced by the current in the field spools, or the open circuit voltage of the alternator.

Then
$$E_o = \sqrt{2} \pi n N M 10^{-8};$$

where

n = total number of turns in series on the armature,

N = frequency,

M = total magnetic flux per field pole.

Let x_o = synchronous reactance,

r_o = internal resistance of alternator;

then $Z_o = r_o - j x_o$ = internal impedance.

If the circuit of the alternator is closed by the external impedance,

$$Z = r - j x,$$

and current

$$I = \frac{E_o}{Z_o + Z} = \frac{E_o}{(r_o + r) - j(x_o + x)},$$

or,

$$I = \frac{E_o}{\sqrt{(r_o + r)^2 + (x_o + x)^2}};$$

and, terminal voltage,

$$\begin{aligned} E &= IZ = E_o - IZ_o \\ &= \frac{E_o (r - j x)}{(r_o + r) - j(x_o + x)}, \end{aligned}$$

or,

$$\begin{aligned} E &= \frac{E_o \sqrt{r^2 + x^2}}{\sqrt{(r_o + r)^2 + (x_o + x)^2}} \\ &= E_o \frac{1}{\sqrt{1 + 2 \frac{r_o r + x_o x}{r^2 + x^2} + \frac{r_o^2 + x_o^2}{r^2 + x^2}}}; \end{aligned}$$

or, expanded in a series,

$$E = E_o \left\{ 1 - \frac{r_o r + x_o x}{r^2 + x^2} + \frac{2(r_o r + x_o x) - (r_o x + x_o r)}{2(r^2 + x^2)} \pm \dots \right\}.$$

As shown, the terminal voltage varies with the conditions of the external circuit.

164. As an instance, in Figs. 113-118, at constant induced, the E.M.F.,

$$E_o = 2500;$$

and the values of the internal impedance,

$$Z_o = r_o - jx_o = 1 - 10j.$$

With the current I as abscissæ, the terminal voltages E as ordinates in drawn line, and the kilowatts output, $= I^2 r$, in dotted lines, the kilovolt-amperes output, $= I E$, in dash-

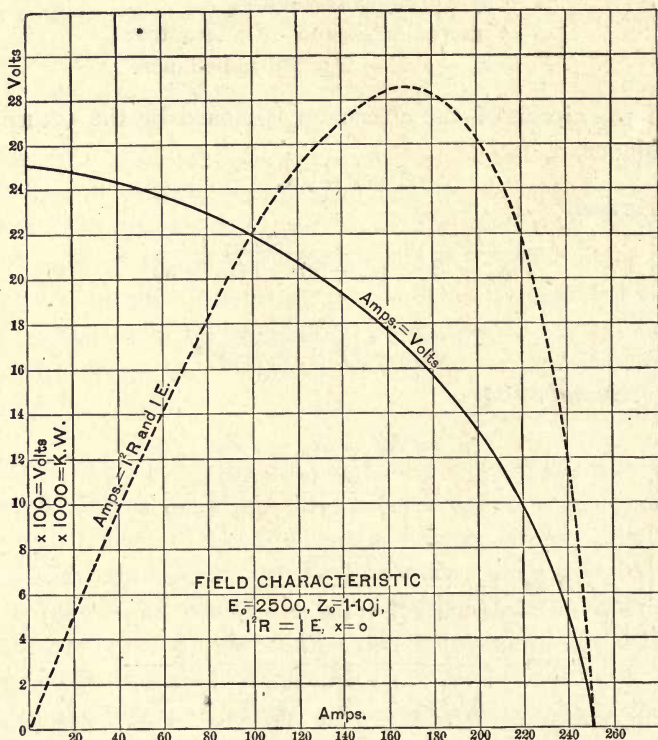


Fig. 113. Field Characteristic of Alternator on Non-inductive Load.

dotted lines, we have, for the following conditions of external circuit :

In Fig. 113, non-inductive external circuit, $x = 0$.

In Fig. 114, inductive external circuit, of the condition, $r/x = +.75$, with a power factor, .6.

In Fig. 115, inductive external circuit, of the condition, $r = 0$, with a power factor, 0.

In Fig. 116, external circuit with leading current, of the condition, $r/x = -.75$, with a power factor, .6.

In Fig. 117, external circuit with leading current, of the condition, $r = 0$, with a power factor, 0.

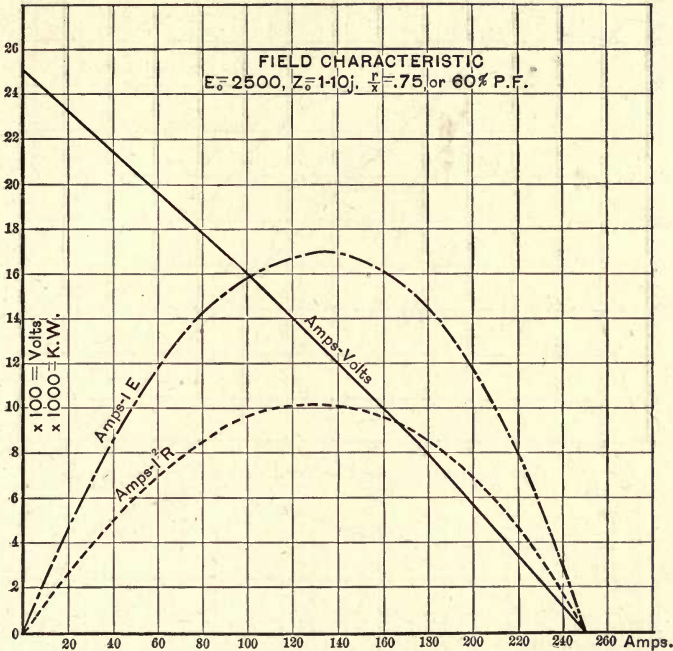


Fig. 114. Field Characteristic of Alternator, at 60% Power-factor on Inductive Load.

Such a curve is called a *field characteristic*.

As shown, the E.M.F. curve at non-inductive load is nearly horizontal at open circuit, nearly vertical at short circuit, and is similar to an arc of an ellipsis.

With reactive load the curves are more nearly straight lines.

The voltage drops rapidly on inductive, rises on capacity load.

The output increases from zero at open circuit to a maximum, and then decreases again to zero at short circuit.

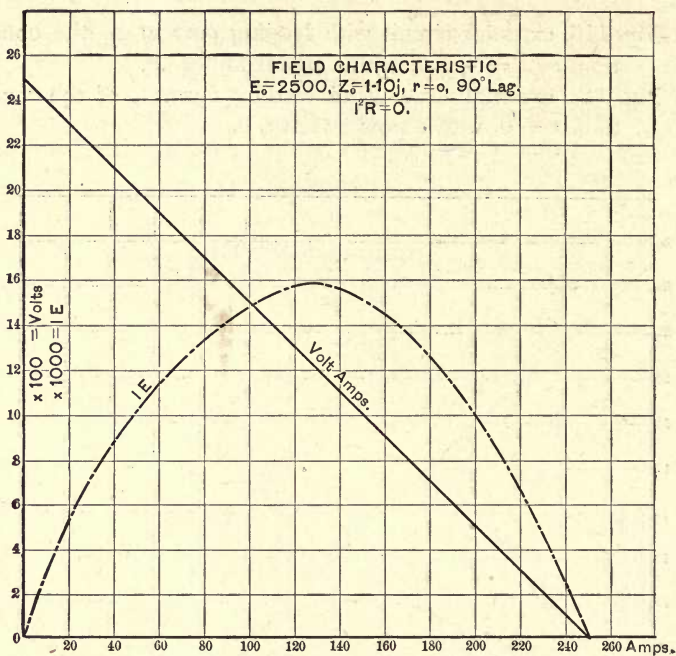


Fig. 115. Field Characteristic of Alternator, on Wattless Inductive Load.

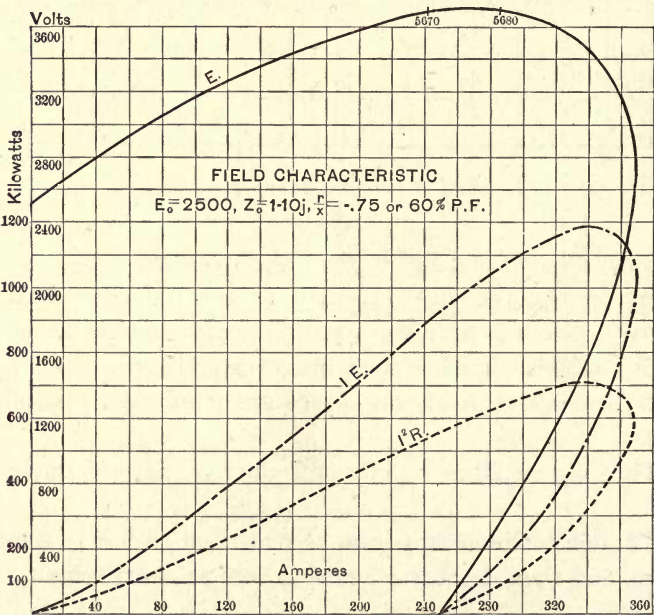


Fig. 116. Field Characteristic of Alternator, at 60% Power-factor on Condenser Load.

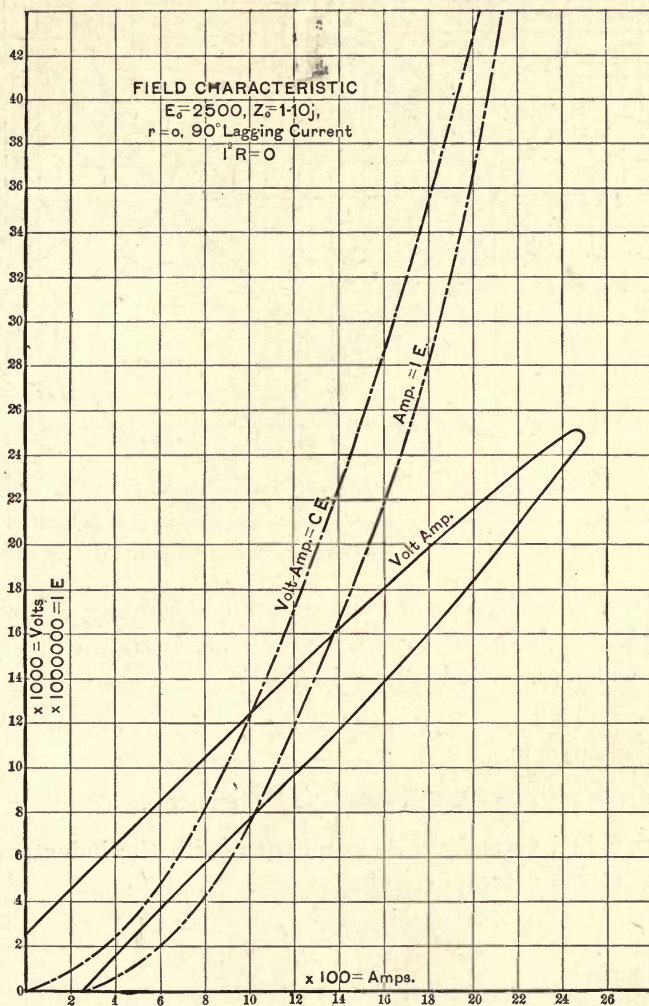


Fig. 117., Field Characteristic of Alternator, on Wattless Condenser Load.

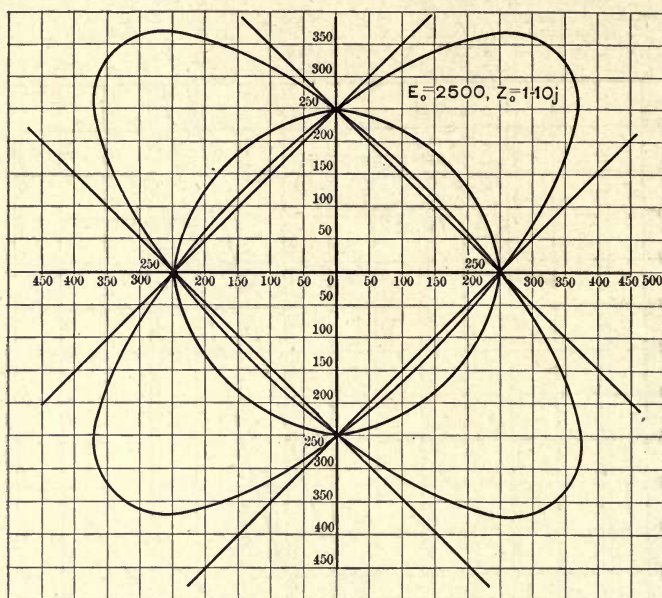


Fig. 118. Field Characteristic of Alternator.

165. The dependence of the terminal voltage, E , upon the phase relation of the external circuit is shown in Fig. 119, which gives, at impressed E.M.F.,

$$E_o = 2,500 \text{ volts,}$$

for the currents,

$$I = 50, 100, 150, 200, 250 \text{ amperes,}$$

the terminal voltages, E , as ordinates, with the inductance factor of the external circuit,

$$\frac{s}{\sqrt{r^2 + x^2}},$$

as abscissæ.

166. If the internal impedance is negligible compared with the external impedance, then, approximately,

$$E = \frac{E_o \sqrt{r^2 + x^2}}{\sqrt{(r_o + r)^2 + (x_o + x)^2}} = E_o;$$

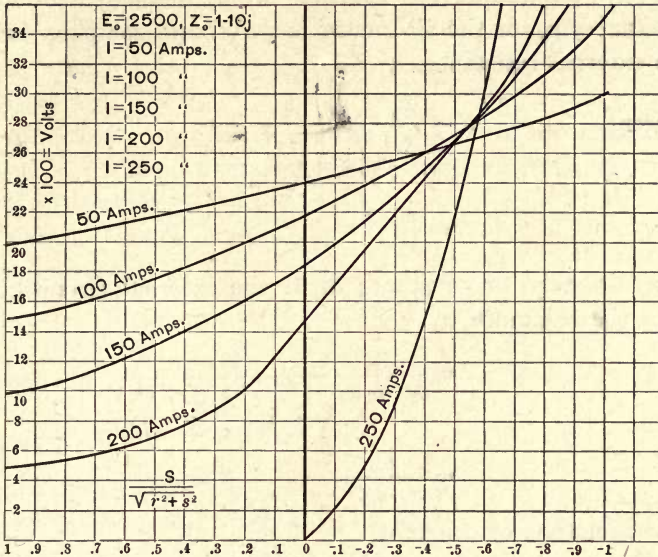


Fig. 119. Regulation of Alternator on Various Loads.

that is, an alternator with small internal resistance and synchronous reactance tends to regulate for constant terminal voltage.

Every alternator does this near open circuit, especially on non-inductive load.

Even if the synchronous reactance, x_o , is not quite negligible, this regulation takes place, to a certain extent, on non-inductive circuit, since for

$$x = 0, \quad E = \frac{E_o}{\sqrt{1 + 2 \frac{r_o}{r} + \frac{x_o^2}{r^2}}};$$

and thus the expression of the terminal voltage, E , contains the synchronous reactance, x_o , only as a term of second order in the denominator.

On inductive circuit, however, x_o appears in the denominator as a term of first order, and therefore constant potential regulation does not take place as well.

With a non-inductive external circuit, if the synchronous reactance, x_0 , of the alternator is very large compared with the external resistance, r ,

$$\begin{aligned} \text{current } I &= \frac{E_0}{x_0} \frac{1}{\sqrt{1 + \left(\frac{r_0 + r}{x_0}\right)^2}} \\ &= \frac{E_0}{x_0}, \end{aligned}$$

approximately, or constant; or, if the external circuit contains the reactance, x ,

$$\begin{aligned} I &= \frac{E_0}{x_0 + x} \frac{1}{\sqrt{1 + \left(\frac{r_0 + r}{x_0 + x}\right)^2}} \\ &= \frac{E_0}{x_0 + x}, \end{aligned}$$

approximately, or constant.

The terminal voltage of a non-inductive circuit is

$$E = \frac{E_0}{x_0} r,$$

approximately, or proportional to the external resistance.

If an inductive circuit,

$$E = \frac{E_0}{x_0 + x} \sqrt{r^2 + x^2},$$

approximately, or proportional to the external impedance.

167. That is, on a non-inductive external circuit, an alternator with very low synchronous reactance regulates for constant terminal voltage, as a constant-potential machine; an alternator with a very high synchronous reactance regulates for a terminal voltage proportional to the external resistance, as a constant-current machine.

Thus, every alternator acts as a constant-potential machine near open circuit, and as a constant-current machine near short circuit.

The modern alternators are generally more or less ma-

chines of the first class; the old alternators, as built by Jablockkoff, Gramme, etc., were machines of the second class, used for arc lighting, where constant-current regulation is an advantage.

Obviously, large external reactances cause the same regulation for constant current independently of the resistance, r , as a large internal reactance, x_0 .

On non-inductive circuit, if

$$I = \frac{E_0}{\sqrt{(r + r_0)^2 + x_0^2}},$$

$$E = \frac{E_0 r}{\sqrt{(r + r_0)^2 + x_0^2}},$$

the output is

$$P = IE = \frac{E_0^2 r}{(r + r_0)^2 + x_0^2};$$

and

$$\frac{dP}{dr} = \frac{x_0^2 - r^2 + r_0^2}{\{(r + r_0)^2 + x_0^2\}^2} E_0^2;$$

hence, if

$$x_0 = \sqrt{r^2 - r_0^2},$$

or

$$r = \sqrt{r_0^2 + x_0^2} = z_0;$$

then

$$\frac{dP}{dr} = 0.$$

That is, the power is a maximum, and

$$P = \frac{E_0^2}{2 \{z_0 + r_0\}},$$

$$E = \frac{E_0}{\sqrt{2 \left\{ 1 + \frac{r_0}{z_0} \right\}}},$$

and

$$I = \frac{E_0}{\sqrt{2 z_0 \{z_0 + r_0\}}}.$$

Therefore, with an external resistance equal to the internal impedance, or, $r = z_0 = \sqrt{r_0^2 + x_0^2}$, the output of an alternator is a maximum, and near this point it regulates for constant output; that is, an increase of current causes a proportional decrease of terminal voltage, and inversely.

The field characteristic of the alternator shows this effect plainly.

CHAPTER XVII.

SYNCHRONIZING ALTERNATORS.

168. All alternators, when brought to synchronism with each other, will operate in parallel more or less satisfactorily. This is due to the reversibility of the alternating-current machine ; that is, its ability to operate as synchronous motor. In consequence thereof, if the driving power of one of several parallel-operating generators is withdrawn, this generator will keep revolving in synchronism as a synchronous motor ; and the power with which it tends to remain in synchronism is the maximum power which it can furnish as synchronous motor under the conditions of running.

169. The principal and foremost condition of parallel operation of alternators is equality of frequency ; that is, the transmission of power from the prime movers to the alternators must be such as to allow them to run at the same frequency without slippage or excessive strains on the belts or transmission devices.

Rigid mechanical connection of the alternators cannot be considered as synchronizing ; since it allows no flexibility or phase adjustment between the alternators, but makes them essentially one machine. If connected in parallel, a difference in the field excitation, and thus the induced E.M.F. of the machines, must cause large cross-current ; since it cannot be taken care of by phase adjustment of the machines.

Thus rigid mechanical connection is not desirable for parallel operation of alternators.

170. The second important condition of parallel operation is uniformity of speed ; that is, constancy of frequency.

If, for instance, two alternators are driven by independent single-cylinder engines, and the cranks of the engines happen to be crossed, the one engine will pull, while the other is near the dead-point, and conversely. Consequently, alternately the one alternator will tend to speed up and the other slow down, then the other speed up and the first slow down. This effect, if not taken care of by fly-wheel capacity, causes a "hunting" or pumping action; that is, a fluctuation of the lights with the period of the engine revolution, due to the alternating transfer of the load from one engine to the other, which may even become so excessive as to throw the machines out of step. This difficulty does not exist with turbine or water-wheel driving.

171. In synchronizing alternators, we have to distinguish the phenomenon taking place when throwing the machines in parallel or out of parallel, and the phenomenon when running in synchronism.

When connecting alternators in parallel, they are first brought approximately to the same frequency and same voltage; and then, at the moment of approximate equality of phase, as shown by a phase-lamp or other device, they are thrown in parallel.

Equality of voltage is much less important with modern alternators than equality of frequency, and equality of phase is usually of importance only in avoiding an instantaneous flickering of the lights on the system. When two alternators are thrown together, currents pass between the machines, which accelerate the one and retard the other machine until equal frequency and proper phase relation are reached.

With modern ironclad alternators, this interchange of mechanical power is usually, even without very careful adjustment before synchronizing, sufficiently limited not to endanger the machines mechanically; since the cross-currents, and thus the interchange of power, are limited by self-induction and armature reaction.

In machines of very low armature reaction, that is, machines of "very good constant potential regulation," much greater care has to be exerted in the adjustment to equality of frequency, voltage, and phase, or the interchange of current may become so large as to destroy the machine by the mechanical shock; and sometimes the machines are so sensitive in this respect that it is preferable not to operate them in parallel. The same applies in getting out of step.

172. When running in synchronism, nearly all types of machines will operate satisfactorily; a medium amount of armature reaction is preferable, however, such as is given by modern alternators—not too high to reduce the synchronizing power too much, nor too low to make the machine unsafe in case of accident, such as falling out of step, etc.

If the armature reaction is very low, an accident,—such as a short circuit, falling out of step, opening of the field circuit, etc.,—may destroy the machine. If the armature reaction is very high, the driving-power has to be adjusted very carefully to constancy; since the synchronizing power of the alternators is too weak to hold them in step, and carry them over irregularities of the driving-power.

173. Series operation of alternators is possible only by rigid mechanical connection, or by some means whereby the machines, with regard to their synchronizing power, act essentially in parallel; as, for instance, by the arrangement shown in Fig. 120, where the two alternators, A_1 , A_2 , are connected in series, but interlinked by the two coils of a large transformer, T , of which the one is connected across the terminals of one alternator, and the other across the terminals of the other alternator in such a way that, when operating in series, the coils of the transformer will be without current. In this case, by interchange of power

through the transformers, the series connection will be maintained stable.

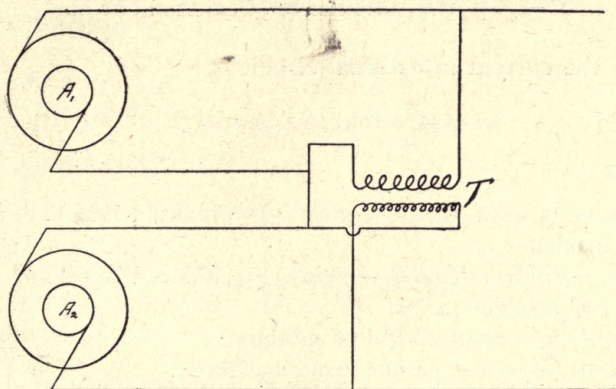


Fig. 120.

174. In two parallel operating alternators, as shown in Fig. 121, let the voltage at the common bus bars be assumed

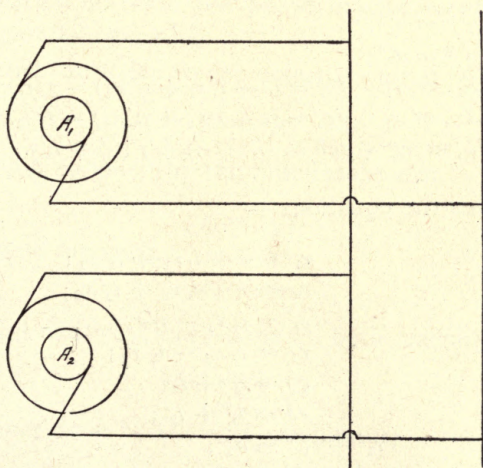


Fig. 121.

as zero line, or real axis of coördinates of the complex method; and let —

e = difference of potential at the common bus bars of the two alternators,

$Z = r - jx$ = impedance of external circuit,

$Y = g + jb$ = admittance of external circuit ;

hence, the current in external circuit is

$$I = \frac{e}{r - jx} = e(g + jb).$$

Let

$E_1 = e_1 - j e_1' = a_2 (\cos \hat{\omega}_1 - j \sin \hat{\omega}_1)$ = induced E.M.F. of first machine ;

$E_2 = e_2 - j e_2' = a_2 (\cos \hat{\omega}_2 - j \sin \hat{\omega}_2)$ = induced E.M.F. of second machine ;

$I_1 = i_1 + j i_1'$ = current of first machine ;

$I_2 = i_2 + j i_2'$ = current of second machine ;

$Z_1 = r_1 - j x_1$ = internal impedance, and $Y_1 = g_1 + j b_1$ = internal admittance, of first machine ;

$Z_2 = r_2 - j x_2$ = internal impedance, and $Y_2 = g_2 + j b_2$ = internal admittance, of second machine.

Then,

$$e_1^2 + e_1'^2 = a_1^2 ;$$

$$e_2^2 + e_2'^2 = a_2^2 ;$$

$E_1 = e + I_1 Z_1$, or $e_1 - j e_1' = (e + i_1 r_1 + i_1' x_1) - j(i_1 x_1 - i_1' r_1)$;

$E_2 = e + I_2 Z_2$, or $e_2 - j e_2' = (e + i_2 r_2 + i_2' x_2) - j(i_2 x_2 - i_2' r_2)$;

$I = I_1 + I_2$, or $eg + jeb = (i_1 + i_2) + j(i_1' + i_2')$.

This gives the equations —

$$e_1 = e + i_1 r_1 + i_1' x_1 ;$$

$$e_2 = e + i_2 r_2 + i_2' x_2 ;$$

$$e_1' = i_1 x_1 - i_1' r_1 ;$$

$$e_2' = i_2 x_2 - i_2' r_2 ;$$

$$eg = i_1 + i_2 ;$$

$$eb = i_1' + i_2' ;$$

$$e_1^2 + e_1'^2 = a_1^2 ;$$

$$e_2^2 + e_2'^2 = a_2^2 ;$$

or eight equations with nine variables: $e_1, e_1', e_2, e_2', i_1, i_1', i_2, i_2', e$.

Combining these equations by twos,

$$e_1 r_1 + e_1' x_1 = e r_1 + i_1 z_1^2;$$

$$e_2 r_2 + e_2' x_2 = e r_2 + i_2 z_2^2;$$

substituted in

$$i_1 + i_2 = e g,$$

we have

$$e_1 g_1 + e_1' b_1 + e_2 g_2 + e_2' b_2 = e (g_1 + g_2 + g);$$

and analogously,

$$e_1 b_1 - e_1' g_1 + e_2 b_2 - e_2' g_2 = e (b_1 + b_2 + b);$$

dividing,

$$\frac{g + g_1 + g_2}{b + b_1 + b_2} = \frac{e_1 g_1 + e_2 g_2 + e_1' b_1 + e_2' b_2}{e_1 b_1 + e_2 b_2 - e_1' g_1 - e_2' g_2};$$

substituting

$$g = v \cos \alpha \quad e_1 = a_1 \cos \hat{\omega}_1 \quad e_2 = a_2 \cos \hat{\omega}_2$$

$$b = v \sin \alpha \quad e_1' = a_1 \sin \hat{\omega}_1 \quad e_2' = a_2 \sin \hat{\omega}_2$$

gives

$$\frac{g + g_1 + g_2}{b + b_1 + b_2} = \frac{a_1 v_1 \cos (a_1 - \hat{\omega}_1) + a_2 v_2 \cos (a_2 - \hat{\omega}_2)}{a_1 v_1 \sin (a_1 - \hat{\omega}_1) + a_2 v_2 \sin (a_2 - \hat{\omega}_2)}$$

as the equation between the phase displacement angles $\hat{\omega}_1$ and $\hat{\omega}_2$ in parallel operation.

The power supplied to the external circuit is

$$p = e^2 g,$$

of which that supplied by the first machine is,

$$p_1 = e i_1;$$

by the second machine,

$$p_2 = e i_2.$$

The total electrical work done by both machines is,

$$P = P_1 + P_2,$$

of which that done by the first machine is,

$$P_1 = e_1 i_1 - e_1' i_1';$$

by the second machine,

$$P_2 = e_2 i_2 - e_2' i_2'.$$

The difference of output of the two machines is,

$$\Delta p = p_1 - p_2 = e(i_1 - i_2);$$

denoting

$$\frac{\hat{\omega}_1 + \hat{\omega}_2}{2} = \epsilon \quad \frac{\hat{\omega}_1 - \hat{\omega}_2}{2} = \delta.$$

$\Delta p / \Delta \delta$ may be called the synchronizing power of the machines, or the power which is transferred from one machine to the other by a change of the relative phase angle.

175. SPECIAL CASE. — *Two equal alternators of equal excitation.*

$$a_1 = a_2 = a \\ Z_1 = Z_2 = Z_0.$$

Substituting this in the eight initial equations, these assume the form, —

$$e_1 = e + i_1 r_0 + i_1' x_0 \\ e_2 = e + i_2 r_0 + i_2' x_0 \\ e_2' = i_1 x_0 - i_1' r_0 \\ e_2' = i_2 x_0 - i_2' r_0. \\ e g = i_1 + i_2 \\ e b = i_1' + i_2' \\ e_1^2 + e_1'^2 = e_2^2 + e_2'^2 = a^2.$$

Combining these equations by twos,

$$e_1 + e_2 = 2e + e(r_0 g + x_0 b) \\ e_1' + e_2' = e(x_0 g - r_0 b);$$

substituting

$$e_1 = a \cos \hat{\omega}_1 \\ e_1' = a \sin \hat{\omega}_1 \\ e_2 = a \cos \hat{\omega}_2 \\ e_2' = a \sin \hat{\omega}_2,$$

we have $a(\cos \hat{\omega}_1 + \cos \hat{\omega}_2) = e(2 + r_0 g + x_0 b)$
 $a(\sin \hat{\omega}_1 + \sin \hat{\omega}_2) = e(x_0 g - r_0 b);$

expanding and substituting —

$$\epsilon = \frac{\hat{\omega}_1 + \hat{\omega}_2}{2} \\ \delta = \frac{\hat{\omega}_1 - \hat{\omega}_2}{2};$$

or ,
$$a \cos \epsilon \cos \delta = e \left(1 + \frac{r_0 g + x_0 b}{2} \right)$$

$$a \sin \epsilon \cos \delta = e \frac{x_0 g - r_0 b}{2};$$
hence
$$\tan \epsilon = \frac{x_0 g - r_0 b}{2 + r_0 g + x_0 b} = \text{constant}.$$

That is
$$\hat{\omega}_1 + \hat{\omega}_2 = \text{constant};$$

and
$$\cos \delta = \frac{e}{a} \sqrt{\left(1 + \frac{r_0 g + x_0 b}{2} \right)^2 + \left(\frac{x_0 g - r_0 b}{2} \right)^2};$$

or,
$$e = \frac{a \cos \delta}{\sqrt{\left(1 + \frac{r_0 g + x_0 b}{2} \right)^2 + \left(\frac{x_0 g - r_0 b}{2} \right)^2}};$$

at no-phase displacement between the alternators, or,

$$\delta = \frac{\hat{\omega}_1 - \hat{\omega}_2}{2} = 0;$$

we have
$$e = \frac{a}{\sqrt{\left(1 + \frac{r_0 g + x_0 b}{2} \right)^2 + \left(\frac{x_0 g - r_0 b}{2} \right)^2}}.$$

From the eight initial equations we get, by combination —

$$e_1 r_0 + i_1' x_0 = e (r_0 + x_0) + i_1 (r_0^2 + x_0^2)$$

$$e_2 r_0 + e_2' x_0 = e (r_0 + x_0) + i_1 (r_0^2 + x_0^2);$$

subtracted and expanded —

$$i_1 - i_2 = \frac{r_0 (e_1 - e_2) + x_0 (e_1' - e_2')}{Z_0^2};$$

or, since

$$e_1 - e_2 = a (\cos \hat{\omega}_1 - \cos \hat{\omega}_2) = -2 a^2 \sin \epsilon \sin \delta$$

$$e_1' - e_2' = a (\sin \hat{\omega}_1 - \sin \hat{\omega}_2) = 2 a \cos \epsilon \sin \delta;$$

we have

$$i_1 - i_2 = \frac{2 a \sin \delta}{z_0^2} \{x_0 \cos \epsilon - r_0 \sin \epsilon\}$$

$$= 2 a y_0 \sin \delta \cos (\epsilon + \alpha),$$

where

$$\tan \alpha = \frac{x_0}{r_0}.$$

The difference of output of the two alternators is

$$\Delta p = p_1 - p_2 = e (i_1 - i_2);$$

hence, substituting,

$$\Delta p = \frac{2ae \sin \delta}{z_0^2} \{x_0 \cos \epsilon - r_0 \sin \epsilon\};$$

substituting,

$$e = \frac{a \cos \delta}{\sqrt{\left(1 + \frac{r_0 g + x_0 b}{2}\right)^2 + \left(\frac{x_0 g - r_0 b}{2}\right)^2}};$$

$$\sin \epsilon = \frac{\frac{x_0 g - r_0 b}{2}}{\sqrt{\left(1 + \frac{r_0 g + x_0 b}{2}\right)^2 + \left(\frac{x_0 g - r_0 b}{2}\right)^2}};$$

$$\cos \epsilon = \frac{1 + \frac{r_0 g + x_0 b}{2}}{\sqrt{\left(1 + \frac{r_0 g + x_0 b}{2}\right)^2 + \left(\frac{x_0 g - r_0 b}{2}\right)^2}}$$

we have,

$$\Delta p = \frac{2a^2 \sin \delta \cos \delta \left\{x_0 \left(1 + \frac{r_0 g + x_0 b}{2}\right) - r_0 \left(\frac{x_0 g - r_0 b}{2}\right)\right\}}{z_0^2 \left\{\left(1 + \frac{r_0 g + x_0 b}{2}\right)^2 + \left(\frac{x_0 g - r_0 b}{2}\right)^2\right\}}$$

expanding,

$$\Delta p = \frac{a^2 \sin 2\delta \left\{x_0 + \frac{g z_0^2}{2}\right\}}{z_0^2 \{1 + r_0 g + x_0 b + z_0^2 v^2\}};$$

or

$$\Delta p = \frac{a^2 \sin 2\delta \left\{b_0 + \frac{b}{2}\right\}}{y_0^2 + g g_0 + b b_0 + v^2};$$

$$\frac{\Delta p}{\Delta \delta} = \frac{2a^2 \cos 2\delta \left\{b_0 + \frac{b}{2}\right\}}{y_0^2 + g g_0 + b b_0 + y^2}.$$

Hence, the transfer of power between the alternators, Δp , is a maximum, if $\delta = 45^\circ$; or $\hat{\omega}_1 - \hat{\omega}_2 = 90^\circ$; that is, when the alternators are in quadrature.

The synchronizing power, $\Delta p / \Delta \delta$, is a maximum if $\delta = 0$; that is, the alternators are in phase with each other.

176. As an instance, curves may be plotted for,

$$a = 2500,$$

$$Z_0 = r_1 - jx_0 = 1 - 10j; \text{ or } Y_0 = g_0 + jb_0 = .01 + .1j,$$

with the angle $\delta = \frac{\hat{\omega}_1 - \hat{\omega}_2}{2}$ as abscissæ, giving

the value of terminal voltage, e ;

the value of current in the external circuit, $i = ey$;

the value of interchange of current between the alternators,

$$i_1 - i_2;$$

the value of interchange of power between the alternators, Δp

$$= p_1 - p_2;$$

the value of synchronizing power, $\frac{\Delta p}{\Delta \delta}$, in dash-dot line, Curve V.

For the condition of external circuit,

$g = 0,$	$b = 0,$	$y = 0,$
.05,	0,	.05,
.08,	0,	.08,
.03,	+ .04,	.05,
.03,	- .04,	.05.

CHAPTER XVIII.

SYNCHRONOUS MOTOR.

177. In the chapter on synchronizing alternators we have seen that when an alternator running in synchronism is connected with a system of given E.M.F., the work done by the alternator can be either positive or negative. In the latter case the alternator consumes electrical, and consequently produces mechanical, power; that is, runs as a synchronous motor, so that the investigation of the synchronous motor is already contained essentially in the equations of parallel-running alternators.

Since in the foregoing we have made use mostly of the symbolic method, we may in the following, as an instance of the graphical method, treat the action of the synchronous motor diagrammatically.

Let an alternator of the E.M.F., E_1 , be connected as synchronous motor with a supply circuit of E.M.F., E_0 , by a circuit of the impedance Z .

If E_0 is the E.M.F. impressed upon the motor terminals, Z is the impedance of the motor of induced E.M.F., E_1 . If E_0 is the E.M.F. at the generator terminals, Z is the impedance of motor and line, including transformers and other intermediate apparatus. If E_0 is the induced E.M.F. of the generator, Z is the sum of the impedances of motor, line, and generator, and thus we have the problem, generator of induced E.M.F. E_0 , and motor of induced E.M.F. E_1 ; or, more general, two alternators of induced E.M.Fs., E_0 , E_1 , connected together into a circuit of total impedance, Z .

Since in this case several E.M.Fs. are acting in circuit

with the same current, it is convenient to use the current, I , as zero line \overline{OI} of the polar diagram.

If $I = i =$ current, and $Z =$ impedance, $r =$ effective resistance, $x =$ effective reactance, and $z = \sqrt{r^2 + x^2} =$ absolute value of impedance, then the E.M.F. consumed by the resistance is $E_1 = ri$, and in phase with the current, hence represented by vector OE_1 ; and the E.M.F. consumed by the reactance is $E_2 = xi$, and 90° ahead of the current, hence the E.M.F. consumed by the impedance is $E = \sqrt{(E_1)^2 + (E_2)^2}$, or $= i \sqrt{r^2 + x^2} = iz$, and ahead of the current by the angle δ , where $\tan \delta = x/r$.

We have now acting in circuit the E.M.F.s., E, E_1, E_0 ; or E_1 and E are components of E_0 ; that is, E_0 is the diagonal of a parallelogram, with E_1 and E as sides.

Since the E.M.F.s. E_1, E_2, E , are represented in the diagram, Fig. 122, by the vectors $\overline{OE_1}, \overline{OE_2}, \overline{OE}$, to get the parallelogram of E_0, E_1, E , we draw arc of circle around O with E_0 , and around E with E_1 . Their point of intersection gives the impressed E.M.F., $\overline{OE_0} = E_0$, and completing the parallelogram OE, E_0, E_1 , we get $\overline{OE_1} = E_1$, the induced E.M.F. of the motor.

$\angle IOE_0$ is the difference of phase between current and impressed E.M.F., or induced E.M.F. of the generator.

$\angle IOE_1$ is the difference of phase between current and induced E.M.F. of the motor.

And the power is the current i times the projection of the E.M.F. upon the current, or the zero line \overline{OI} .

Hence, dropping perpendiculars, $\overline{E_0E_0^1}$ and $\overline{E_1E_1^1}$, from E_0 and E_1 upon \overline{OI} , it is —

$P_0 = i \times \overline{OE_0^1} =$ power supplied by induced E.M.F. of generator.

$P_1 = i \times \overline{OE_1^1} =$ electric power transformed in mechanical power by the motor.

$P = i \times \overline{OE_1} =$ power consumed in the circuit by effective resistance.

Obviously $P_0 = P_1 + P$.

Since the circles drawn with E_0 and E_1 around O and E respectively intersect twice, two diagrams exist. In general, in one of these diagrams shown in Fig. 122 in drawn

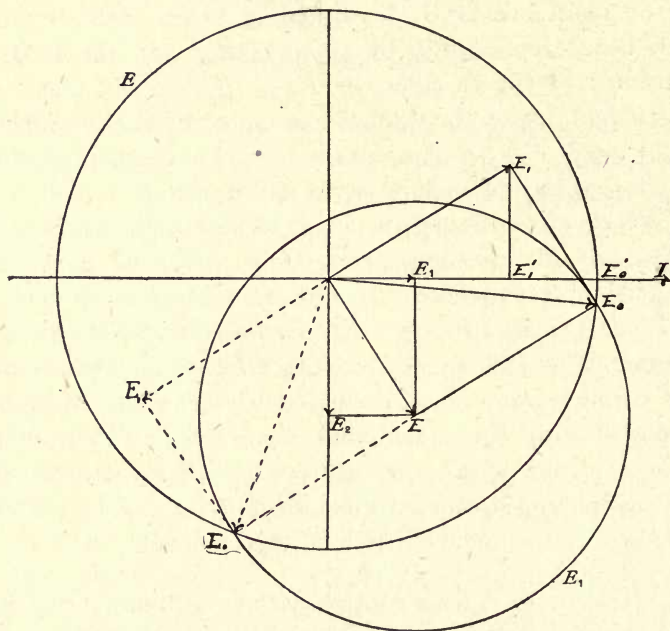


Fig. 122.

lines, current and E.M.F. are in the same direction, representing mechanical work done by the machine as motor. In the other, shown in dotted lines, current and E.M.F. are in opposite direction, representing mechanical work consumed by the machine as generator.

Under certain conditions, however, E_0 is in the same, E_1 in opposite direction, with the current; that is, both machines are generators.

178. It is seen that in these diagrams the E.M.F.s. are considered from the point of view of the motor; that is,

The phase relation of the current with the E.M.Fs. E_1 , E_0 , depends upon the current strength and the E.M.Fs. E_1 and E_0 .

179. Figs. 123 to 125 show several such diagrams for different values of E_1 , but the same value of I and E_0 . The motor diagram being given in drawn line, the generator diagram in dotted line.

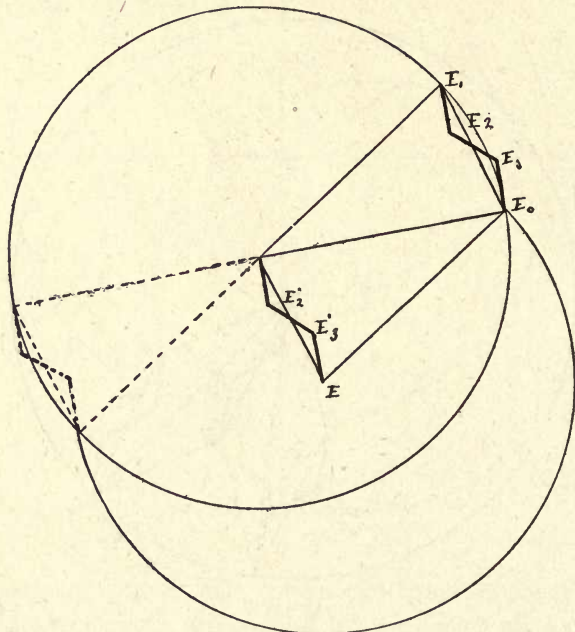


Fig. 124.

As seen, for small values of E_1 the potential drops in the alternator and in the line. For the value of $E_1 = E_0$ the potential rises in the generator, drops in the line, and rises again in the motor. For larger values of E_1 , the potential rises in the alternator as well as in the line, so that the highest potential is the induced E.M.F. of the motor, the lowest potential the induced E.M.F. of the generator.

It is of interest now to investigate how the values of these quantities change with a change of the constants.

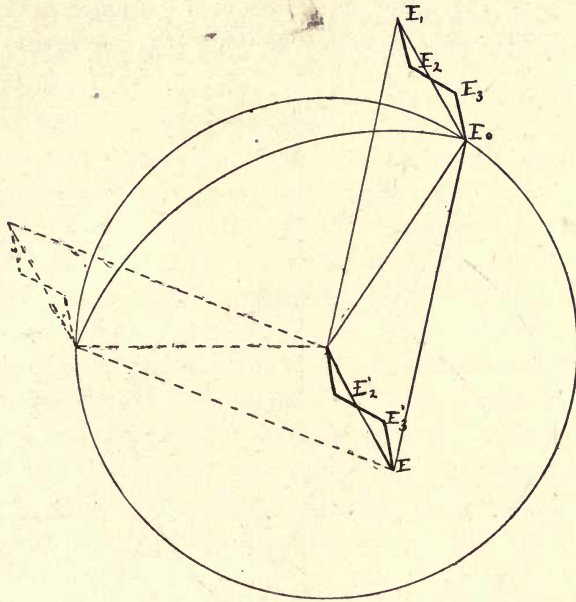


Fig. 125.

180. A. — *Constant impressed E.M.F. E_0 , constant current strength $I = i$, variable motor excitation E_1 .* (Fig. 126.)

If the current is constant, $= i$; \overline{OE} , the E.M.F. consumed by the impedance, and therefore point E , are constant. Since the intensity, but not the phase of E_0 is constant, E_0 lies on a circle e_0 with E_0 as radius. From the parallelogram, OE, E_0, E_1 follows, since $\overline{E_1 E_0}$ parallel and $= \overline{OE}$, that E_1 lies on a circle e_1 congruent to the circle e_0 , but with E_1 , the image of E , as center: $\overline{OE_1} = \overline{OE}$.

We can construct now the variation of the diagram with the variation of E_1 ; in the parallelogram OE, E_0, E_1 , O and E are fixed, and E_0 and E_1 move on the circles e_0, e_1 so that $\overline{E_0 E_1}$ is parallel to \overline{OE} .

The smallest value of E_1 consistent with current strength I is $\overline{01}_1 = E_1$, $\overline{01} = E_0$. In this case the power of the motor is $01_1^1 \times I$, hence already considerable. Increasing E_1 to $\overline{02}_1$, $\overline{03}_1$, etc., the impressed E.M.F.s. move to $\overline{02}$, $\overline{03}$, etc., the power is $I \times \overline{02}_1^1$, $I \times \overline{03}_1^1$, etc., increases first,

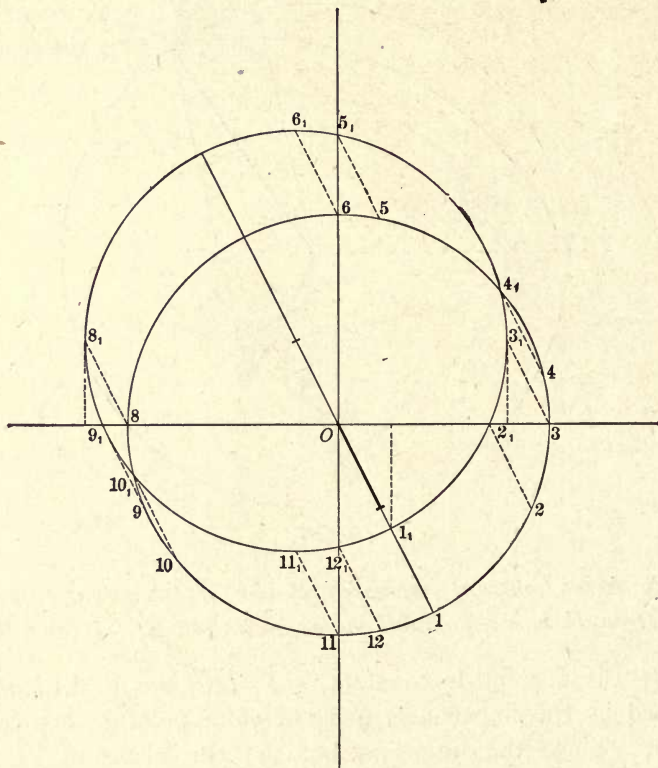


Fig. 126.

reaches the maximum at the point 3_1 , 3 , the most extreme point at the right, with the impressed E.M.F. in phase with the current, and then decreases again, while the induced E.M.F. of the motor E_1 increases and becomes $= E_0$ at 4_1 , 4 . At 5_1 , 5 , the power becomes zero, and further on negative; that is, the motor has changed to a dynamo, and

produces electrical energy, while the impressed E.M.F. E_0 still furnishes electrical energy, that is, both machines as generators feed into the line, until at $6_1, 6$, the power of the impressed E.M.F. E_0 becomes zero, and further on power begins to flow back; that is, the motor is changed to a generator and the generator to a motor, and we are on the generator side of the diagram. At $7_1, 7$, the maximum value of E_1 , consistent with the current C , has been reached, and passing still further the E.M.F. E_1 decreases again, while the power still increases up to the maximum at $8_1, 8$, and then decreases again, but still E_1 remaining generator, E_0 motor, until at $11_1, 11$, the power of E_0 becomes zero; that is, E_0 changes again to a generator, and both machines are generators, until at $12_1, 12$, where the power of E_1 is zero, E_1 changes from generator to motor, and we come again to the motor side of the diagram, and while E_1 still decreases, the power of the motor increases until $1_1, 1$, is reached.

Hence, there are two regions, for very large E_1 from 6 to 7, and for very small E_1 from 11 to 12, where both machines are generators; otherwise the one is generator, the other motor.

For small values of E_1 the current is lagging, begins, however, at 2 to lead the induced E.M.F. of the motor E_1 , at 3 the induced E.M.F. of the generator E_0 .

It is of interest to note that at the smallest possible value of $E_1, 1_1$, the power is already considerable. Hence, the motor can run under these conditions only at a certain load. If this load is thrown off, the motor cannot run with the same current, but the current must increase. We have here the curious condition that loading the motor reduces, unloading increases, the current within the range between 1 and 12.

The condition of maximum output is 3, current in phase with impressed E.M.F. Since at constant current the loss is constant, this is at the same time the condition of maximum efficiency: no displacement of phase of the impressed

E.M.F., or self-induction of the circuit compensated by the effect of the lead of the motor current. This condition of maximum efficiency of a circuit we have found already in Chapter VIII. on Inductance and Capacity.

181. B. E_0 and E_1 constant, I variable.

Obviously E_0 lies again on the circle e_0 with E_0 as radius and O as center.

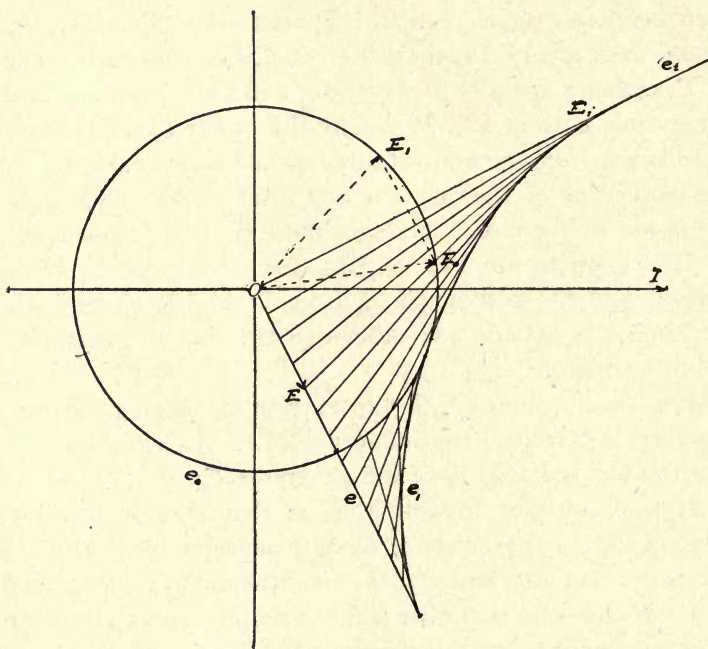


Fig. 127.

E lies on a straight line e , passing through the origin.

Since in the parallelogram $OE E_0 E_1$, $\overline{EE_0} = E_1$, we derive E_0 by laying a line $\overline{EE_0} = E_1$ from any point E in the circle e_0 , and complete the parallelogram.

All these lines $\overline{EE_0}$ envelop a certain curve e_1 , which

can be considered as the characteristic curve of this problem, just as circle e_1 in the former problem.

These curves are drawn in Figs. 127, 128, 129, for the three cases: 1st, $E_1 = E_0$; 2d, $E_1 < E_0$; 3d, $E_1 > E_0$.

In the first case, $E_1 = E_0$ (Fig. 127), we see that at

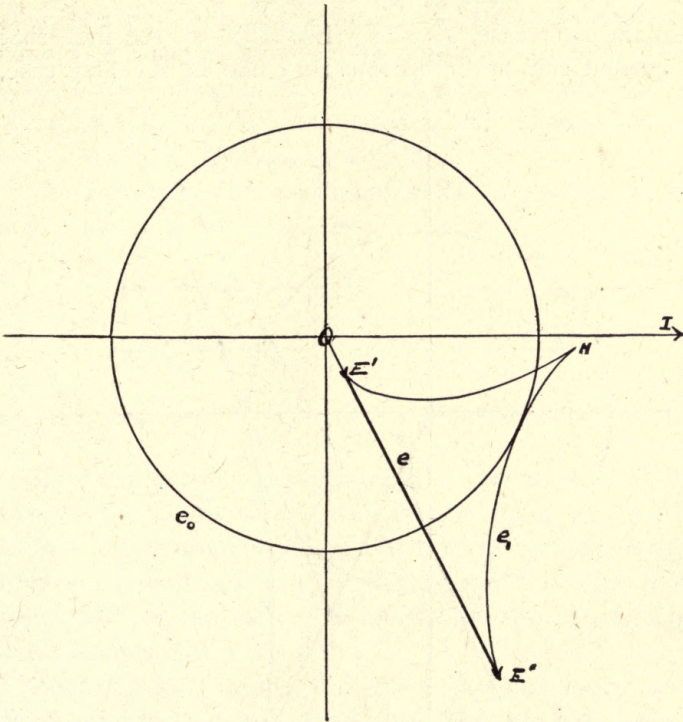


Fig. 128.

very small current, that is very small \overline{OE} , the current I leads the impressed E.M.F. E_0 by an angle $E_0OC = \hat{\omega}_0$. This lead decreases with increasing current, becomes zero, and afterwards for larger current, the current lags. Taking now any pair of corresponding points E, E_0 , and producing $\overline{EE_0}$ until it intersects e_i , in E_i we have $\angle E_i OE = 90^\circ$, $\overline{E_1} = \overline{E_0}$, thus: $\overline{OE_1} = \overline{EE_0} = \overline{OE_0} = \overline{E_0E_i}$; that is, $\overline{EE_i} =$

$2E_0$. That means the characteristic curve e_1 is the envelope of lines $\overline{EE_i}$, of constant lengths $2E_0$, sliding between the legs of the right angle $E_i OE$; hence, it is the sextic hypocycloid osculating circle e_0 , which has the general equation, with e, e_i as axes of coördinates :

$$\sqrt[3]{H^2} + \sqrt[3]{y^2} = \sqrt[3]{4E_0^2}$$

In the next case, $E_1 < E_0$ (Fig. 128) we see first, that the current can never become zero like in the first case,

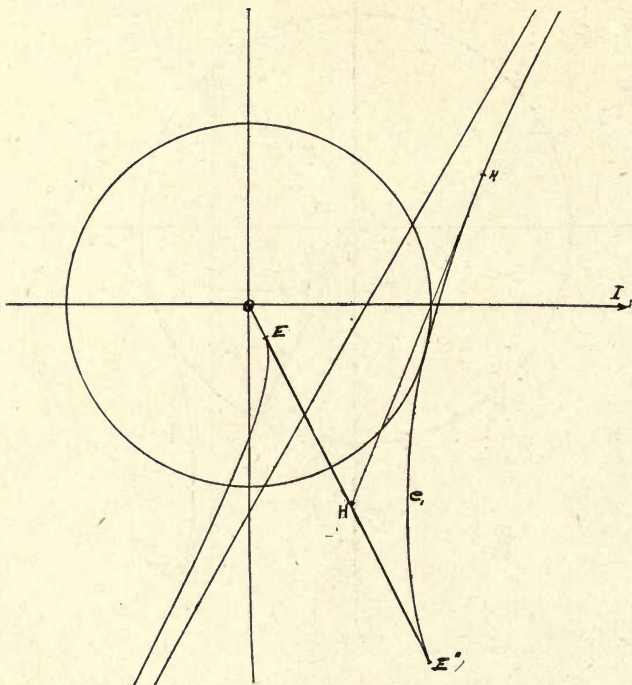


Fig. 129.

$E_1 = E_0$, but has a minimum value corresponding to the minimum value of $\overline{OE_1}$: $I_1' = \frac{E_0 - E_1}{s}$, and a maximum value: $I_1' = \frac{E_0 + E_1}{s}$. Furthermore, the current can never lead the impressed E.M.F. E_0 , but always lags. The mini-

mum lag is at the point H . The locus e_1 , as envelope of the lines $\overline{EE_0}$, is a finite sextic curve, shown in Fig. 128.

In the case $E_1 > E_0$ (Fig. 129) the current cannot equal zero either, but begins at a finite value C'_1 , corresponding to the minimum value of $\overline{OE_0}$: $I'_1 = \frac{E_1 - E_0}{z}$. At this value however, the alternator E_1 is still generator and changes to a motor, its power passing through zero, at the point corresponding to the vertical tangent, onto e_1 , with a very large lead of the impressed E.M.F. against the current. At H the lead changes to lag.

The minimum and maximum value of current in the three conditions are given by :

$$1st. \quad I = 0, \quad I = \frac{2E_0}{z}.$$

$$2d. \quad I = \frac{E_0 - E_1}{z}, \quad I = \frac{E_0 + E_1}{z},$$

$$3d. \quad I = \frac{E_1 - E_0}{z}, \quad I = \frac{E_0 + E_1}{z},$$

Since the current passing over the line at $E_1 = 0$, that is, when the motor stands still, is $I_0 = E_0/z$, we see that in such a synchronous motor-plant, when running at synchronism, the current can rise far beyond the value it has at standstill of the motor, to twice this value at 1, somewhat less at 2, but more at 3.

Hence in such a case, if the synchronous motor drops out of step, the current passing over the line goes down to one-half or less ; or, in other words, in such a system the motor, under certain conditions of running, is more liable to burn up than when getting out of step.

182. C. $E_0 = \text{constant}$, E_1 varied so that the efficiency is a maximum for all currents. (Fig. 130.)

Since we have seen that the output at a given current strength, that is, a given loss, is a maximum, and therefore

the efficiency a maximum, when the current is in phase with the induced E.M.F. E_0 of the generator, we have as the locus of E_0 the point E_0 (Fig. 130), and when E with increasing current varies on e , E_1 must vary on the straight line e_1 parallel to e .

Hence, at no-load or zero current, $E_1 = E_0$, decreases with increasing load, reaches a minimum at $\overline{OE_1^1}$ perpendicular to e_1 , and then increases again, reaches once more

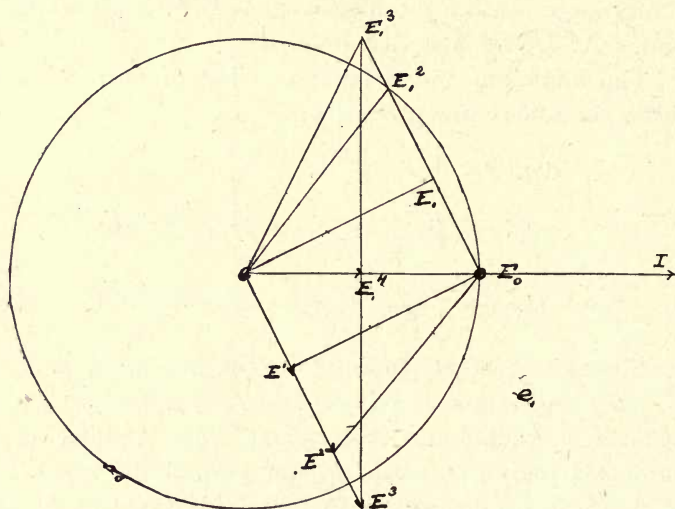


Fig. 130.

$E_1 = E_0$ at E_1^2 , and then increases beyond E_0 . The current is always ahead of the induced E.M.F. E_1 of the motor, and by its lead compensates for the self-induction of the system, making the total circuit non-inductive.

The power is a maximum at E_1^3 , where $\overline{OE_1^4} = \overline{E_1^4 E_0} = 1/2 \times \overline{OE_0}$, and is then $= I \times \overline{EO}/2$. Hence, since $\overline{OE_1^4} = Ir = E_0/2$, $I = E_0/2r$ and $P = E_0^2/4r$, hence $=$ the maximum power which, over a non-inductive line of resistance r can be transmitted, at 50 per cent. efficiency, into a non-inductive circuit.

In this case,

$$E_1^2 = \frac{z}{r} \times \frac{E_0}{2} = \frac{E_0}{2} \sqrt{1 + \left(\frac{x}{r}\right)^2}.$$

In general, it is, taken from the diagram, at the condition of maximum efficiency :

$$E_1 = \sqrt{(E_0 - Ir)^2 + i^2 x^2}.$$

Comparing these results with those in Chapter IX. on Self-induction and Capacity, we see that the condition of maximum efficiency of the synchronous motor system is the same as in a system containing only inductance and capacity, the lead of the current against the induced E.M.F. E_1 here acting in the same way as the condenser capacity in Chapter IX.

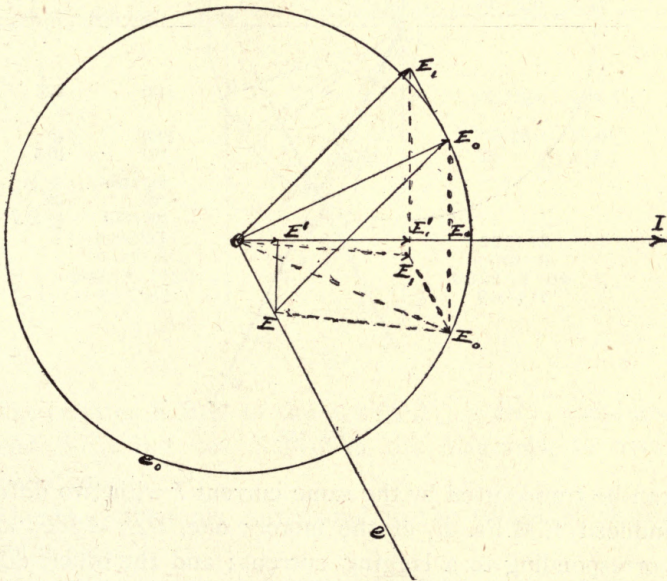


Fig. 131.

183. D. $E_0 = \text{constant}$; $P = \text{constant}$.

If the power of a synchronous motor remains constant, we have (Fig. 131) $I \times \overline{OE_1} = \text{constant}$, or, since $\overline{OE_1} =$

$I r$, $I = \overline{OE}^1 / r$, and: $\overline{OE}^1 \times \overline{OE}_1^1 = \overline{OE} \times \overline{E}^1 E_0^1 =$ constant.

Hence we get the diagram for any value of the current I , at constant power P_1 , by making $\overline{OE}^1 = I r$, $\overline{E}^1 E_0^1 = P_1 / C$ erecting in E_0^1 a perpendicular, which gives two points of intersection with circle e_0 , E_0 , one leading, the other lagging. Hence, at a given impressed E.M.F. E_0 , the same power P_1

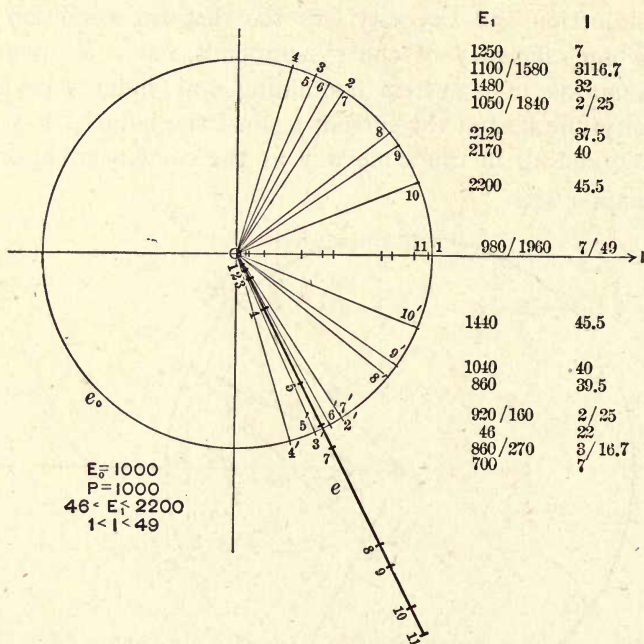


Fig. 132.

can be transmitted by the same current I with two different induced E.M.F.s. E_1 of the motor; one, $\overline{OE}_1 = \overline{EE}_0$ small, corresponding to a lagging current; and the other, $\overline{OE}_1 = \overline{EE}_0$ large, corresponding to a leading current. The former is shown in dotted lines, the latter in drawn lines, in the diagram, Fig. 131.

Hence a synchronous motor can work with a given output, at the same current with two different counter E.M.F.s.

E_1 , and at the same counter E.M.F. E_1 , at two different currents I . In one of the cases the current is leading, in the other lagging.

In Figs. 132 to 135 are shown diagrams, giving the points

E_0 = impressed E.M.F., assumed as constant = 1000 volts,

E = E.M.F. consumed by impedance,

E' = E.M.F. consumed by resistance.

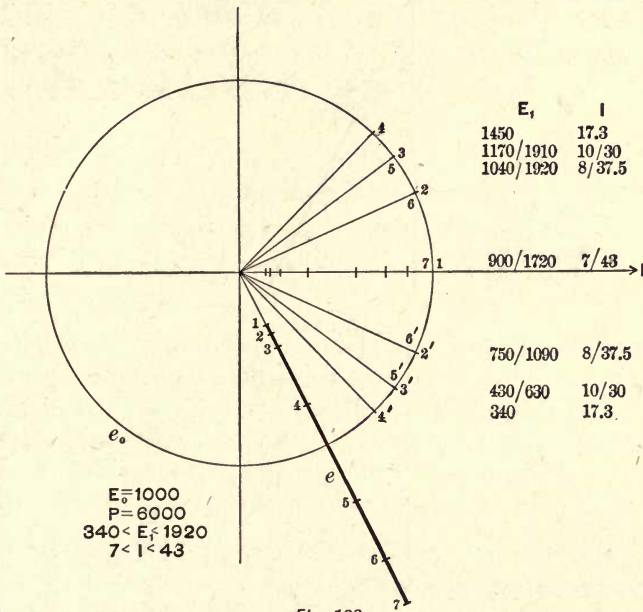


Fig. 133.

The counter E.M.F. of the motor, E_1 , is $\overline{OE_1}$, equal and parallel $\overline{EE_0}$, but not shown in the diagrams, to avoid complication.

The four diagrams correspond to the values of power, or motor output,

$P = 1,000, 6,000, 9,000, 12,000$ watts, and give :

$P = 1,000$ $46 < E < 2,200,$ $1 < I < 49$ Fig. 132.

$P = 6,000$ $340 < E_1 < 1,920,$ $7 < I < 43$ Fig. 133.

$P = 9,000$ $540 < E_1 < 1,750,$ $11.8 < I < 38.2$ Fig. 134.

$P = 12,000$ $920 < E_1 < 1,320,$ $20 < I < 30$ Fig. 135.

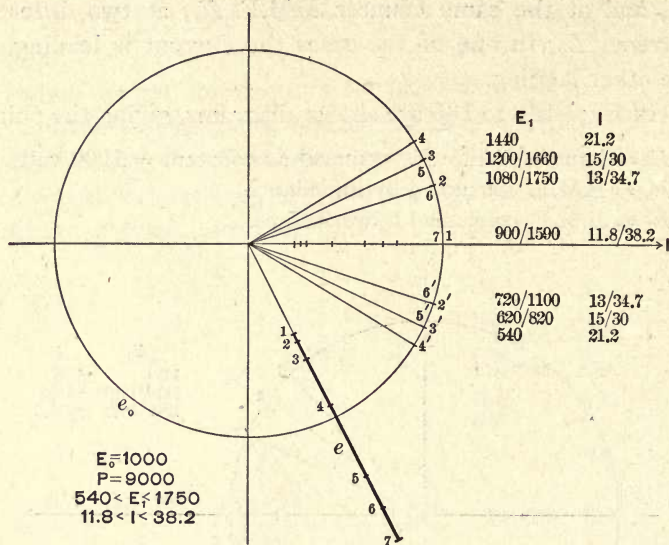


Fig. 134.

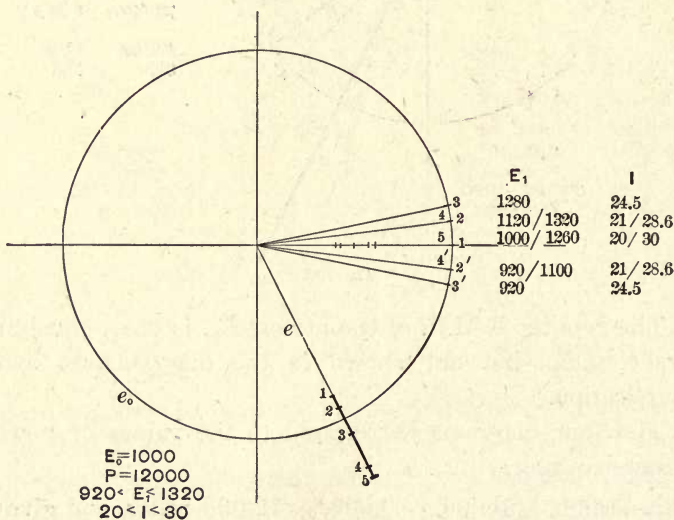


Fig. 135.

As seen, the permissible value of counter E.M.F. E_1 and of current I , becomes narrower with increasing output.

In the diagrams, different points of E_0 are marked with 1, 2, 3 . . . , when corresponding to leading current, with 2¹, 3¹, . . . , when corresponding to lagging current.

The values of counter E.M.F. E_1 and of current I are noted on the diagrams, opposite to the corresponding points E_0 .

In this condition it is interesting to plot the current as function of the induced E.M.F. E_1 of the motor, for constant power P_1 . Such curves are given in Fig. 139 and explained in the following on page 278.

184. While the graphic method is very convenient to get a clear insight into the interdependence of the different quantities, for numerical calculation it is preferable to express the diagrams analytically.

For this purpose,

Let $z = \sqrt{r^2 + x^2}$ = impedance of the circuit of (equivalent) resistance r and (equivalent) reactance $x = 2\pi NL$, containing the impressed E.M.F. e_0^* and the counter E.M.F. e_1 of the synchronous motor; that is, the E.M.F. induced in the motor armature by its rotation through the (resultant) magnetic field.

Let i = current in the circuit (effective values).

The mechanical power delivered by the synchronous motor (including friction and core loss) is the electric power consumed by the C.E.M.F. e_1 ; hence —

$$p = i e_1 \cos(i_1 e_1), \tag{1}$$

thus, —

$$\left. \begin{aligned} \cos(i_1 e_1) &= \frac{p}{i e_1} \\ \sin(i_1 e_1) &= \sqrt{1 - \left(\frac{p}{i e_1}\right)^2} \end{aligned} \right\} \tag{2}$$

* If e_0 = E.M.F. at motor terminals, z = internal impedances of the motor; if e_0 = terminal voltage of the generator, z = total impedance of line and motor; if e_0 = E.M.F. of generator, that is, E.M.F. induced in generator armature by its rotation through the magnetic field, z includes the generator impedance also.

The displacement of phase between current i and E.M.F. $e = z i$ consumed by the impedance z is :

$$\left. \begin{aligned} \cos (i e) &= \frac{r}{z} \\ \sin (i e) &= \frac{x}{z} \end{aligned} \right\} \quad (3)$$

Since the three E.M.Fs. acting in the closed circuit :

$$\begin{aligned} e_0 &= \text{E.M.F. of generator,} \\ e_1 &= \text{C.E.M.F. of synchronous motor,} \\ e &= z i = \text{E.M.F. consumed by impedance,} \end{aligned}$$

form a triangle, that is, e_1 and e are components of e_0 , it is (Fig. 136) :

$$e_0^2 = e_1^2 + e^2 + 2 e e_1 \cos (e_1 e), \quad (4)$$

$$\text{hence, } \cos (e_1, e) = \frac{e_0^2 - e_1^2 - e^2}{2 e_1 e} = \frac{e_0^2 - e_1^2 - z^2 i^2}{2 z i e_1}, \quad (5)$$

since, however, by diagram :

$$\begin{aligned} \cos (e_1, e) &= \cos (i, e - i, e_1) \\ &= \cos (i, e) \cos (i, e_1) + \sin (i, e) \sin (i, e_1) \end{aligned} \quad (6)$$

substitution of (2), (3) and (5) in (6) gives, after some transposition :

$$e_0^2 - e_1^2 - z^2 i^2 - 2 r p = 2 x \sqrt{i^2 e_1^2 - p^2}, \quad (7)$$

the *Fundamental Equation of the Synchronous Motor*, relating impressed E.M.F., e_0 ; C.E.M.F., e_1 ; current i ; power, p , and resistance, r ; reactance, x ; impedance z .

This equation shows that, at given impressed E.M.F. e_0 , and given impedance $z = \sqrt{r^2 + x^2}$, three variables are left, e_1 , i , p , of which two are independent. Hence, at given e_0 and z , the current i is not determined by the load p only, but also by the excitation, and thus the same current i can represent widely different loads p , according to the excitation; and with the same load, the current i can be varied in a wide range, by varying the field excitation e_1 .

The meaning of equation (7) is made more perspicuous

by some transformations, which separate e_1 and i , as function of p and of an angular parameter ϕ .

Substituting in (7) the new coördinates :

$$\left. \begin{aligned} a &= \frac{e_1^2 + z^2 i^2}{\sqrt{2}} \\ \beta &= \frac{e_1^2 - z^2 i^2}{\sqrt{2}} \end{aligned} \right\} \text{ or, } \left\{ \begin{aligned} e_1^2 &= \frac{a + \beta}{\sqrt{2}} \\ z^2 i^2 &= \frac{a - \beta}{\sqrt{2}} \end{aligned} \right. \quad (8)$$

we get

$$e_0^2 - a\sqrt{2} - 2rp = 2\frac{x}{z}\sqrt{\frac{a^2 - \beta^2}{2} - z^2 p^2}; \quad (9)$$

substituting again,

$$\left. \begin{aligned} e_0^2 &= a \\ 2zp &= b \\ r &= \epsilon z \\ s &= z\sqrt{1 - \epsilon^2} \\ 2rp &= \epsilon b \end{aligned} \right\}$$

hence,

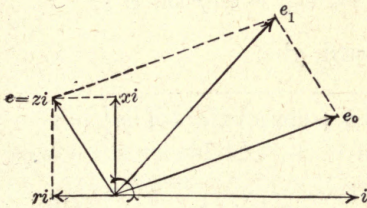


Fig. 136.

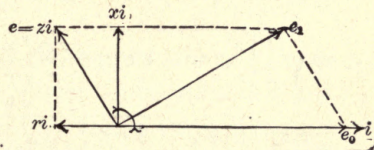


Fig. 137.

we get

$$a - a\sqrt{2} - \epsilon b = \sqrt{(1 - \epsilon^2)(2a^2 - 2\beta^2 - b^2)}, \quad (11)$$

and, squared,

$$\epsilon^2 a^2 + (1 - \epsilon^2)\beta^2 - a\sqrt{2}(a - \epsilon b) + \frac{b^2(1 - \epsilon^2)}{2} + \frac{(a - \epsilon b)^2}{2} = 0, \quad (12)$$

substituting

$$\left. \begin{aligned} \epsilon a - \frac{(a - \epsilon b)\sqrt{2}}{2\epsilon} &= v, \\ \beta\sqrt{1 - \epsilon^2} &= w, \end{aligned} \right\} \quad (13)$$

gives, after some transposition,

$$v^2 + w^2 = \frac{(1 - \epsilon^2)}{2\epsilon^2} a(a - 2\epsilon b), \quad (14)$$

hence, if

$$R = \sqrt{\frac{(1 - \epsilon^2)(a - 2\epsilon b)a}{2\epsilon^2}}, \quad (15)$$

it is

$$v^2 + w^2 = R^2 \quad (16)$$

the equation of a circle with radius R .

Substituting now backwards, we get, with some transpositions :

$$\{r^2(e_1^2 + z^2 i^2) - z^2(e_0^2 - 2rp)\}^2 + \{rx(e_1^2 - z^2 i^2)\}^2 = s^2 z^2 e_0^2 (e_0^2 - 4rp) \quad (17)$$

the *Fundamental Equation of the Synchronous Motor* in a modified form.

The separation of e_1 and i can be effected by the introduction of a parameter ϕ by the equations :

$$\left. \begin{aligned} r^2(e_1^2 - z^2 i^2) - z^2(e_0^2 - 2rp) &= xz e_0 \sqrt{e_0^2 - 4rp} \cos \phi \\ rx(e_1^2 - z^2 i^2) &= xz e_0 \sqrt{e_0^2 - 4rp} \sin \phi \end{aligned} \right\} \quad (18)$$

These equations (18), transposed, give

$$\begin{aligned} e_1 &= \sqrt{\frac{1}{2} \left\{ \frac{z^2}{r^2} (e_0^2 - 2rp) + \frac{z e_0}{r} \left(\frac{x}{r} \cos \phi + \sin \phi \right) \sqrt{e_0^2 - 4rp} \right\}} \\ &= \frac{e_0 z}{r} \sqrt{\frac{1}{2} \left\{ \left(1 - \frac{2rp}{e_0^2} \right) + \left(\frac{x}{z} \cos \phi + \frac{r}{z} \sin \phi \right) \sqrt{1 - \frac{4rp}{e_0^2}} \right\}}. \end{aligned} \quad (19)$$

$$\begin{aligned} i &= \sqrt{\frac{1}{2} \left\{ \frac{1}{r^2} (e_0^2 - 2rp) + \frac{e_0}{rz} \left(\frac{x}{r} \cos \phi - \sin \phi \right) \sqrt{e_0^2 - 4rp} \right\}} \\ &= \frac{e_0}{r} \sqrt{\frac{1}{2} \left\{ \left(1 - \frac{2rp}{e_0^2} \right) + \left(\frac{x}{z} \cos \phi - \frac{r}{z} \sin \phi \right) \sqrt{1 - \frac{4rp}{e_0^2}} \right\}}. \end{aligned} \quad (20)$$

The parameter ϕ has no direct physical meaning, apparently.

These equations (19) and (20), by giving the values of e_1 and i as functions of p and the parameter ϕ enable us to construct the *Power Characteristics of the Synchronous Motor*, as the curves relating e_1 and i , for a given power p , by attributing to ϕ all different values.

Since the variables v and w in the equation of the circle (16) are quadratic functions of e_1 and i , the *Power Characteristics of the Synchronous Motor are Quartic Curves*.

They represent the action of the synchronous motor under all conditions of load and excitation, as an element of power transmission even including the line, etc.

Before discussing further these Power Characteristics, some special conditions may be considered.

185. A. *Maximum Output.*

Since the expression of e_1 and i [equations (19) and (20)] contain the square root, $\sqrt{e_0^2 - 4rp}$, it is obvious that the maximum value of p corresponds to the moment where this square root disappears by passing from real to imaginary; that is,

$$e_0^2 - 4rp = 0,$$

or,

$$p = \frac{e_0^2}{4r}. \quad (21)$$

This is the same value which represents the maximum power transmissible by E.M.F., e_0 , over a non-inductive line of resistance, r ; or, more generally, the maximum power which can be transmitted over a line of impedance,

$$z = \sqrt{r^2 + x^2},$$

into any circuit, shunted by a condenser of suitable capacity.

Substituting (21) in (19) and (20), we get,

$$\left. \begin{aligned} e_1 &= \frac{z}{2r} e_0 \\ i &= \frac{e_0}{2r} \end{aligned} \right\} \quad (22)$$

and the displacement of phase in the synchronous motor.

$$\cos(e_1, i) = \frac{p}{ic_1} = \frac{r}{z};$$

hence,

$$\tan(e_1, i) = -\frac{x}{r}, \quad (23)$$

that is, the angle of internal displacement in the synchronous motor is equal, but opposite to, the angle of displacement of line impedance,

$$\begin{aligned}(e_1, i) &= -(e, i), \\ &= -(z, r),\end{aligned}\tag{24}$$

and consequently,

$$(e_0, i) = 0;\tag{25}$$

that is, the current, i , is in phase with the impressed E.M.F., e_0 .

If $z < 2r$, $e_1 < e_0$; that is, motor E.M.F. < generator E.M.F.

If $z = 2r$, $e_1 = e_0$; that is, motor E.M.F. = generator E.M.F.

If $z > 2r$, $e_1 > e_0$; that is, motor E.M.F. > generator E.M.F.

In either case, the current in the synchronous motor is leading.

186. B. *Running Light*, $p = 0$.

When running light, or for $p = 0$, we get, by substituting in (19) and (20),

$$\left. \begin{aligned}e_1 &= \frac{e_0 z}{r} \sqrt{\frac{1}{2} \left\{ 1 + \frac{x}{z} \cos \phi + \frac{r}{z} \sin \phi \right\}} \\ i &= \frac{e_0}{r} \sqrt{\frac{1}{2} \left\{ 1 + \frac{x}{z} \cos \phi - \frac{r}{z} \sin \phi \right\}}\end{aligned}\right\}\tag{26}$$

Obviously this condition can never be fulfilled absolutely, since p must at least equal the power consumed by friction, etc.; and thus the true no-load curve merely approaches the curve $p = 0$, being, however, rounded off, where curve (26) gives sharp corners.

Substituting $p = 0$ into equation (7) gives, after squaring and transposing,

$$e_1^2 + e_0^2 + z^4 i^4 - 2e_1^2 e_0^2 - 2z^2 i^2 e_0^2 + 2r^2 i^2 e_1^2 - 2x^2 i^2 e_1^2 = 0.\tag{27}$$

This quartic equation can be resolved into the product of two quadratic equations,

$$\left. \begin{aligned}e_1^2 + z^2 i^2 - e_0^2 + 2x i e_1 &= 0 \text{ generator.} \\ e_1^2 + z^2 i^2 - e_0^2 - 2x i e_1 &= 0 \text{ motor.}\end{aligned}\right\}\tag{28}$$

which are the equations of two ellipses, the one the image of the other, both inclined with their axes.

The minimum value of C.E.M.F., e_1 , is $e_1 = 0$ at $i = \frac{e_0}{z}$. (29)

The minimum value of current, i , is $i = 0$ at $e_1 = e_0$. (30)

The maximum value of E.M.F., e_1 , is given by Equation (28),

$$f = e_1^2 + z^2 i^2 - e_0^2 \pm 2 x i e_1 = 0;$$

by the condition,

$$\frac{de_1}{di} = -\frac{df/di}{df/de_1} = 0, \text{ as } z^2 i \pm x e_1 = 0.$$

hence,

$$i = e_0 \frac{x}{r z}, \quad e_1 = \mp e_0 \frac{z}{r} \tag{31}$$

The maximum value of current, i , is given by equation (28) by

$$\frac{di}{de_1} = 0, \text{ as}$$

$$i = \frac{e_0}{r} \quad e_1 = \mp e_0 \frac{x}{r}. \tag{32}$$

If, as abscissæ, e_1 , and as ordinates, $z i$, are chosen, the axis of these ellipses pass through the points of maximum power given by equation (22).

It is obvious thus, that in the curves of synchronous motors running light, published by Mordey and others, the two sides of the V-shaped curves are not straight lines, as usually assumed, but arcs of ellipses, the one of concave, the other of convex, curvature.

These two ellipses are shown in Fig. 138, and divide the whole space into six parts — the two parts A and A' , whose areas contain the quartic curves (19) (20) of synchronous motor, the two parts B and B' , whose areas contain the quartic curves of generator, and the interior space C and exterior space D , whose points do not represent any actual condition of the alternator circuit, but make e_1, i imaginary.

A and A' and the same B and B' , are identical conditions of the alternator circuit, differing merely by a simul-

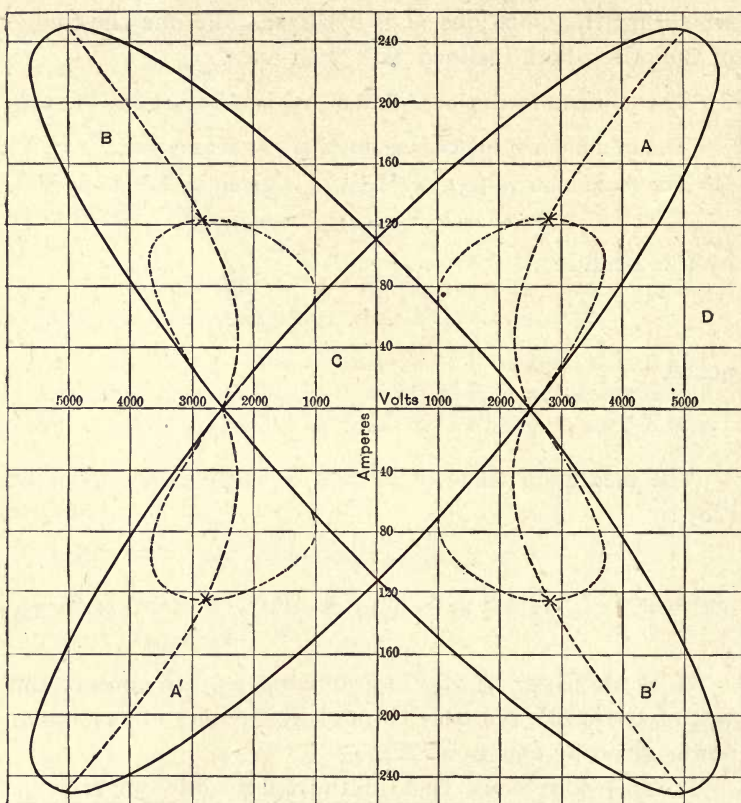


Fig. 138.

taneous reversal of current and E.M.F.; that is, differing by the time of a half period.

Each of the spaces *A* and *B* contains one point of equation (22), representing the condition of maximum output of generator, viz., synchronous motor.

187. C. Minimum Current at Given Power.

The condition of minimum current, i , at given power, p , is determined by the absence of a phase displacement at the impressed E.M.F. e_0 ,

$$(e_0, i) = 0.$$

This gives from diagram Fig. 132,

$$e_1^2 = e_0^2 + i^2 z^2 - 2 i e_0 \frac{r}{z}, \quad (33)$$

or, transposed,

$$e_1 = \sqrt{(e_0 - ir)^2 + i^2 z^2}. \quad (34)$$

This quadratic curve passes through the point of zero current and zero power,

$$i = 0, \quad e_1 = e_0,$$

through the point of maximum power (22),

$$i = \frac{e_0}{2r}, \quad e_1 = \frac{e_0 z}{2r},$$

and through the point of maximum current and zero power,

$$i = \frac{e_0}{r}, \quad e_1 = \frac{e_0 x}{r}, \quad (35)$$

and divides each of the quartic curves or power characteristics into two sections, one with leading, the other with lagging, current, which sections are separated by the two points of equation 34, the one corresponding to minimum, the other to maximum, current.

It is interesting to note that at the latter point the current can be many times larger than the current which would pass through the motor while at rest, which latter current is,

$$i = \frac{e_0}{z}, \quad (36)$$

while at no-load, the current can reach the maximum value,

$$i = \frac{e_0}{r}, \quad (35)$$

the same value as would exist in a non-inductive circuit of the same resistance.

The minimum value at C.E.M.F. e_1 , at which coincidence

of phase $(e_0, i) = 0$, can still be reached, is determined from equation (34) by,

$$\frac{de_1}{di} = 0;$$

as

$$i = e_0 \frac{r}{z^2} \quad e_1 = e_0 \frac{x}{z}. \quad (37)$$

The curve of no-displacement, or of minimum current, is shown in Figs. 138 and 139 in dotted lines.*

188. D. Maximum Displacement of Phase.

$$(e_0, i) = \text{maximum.}$$

At a given power p the input is,

$$p_0 = p + i^2 r = e_0 i \cos(e_0, i); \quad (38)$$

hence,

$$\cos(e_0, i) = \frac{p + i^2 r}{e_0 i}. \quad (39)$$

At a given power p , this value, as function of the current i , is a maximum when

$$\frac{d}{di} \left(\frac{p + i^2 r}{e_0 i} \right) = 0,$$

this gives,

$$p = i^2 r; \quad (40)$$

or,

$$i = \sqrt{\frac{p}{r}}. \quad (41)$$

That is, the displacement of phase, lead or lag, is a maximum, when the power of the motor equals the power

* It is interesting to note that the equation (34) is similar to the value, $e_1 = \sqrt{(e_0 - ir)^2 - i^2 x^2}$, which represents the output transmitted over an inductive line of impedance, $z = \sqrt{r^2 + x^2}$ into a non-inductive circuit.

Equation (34) is identical with the equation giving the maximum voltage, e_1 , at current, i , which can be produced by shunting the receiving circuit with a condenser; that is, the condition of "complete resonance" of the line, $z = \sqrt{r^2 + x^2}$, with current, i . Hence, referring to equation (35), $e_1 = e_0 \frac{x}{r}$ is the maximum resonance voltage of the line, reached when closed by a condenser of reactance, $-x$.

consumed by the resistance; that is, at the electrical efficiency of 50 per cent.

Substituting (40) in equation (7) gives, after squaring

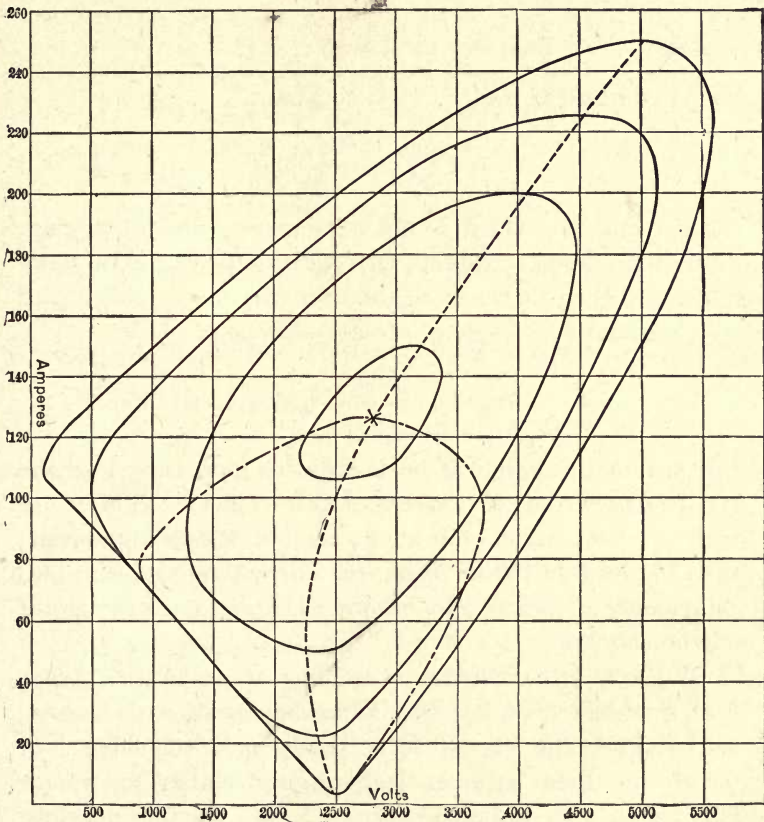


Fig. 139.

and transposing, the Quartic Equation of Maximum Displacement,

$$(e_0^2 - e_1^2)^2 + i^4 z^2 (z^2 + 8 r^2) + 2 i^2 e_1^2 (5 r^2 - z^2) - 2 i^2 e_0^2 (z^2 + 3 r^2) = 0. \tag{42}$$

The curve of maximum displacement is shown in dash-dotted lines in Figs. 138 and 139. It passes through the

point of zero current — as singular or nodal point — and through the point of maximum power, where the maximum displacement is zero, and it intersects the curve of zero displacement.

189. E. *Constant Counter E.M.F.*

At constant C.E.M.F., $e_1 = \text{constant}$,

$$\text{If } e_1 < e_0 \sqrt{1 - \frac{r^2 x^2}{z^4}},$$

the current at no-load is not a minimum, and is lagging. With increasing load, the lag decreases, reaches a minimum, and then increases again, until the motor falls out of step, without ever coming into coincidence of phase.

$$\text{If } e_0 \sqrt{1 - \frac{r^2 x^2}{z^4}} < e_1 < e_0,$$

the current is lagging at no load; with increasing load the lag decreases, the current comes into coincidence of phase with e_0 , then becomes leading, reaches a maximum lead; then the lead decreases again, the current comes again into coincidence of phase, and becomes lagging, until the motor falls out of step.

If $e_0 < e_1$, the current is leading at no load, and the lead first increases, reaches a maximum, then decreases; and whether the current ever comes into coincidence of phase, and then becomes lagging, or whether the motor falls out of step while the current is still leading, depends, whether the C.E.M.F. at the point of maximum output is $> e_0$ or $< e_0$.

190. F. *Numerical Instance.*

Figs. 138 and 139 show the characteristics of a 100-kilowatt motor, supplied from a 2500-volt generator over a distance of 5 miles, the line consisting of two wires, No. 2 B. & S.G., 18 inches apart.

In this case we have,

$$\left. \begin{aligned} e_0 &= 2500 \text{ volts constant at generator terminals;} \\ r &= 10 \text{ ohms, including line and motor;} \\ x &= 20 \text{ ohms, including line and motor;} \end{aligned} \right\} \quad (43)$$

hence $z = 22.36$ ohms.

Substituting these values, we get,

$$2500^2 - e_1^2 - 500 i^2 - 20 p = 40 \sqrt{i^2 e_1^2 - p^2} \quad (7)$$

$$\{e_1^2 + 500 i^2 - 31.25 \times 10^6 + 100 p\}^2 + \{2 e_1^2 - 1000 i^2\}^2 = 7.8125 \times 10^{15} - 5 + 10^9 p. \quad (17)$$

$$e_1 = 5590 \quad (19)$$

$$\sqrt{\frac{1}{2} \{(1 - 3.2 \times 10^{-6} p) + (.894 \cos \phi + .447 \sin \phi) \sqrt{1 - 6.4 \times 10^{-6} p}\}}. \\ i = 559 \quad (20)$$

$$\sqrt{\frac{1}{2} \{(1 - 3.2 \times 10^{-6} p) + (.894 \cos \phi - .447 \sin \phi) \sqrt{1 - 6.4 \times 10^{-6} p}\}}.$$

Maximum output,

$$p = 156.25 \text{ kilowatts} \quad (21)$$

at $\left. \begin{aligned} e_1 &= 2,795 \text{ volts} \\ i &= 125 \text{ amperes} \end{aligned} \right\} \quad (22)$

Running light,

$$\left. \begin{aligned} e_1^2 + 500 i^2 - 6.25 \times 10^4 \mp 40 i e_1 &= 0 \\ e_1 &= 20 i \pm \sqrt{6.25 \times 10^4 - 100 i^2} \end{aligned} \right\} \quad (28)$$

At the minimum value of C.E.M.F. $e_1 = 0$ is $i = 112$ (29)

At the minimum value of current, $i = 0$ is $e_1 = 2500$ (30)

At the maximum value of C.E.M.F. $e_1 = 5590$ is $i = 223.5$ (31)

At the maximum value of current $i = 250$ is $e_1 = 5000$ (32)

Curve of zero displacement of phase,

$$\begin{aligned} e_1 &= 10 \sqrt{(250 - i)^2 + 4 i^2} \\ &= 10 \sqrt{6.25 \times 10^4 - 500 i + 5 i^2} \end{aligned} \quad (34)$$

Minimum C.E.M.F. point of this curve,

$$i = 50 \quad e_1 = 2240 \quad (35)$$

Curve of maximum displacement of phase,

$$\begin{aligned} p &= 10 i^2 \\ (6.25 \times 10^6 - e_1^2)^2 + .65 \times 10^6 i^4 - 10^{10} i^2 &= 0. \end{aligned} \quad (40)$$

$$(42)$$

Fig. 138 gives the two ellipses of zero power, in drawn lines, with the curves of zero displacement in dotted, the curves of maximum displacement in dash-dotted lines, and the points of maximum power as crosses.

Fig. 139 gives the motor-power characteristics, for,

$p = 10$	kilowatts.
$p = 50$	kilowatts.
$p = 100$	kilowatts.
$p = 150$	kilowatts.
$p = 156.25$	kilowatts.

together with the curves of zero displacement, and of maximum displacement.

191. G. Discussion of Results.

The characteristic curves of the synchronous motor, as shown in Fig. 139, have been observed frequently, with their essential features, the V-shaped curve of no load, with the point rounded off and the two legs slightly curved, the one concave, the other convex; the increased rounding off and contraction of the curves with increasing load; and the gradual shifting of the point of minimum current with increasing load, first towards lower, then towards higher, values of C.E.M.F. e_1 .

The upper parts of the curves, however, I have never been able to observe experimentally, and consider it as probable that they correspond to a condition of synchronous motor-running, which is unstable. The experimental observations usually extend about over that part of the curves of Fig. 139 which is reproduced in Fig. 140, and in trying to extend the curves further to either side, the motor is thrown out of synchronism.

It must be understood, however, that these power characteristics of the synchronous motor in Fig. 139 can be considered as approximations only, since a number of assump-

tions are made which are not, or only partly, fulfilled in practice. The foremost of these are:

1. It is assumed that e_1 can be varied unrestrictedly, while in reality the possible increase of e_1 is limited by magnetic saturation. Thus in Fig. 139, at an impressed E.M.F., $e_0 = 2,500$ volts, e_1 rises up to 5,590 volts, which may or may not be beyond that which can be produced by the motor, but certainly is beyond that which can be constantly given by the motor.

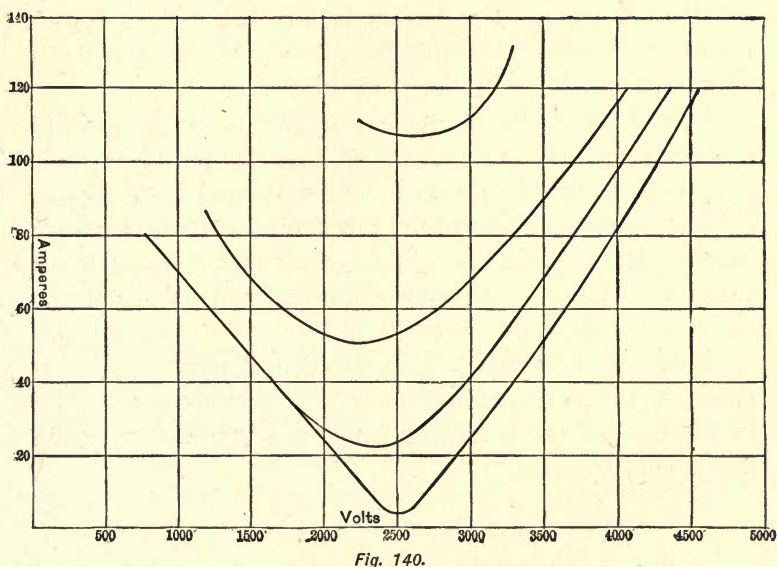


Fig. 140.

2. The reactance, x , is assumed as constant. While the reactance of the line is practically constant, that of the motor is not, but varies more or less with the saturation, decreasing for higher values. This decrease of x increases the current i , corresponding to higher values of e_1 , and thereby bends the curves upwards at a lower value of e_1 than represented in Fig. 139.

It must be understood that the motor reactance is not a simple quantity, but represents the combined effect of

self-induction, that is, the E.M.F. induced in the armature conductor by the current flowing therein and armature reaction, or the variation of the C.E.M.F. of the motor by the change of the resultant field, due to the superposition of the M.M.F. of the armature current upon the field excitation; that is, it is the "synchronous reactance."

3. These curves in Fig. 139 represent the conditions of constant electric power of the motor, thus including the mechanical and the magnetic friction (core loss). While the mechanical friction can be considered as approximately constant, the magnetic friction is not, but increases with the magnetic induction; that is, with e_1 , and the same holds for the power consumed for field excitation.

Hence the useful mechanical output of the motor will on the same curve, $p = \text{const.}$, be larger at points of lower C.E.M.F., e_1 , than at points of higher e_1 ; and if the curves are plotted for constant useful mechanical output, the whole system of curves will be shifted somewhat towards lower values of e_1 ; hence the points of maximum output of the motor correspond to a lower E.M.F. also.

It is obvious that the true mechanical power-characteristics of the synchronous motor can be determined only in the case of the particular conditions of the installation under consideration.

CHAPTER XIX.

COMMUTATOR MOTORS.

192. Commutator motors—that is, motors in which the current enters or leaves the armature over brushes through a segmental commutator—have been built of various types, but have not found any extensive application, in consequence of the superiority of the induction and synchronous motors, due to the absence of commutators.

The main subdivisions of commutator motors are the repulsion motor, the series motor, and the shunt motor.

REPULSION MOTOR.

193. The repulsion motor is an induction motor or transformer motor; that is, a motor in which the main current enters the primary member or field only, while in the secondary member, or armature, a current is induced, and thus the action is due to the repulsive thrust between induced current and inducing magnetism.

As stated under the heading of induction motors, a multiple circuit armature is required for the purpose of having always secondary circuits in inductive relation to the primary circuit during the rotation. If with a single-coil field, these secondary circuits are constantly closed upon themselves as in the induction motor, the primary circuit will not exert a rotary effect upon the armature while at rest, since in half of the armature coils the current is induced so as to give a rotary effort in the one direction, and in the other half the current is induced to

give a rotary effort in the opposite direction, as shown by the arrows in Fig. 141.

In the induction motor a second magnetic field is used to act upon the currents induced by the first, or inducing magnetic field, and thereby cause a rotation. That means the motor consists of a primary electric circuit, inducing

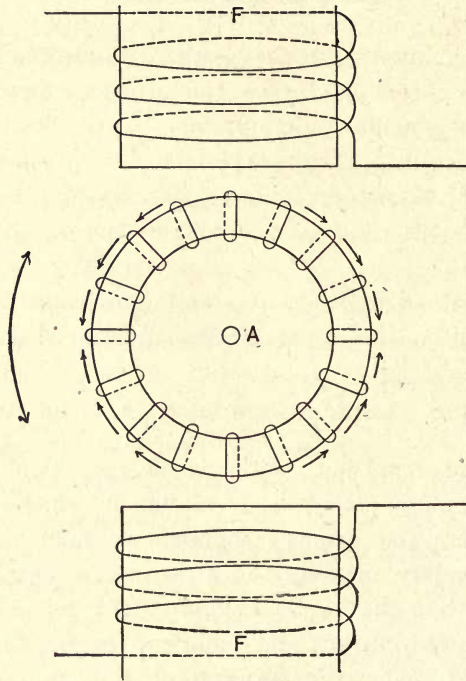


Fig. 141.

in the armature the secondary currents, and a primary magnetizing circuit producing the magnetism to act upon the secondary currents.

In the polyphase induction motor both functions of the primary circuit are usually combined in the same coils; that is, each primary coil induces secondary currents, and produces magnetic flux acting upon secondary currents induced by another primary coil.

194. In the repulsion motor the difficulty due to the equal and opposite rotary efforts, caused by the induced armature currents when acted upon by the inducing magnetic field, is overcome by having the armature coils closed upon themselves, either on short circuit or through resistance, only in that position where the induced currents give

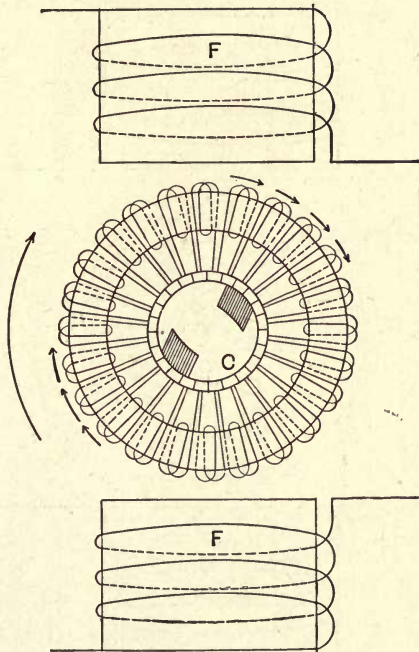


Fig. 142.

a rotary effort in the desired direction, while the armature coils are open-circuited in the position where the rotary effort of the induced currents would be in opposition to the desired rotation. This requires means to open or close the circuit of the armature coils and thereby introduces the commutator.

Thus the general construction of a repulsion motor is as shown in Figs. 142 and 143 diagrammatically as bipolar

motor. The field is a single-phase alternating field F , the armature shown diagrammatically as ring wound A consists of a number of coils connected to a segmental commutator C , in general in the same way as in continuous-current machines. Brushes standing under an angle of about 45° with the direction of the magnetic field, short-circuit either a

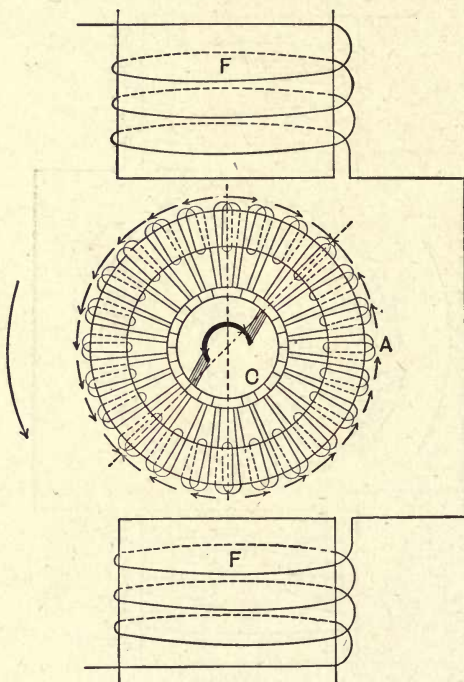


Fig. 143.

part of the armature coils as shown in Fig. 142, or the whole armature by a connection from brush to brush as shown in Fig. 143.

The former arrangement has the disadvantage of using a part of the armature coils only. The second arrangement has the disadvantage that, in the passage of the brush from segment to segment, individual armature coils are short-

circuited, and thereby give a torque in opposite direction to the torque developed by the main induced current flowing through the whole armature from brush to brush.

195. Thus the repulsion motor consists of a primary electric circuit, a magnetic circuit interlinked therewith, and a secondary circuit closed upon itself and displaced in

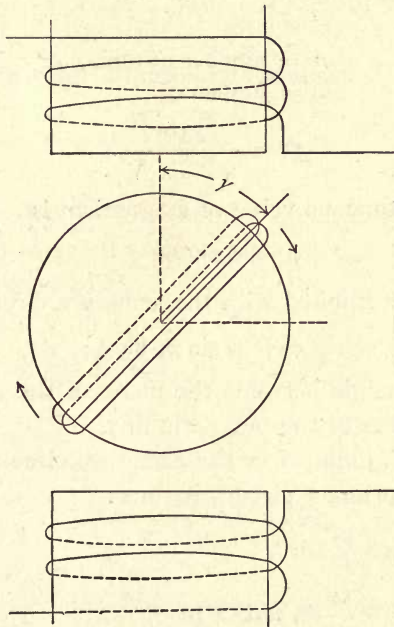


Fig. 144.

space by 45° — in a bipolar motor — from the direction of the magnetic flux, as shown diagrammatically in Fig. 144.

This secondary circuit, while set in motion, still remains in the same position of 45° displacement, with the magnetic flux, or rather, what is theoretically the same, when moving out of this position, is replaced by other secondary circuits entering this position of 45° displacement.

For simplicity, in the following all the secondary quan-

tities, as E.M.F., current, resistance, reactance, etc., are assumed as reduced to the primary circuit by the ratio of turns, in the same way as done in the chapter on Induction Motors.

196. Let

Φ = maximum magnetic flux per field pole;

e = effective E.M.F. induced thereby in the field turns; thus :

$$e = \sqrt{2} \pi N n \Phi 10^{-8};$$

where

n = number of turns,

N = frequency.

thus :

$$\Phi = \frac{e 10^8}{\sqrt{2} \pi n N}.$$

The instantaneous value of magnetism is

$$\phi = \Phi \sin \beta;$$

and the flux interlinked with the armature circuit

$$\phi_1 = \Phi \sin \beta, \sin \lambda;$$

when λ is the angle between the plane of the armature coil and the direction of the magnetic flux.

The E.M.F. induced in the armature circuit, of n turns, as reduced to primary circuit, is thus :

$$\begin{aligned} e_1 &= -n \frac{d\phi_1}{dt} 10^{-8}, \\ &= -n \Phi \frac{d}{dt} \sin \beta \sin \lambda 10^{-8}, \\ &= -n \Phi \left\{ \sin \lambda \cos \beta \frac{d\beta}{dt} + \sin \beta \cos \lambda \frac{d\lambda}{dt} \right\} 10^{-8}. \end{aligned}$$

If N = frequency in cycles per second, N_1 = speed in cycles per second (equal revolutions per second times number of pairs of poles), it is :

$$\frac{d\beta}{dt} = 2\pi N;$$

$$\frac{d\lambda}{dt} = 2\pi N_1;$$

and since $\lambda = 45^\circ$, or $\sin \lambda = \cos \lambda = 1/\sqrt{2}$, it is, substituted :

$$e_1 = -\sqrt{2} \pi n \Phi \{ N \cos \beta + N_1 \sin \beta \} 10^{-8}$$

or, since

$$\Phi = \frac{e 10^8}{\sqrt{2} \pi n N};$$

$$e_1 = -e \{ \cos \beta + k \sin \beta \};$$

where

$$k = \frac{N_1}{N} = \text{ratio } \frac{\text{speed}}{\text{frequency}};$$

or the effective value of secondary induced E.M.F.,

$$e_1 = e \sqrt{\frac{1+k^2}{2}}.$$

197. Introducing now complex quantities, and counting the time from the zero value of rising magnetism, the magnetism is represented by

$$j\Phi;$$

the primary induced E.M.F.,

$$E = -e;$$

the secondary induced E.M.F. :

$$E_1 = -\frac{e}{\sqrt{2}}(1+jk);$$

hence, if

$Z_1 = r_1 - jx_1 =$ secondary impedance reduced to primary circuit,

$Z = r - jx =$ primary impedance,

$Y = g + jb =$ primary admittance,

it is,

secondary current,

$$I_1 = \frac{E_1}{Z_1} = -\frac{e}{\sqrt{2}} \frac{1+jk}{r_1 - jx_1};$$

primary exciting current,

$$I_0 = eY = e(g + jb);$$

hence, total primary current,

$$I = I_0 - I_1;$$

or

$$I = e \left\{ g + jb + \frac{1}{\sqrt{2}} \frac{1 + jk}{r_1 - jx_1} \right\}.$$

Primary impressed E.M.F.,

$$E_0 = -E + IZ;$$

or

$$E_0 = e \left\{ 1 + \frac{1 + jk}{\sqrt{2}} \frac{r - jx}{r_1 - jx_1} + (g + jb)(r - jx) \right\}$$

Neglecting in E_0 the last term, as of higher order,

$$E_0 = e \left\{ 1 + \frac{1 + jk}{\sqrt{2}} \frac{r - jx}{r_1 - jx_1} \right\};$$

or, eliminating imaginary quantities,

$$e_0 = e \frac{\sqrt{(r + r_1\sqrt{2} + kx)^2 + (x + x_1\sqrt{2} - kr)^2}}{\sqrt{2}(r_1^2 + x_1^2)}.$$

198. The power consumed by the primary counter E.M.F., e , that is, transferred into the secondary circuit, is

$$\begin{aligned} P' &= |e I_1| \\ &= \frac{e^2}{\sqrt{2}} \frac{1 + jk}{r_1 - jx_1}; \end{aligned}$$

or, eliminating the imaginary quantities,

$$P' = \frac{e^2}{\sqrt{2}} \frac{r_1 + kx_1}{r_1^2 + x_1^2}.$$

The power consumed by the secondary resistance is

$$\begin{aligned} P_1 &= I_1^2 r_1 \\ &= \frac{e^2}{2} \frac{(1 + k^2) r_1}{r_1^2 + x_1^2}; \end{aligned}$$

Hence, the difference, or the mechanical power at the motor shaft —

$$\begin{aligned} P &= P' - P_1 \\ &= \frac{e^2}{2(r_1^2 + x_1^2)} \{r_1(\sqrt{2} - 1) + kx_1\sqrt{2} - k^2 r_1\}, \end{aligned}$$

and, substituting for e ,

$$P = \frac{e_0^2 \{r_1 (\sqrt{2} - 1) + k x_1 \sqrt{2} - k^2 r_1\}}{(r + r_1 \sqrt{2} + kx)^2 + (x + x_1 \sqrt{2} - kr)^2}.$$

If r and r_1 are small compared with x and x_1 , this is approximately,

$$P = \frac{e_0^2 k x_1 \sqrt{2}}{(x + x_1 \sqrt{2})^2 + k^2 x^2}.$$

Thus the power is a maximum for $dP/dk = 0$, that is,

$$k = \frac{x + x_1 \sqrt{2}}{x}.$$

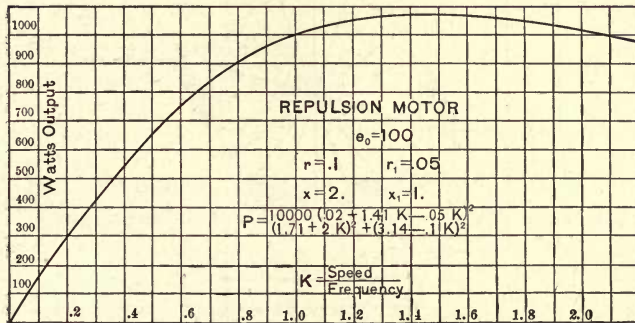


Fig. 145. Repulsion Motor.

As an instance is shown, in Fig. 145, the power output as ordinates, with the speed $k = N_1/N$ as abscissæ, of a repulsion motor of the constants,

$$\begin{aligned} e_0 &= 100. \\ r &= .1 \quad r_1 = .05 \\ x &= 2.0 \quad x_1 = 1.0 \end{aligned}$$

giving the power,

$$P = \frac{10,000 \{0.02 + 1.41 k - 0.05 k^2\}}{(.171 + 2 k)^2 + (3.14 - .1 k)^2}.$$

SERIES MOTOR. SHUNT MOTOR.

199. If, in a continuous-current motor, series motor as well as shunt motor, the current is reversed, the direction of rotation remains the same, since field magnetism and armature current have reversed their sign, and their prod-

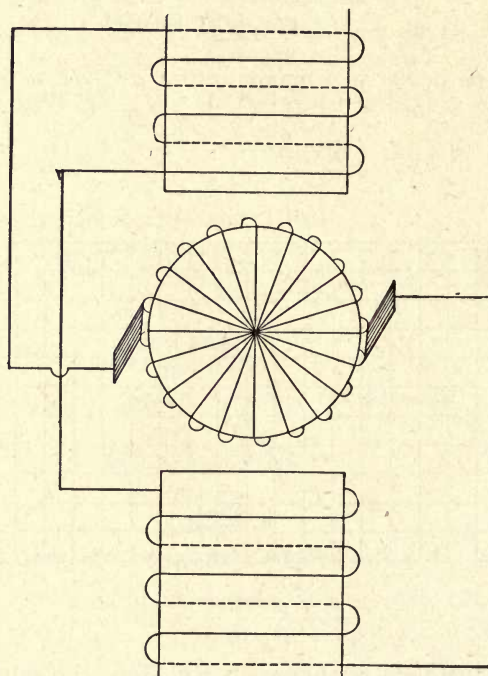


Fig. 146. Series Motor.

uct, the torque, thus maintained the same sign. Therefore such a motor, when supplied by an alternating current, will operate also, provided that the reversals in field and in armature take place simultaneously. In the series motor this is necessarily the case, the same current passing through field and through armature.

With an alternating current in the field, obviously the

magnetic circuit has to be laminated to exclude eddy currents.

Let, in a *series motor*, Fig. 146,

Φ = effective magnetism per pole,

n = number of field turns per pole in series,

n_1 = number of armature turns in series between brushes,

p = number of poles,

\mathcal{R} = magnetic reluctance of field circuit,

\mathcal{R}_1 = magnetic reluctance of armature circuit,

Φ_1 = effective magnetic flux produced by armature current
(cross magnetization),

r = resistance of field (effective resistance, including hysteresis),

r_1 = resistance of armature (effective resistance, including hysteresis),

N = frequency of alternations,

N_1 = speed in cycles per second.

It is then,

E.M.F. induced in armature conductors by their rotation through the magnetic field (counter E.M.F. of motor).

$$E = 4 n_1 N_1 \Phi 10^{-8}$$

E.M.F. of self-induction of field,

$$E' = 2 \pi p n N \Phi 10^{-8},$$

E.M.F. of self-induction of armature,

$$E_1' = 2 \pi n_1 N \Phi_1 10^{-8},$$

E.M.F. consumed by resistance,

$$E_r = (r + r_1) I,$$

where

I = current passing through motor, in amperes effective.

Further, it is :

Field magnetism :

$$\Phi = \frac{n I 10^8}{P}$$

Armature magnetism :

$$\Phi_1 = \frac{n_1 I 10^8}{P_1},$$

Substituting these values,

$$E = \frac{4 n n_1 N_1 I}{P};$$

$$E' = \frac{2 \pi p n^2 N I}{P};$$

$$E_1' = \frac{2 \pi n_1^2 N I}{P_1};$$

$$E_r = (r + r_1) I.$$

Thus the impressed E.M.F.,

$$\begin{aligned} E_0 &= \sqrt{(E + E_r)^2 + (E' + E_1')^2} \\ &= I \sqrt{\left(\frac{4 n n_1 N_1}{P} + r + r_1\right)^2 + 4 \pi^2 N^2 \left(\frac{p n^2}{P} + \frac{n_1^2}{P_1}\right)^2}; \end{aligned}$$

or, since

$$x = 2 \pi N \frac{p n^2}{P} = \text{reactance of field};$$

$$x_1 = 2 \pi N \frac{n_1^2}{P_1} = \text{reactance of armature};$$

$$\begin{aligned} E_0 &= I \sqrt{\left(\frac{4 n n_1 N_1}{P} + r + r_1\right)^2 + (x + x_1)^2} \\ &= I \sqrt{\left(\frac{2}{\pi} \frac{n_1}{p n} \frac{N_1}{N} x + r + r_1\right)^2 + (x + x_1)^2}; \end{aligned}$$

and

$$\begin{aligned} I &= \frac{E_0}{\sqrt{\left(\frac{4 n n_1 N_1}{P} + r + r_1\right)^2 + 4 \pi^2 N^2 \left(\frac{p n^2}{P} + \frac{n_1^2}{P_1}\right)^2}} \\ &= \frac{E_0}{\sqrt{\left(\frac{4 n n_1 N_1}{P} + r + r_1\right)^2 + (x + x_1)^2}} \\ &= \frac{E_0}{\sqrt{\left(\frac{2}{\pi} \frac{n_1}{p n} \frac{N_1}{N} x + r + r_1\right)^2 + (x + x_1)^2}}. \end{aligned}$$

200. The power output at armature shaft is,

$$P = EI$$

$$\begin{aligned} &= \frac{\frac{4nn_1N_1}{P}E_0^2}{\left(\frac{4nn_1N_1}{P} + r + r_1\right)^2 + 4\pi^2N^2\left(\frac{pn^2}{P} + \frac{n_1^2}{P_1}\right)^2} \\ &= \frac{\frac{4nn_1N_1}{P}E_0^2}{\left(\frac{4nn_1N_1}{P} + r + r_1\right)^2 + (x + x_1)^2} \\ &= \frac{\frac{2}{\pi}\frac{n_1}{pn}\frac{N_1}{N}xE_0^2}{\left(\frac{2}{\pi}\frac{n_1}{pn}\frac{N_1}{N}x + r + r_1\right)^2 + (x + x_1)^2}. \end{aligned}$$

The displacement of phase between current and E.M.F.

is

$$\begin{aligned} \tan \hat{\omega} &= \frac{E' + E_1'}{E + E_r} \\ &= \frac{2\pi N\left(\frac{pn^2}{P} + \frac{n_1^2}{P_1}\right)}{\frac{4nn_1N_1}{P} + r + r_1} \\ &= \frac{x + x_1}{\frac{2}{\pi}\frac{n_1}{pn}\frac{N_1}{N}x + r + r_1}. \end{aligned}$$

Neglecting, as approximation, the resistances $r + r_1$, it is,

$$\begin{aligned} \tan \hat{\omega} &= \frac{1 + \frac{x_1}{x}}{\frac{2}{\pi}\frac{n_1}{pn}\frac{N_1}{N}} \\ P &= \frac{E_0^2}{\frac{2}{\pi}\frac{n_1}{pn}\frac{N_1}{N} + \frac{\left(1 + \frac{x_1}{x}\right)^2}{\frac{2}{\pi}\frac{n_1}{pn}\frac{N_1}{N}}} \end{aligned}$$

hence a maximum for,

$$\frac{\frac{2}{\pi} \frac{n_1}{p n} \frac{N_1}{N}}{\frac{2}{\pi} \frac{n_1}{p n} \frac{N_1}{N}} = \frac{\left(1 + \frac{x_1}{x}\right)^2}{\frac{2}{\pi} \frac{n_1}{p n} \frac{N_1}{N}},$$

or,

$$\frac{N_1}{N} = \frac{1 + \frac{x_1}{x}}{\frac{2}{\pi} \frac{n_1}{p n}},$$

substituting this in $\tan \hat{\omega}$, it is :

$$\tan \hat{\omega} = 1, \quad \text{or,} \quad \hat{\omega} = 45^\circ.$$

201. Instance of such an alternating-current† motor,

$$E_0 = 100 \quad N = 60 \quad p = 2.$$

$$r = .03 \quad r_1 = .12$$

$$x = .9 \quad x_1 = .5$$

$$n = 10 \quad n_1 = 48$$

Special provisions were made to keep the armature reactance a minimum, and overcome the distortion of the field by the armature M.M.F., by means of a coil closely surrounding the armature and excited by a current of equal phase but opposite direction with the armature current (Eickemeyer). Thereby it was possible to operate a two-circuit, 96-turn armature in a bipolar field of 20 turns, at a ratio of

$$\frac{\text{armature ampere-turns}}{\text{field ampere-turns}} = 2.4.$$

It is in this case,

$$I = \frac{100}{\sqrt{(.023 N_1 + .15)^2 + 1.96}}$$

$$P = \frac{230 N_1}{(.023 N_1 + .15)^2 + 1.96}$$

$$\tan \hat{\omega} = \frac{1.4}{.023 N_1 + .15}, \quad \text{or,} \quad \cos \hat{\omega} = \frac{.023 N_1 + .15}{\sqrt{(.023 N_1 + .15)^2 + 1.96}}$$

In Fig. 147 are given, with the speed N_1 as abscissæ, the values of current I , power P , and power factor $\cos \hat{\omega}$ of this motor.

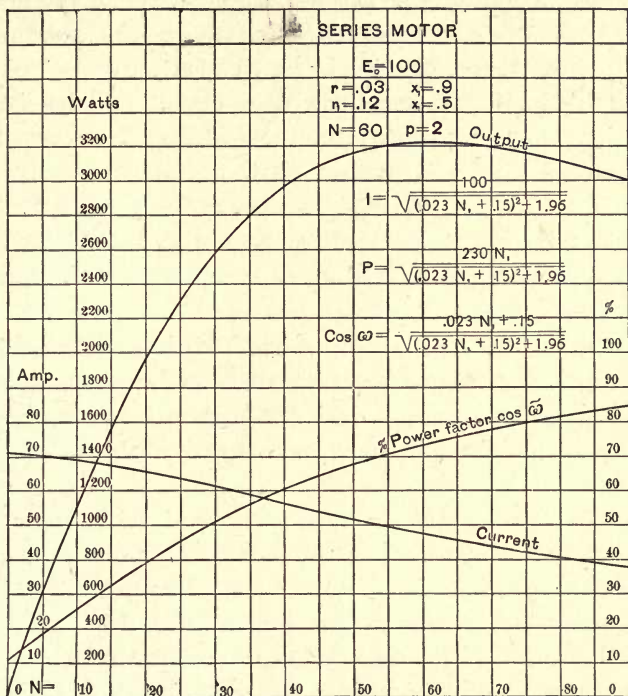


Fig. 147. Series Motor.

202. The *shunt motor* with laminated field will not operate satisfactorily in an alternating-current circuit. It will start with good torque, since in starting the current in armature, as well as in field, are greatly lagging, and thus approximately in phase with each other. With increasing speed, however, the counter E.M.F. of the armature should be in phase with the impressed E.M.F., and thereby the armature current lag less, to represent power. Since however, the field current, and thus the field magnetism, lag nearly 90° , the induced E.M.F. of the armature will lag nearly 90° , and thus not represent power.

Hence, to make a shunt motor work on alternating-current circuits, the magnetism of the field should be approximately in phase with the impressed E.M.F., that is, the field reactance negligible. Since the self-induction of the field is far in excess to its resistance, this requires the insertion of negative reactance, or capacity, in the field.

If the self-induction of the field circuit is balanced by capacity, the motor will operate, provided that the armature reactance is low, and that in starting sufficient resistance is inserted in the armature circuit to keep the armature current approximately in phase with the E.M.F. Under these conditions the equations of the motor will be similar to those of the series motor.

However, such motors have not been introduced, due to the difficulty of maintaining the balance between capacity and self-induction in the field circuit, which depends upon the square of the frequency, and thus is disturbed by the least change of frequency.

The main objection to both series and shunt motors is the destructive sparking at the commutator due to the induction of secondary currents in those armature coils which pass under the brushes. As seen in Fig. 146, with the normal position of brushes midway between the field poles, the armature coil which passes under the brush incloses the total magnetic flux. Thus, in this moment no E.M.F. is induced in the armature coil due to its rotation, but the E.M.F. induced by the alternation of the magnetic flux has a maximum at this moment, and the coil, when short-circuited by the brush, acts as a short-circuited secondary to the field coils as primary; that is, an excessive current flows through this armature coil, which either destroys it, or at least causes vicious sparking when interrupted by the motion of the armature.

To overcome this difficulty various arrangements have been proposed, but have not found an application.

203. Compared with the synchronous motor which has practically no lagging currents, and the induction motor which reaches very high power factors, the power factor of the series motor is low, as seen from Fig. 147, which represents about the best possible design of such motors.

In the alternating-series motor, as well as in the shunt motor, no position of an armature coil exists wherein the coil is dead; but in every position E.M.F. is induced in the armature coil: in the position parallel with the field flux an E.M.F. in phase with the current, in the position at right angles with the field flux an E.M.F. in quadrature with the current, intermediate E.M.Fs. in intermediate positions. At the speed $\pi N/2$ the two induced E.M.Fs. in phase and in quadrature with the current are equal, and the armature coils are the seat of a complete system of symmetrical and balanced polyphase E.M.Fs. Thus, by means of stationary brushes, from such a commutator polyphase currents could be derived.

CHAPTER XX.

REACTION MACHINES.

204. In the chapters on Alternating-Current Generators and on Induction Motors, the assumption has been made that the reactance x of the machine is a constant. While this is more or less approximately the case in many alternators, in others, especially in machines of large armature reaction, the reactance x is variable, and is different in the different positions of the armature coils in the magnetic circuit. This variation of the reactance causes phenomena which do not find their explanation by the theoretical calculations made under the assumption of constant reactance.

It is known that synchronous motors of large and variable reactance keep in synchronism, and are able to do a considerable amount of work, and even carry under circumstances full load, if the field-exciting circuit is broken, and thereby the counter E.M.F. E_1 reduced to zero, and sometimes even if the field circuit is reversed and the counter E.M.F. E_1 made negative.

Inversely, under certain conditions of load, the current and the E.M.F. of a generator do not disappear if the generator field is broken, or even reversed to a small negative value, in which latter case the current flows against the E.M.F. E_0 of the generator.

Furthermore, a shuttle armature without any winding will in an alternating magnetic field revolve when once brought up to synchronism, and do considerable work as a motor.

These phenomena are not due to remanant magnetism nor to the magnetizing effect of Foucault currents, because

they exist also in machines with laminated fields, and exist if the alternator is brought up to synchronism by external means and the remanant magnetism of the field poles destroyed beforehand by application of an alternating current.

205. These phenomena cannot be explained under the assumption of a constant synchronous reactance; because in this case, at no-field excitation, the E.M.F. or counter E.M.F. of the machine is zero, and the only E.M.F. existing in the alternator is the E.M.F. of self-induction; that is, the E.M.F. induced by the alternating current upon itself. If, however, the synchronous reactance is constant, the counter E.M.F. of self-induction is in quadrature with the current and wattless; that is, can neither produce nor consume energy.

In the synchronous motor running without field excitation, always a large lag of the current behind the impressed E.M.F. exists; and an alternating generator will yield an E.M.F. without field excitation, only when closed by an external circuit of large negative reactance; that is, a circuit in which the current leads the E.M.F., as a condenser, or an over-excited synchronous motor, etc.

Self-excitation of the alternator by armature reaction can be explained by the fact that the counter E.M.F. of self-induction is not wattless or in quadrature with the current, but contains an energy component; that is, that the reactance is of the form $X = h - jx$, where x is the wattless component of reactance and h the energy component of reactance, and h is positive if the reactance consumes power, — in which case the counter E.M.F. of self-induction lags more than 90° behind the current, — while h is negative if the reactance produces power, — in which case the counter E.M.F. of self-induction lags less than 90° behind the current.

206. A case of this nature has been discussed already in the chapter on Hysteresis, from a different point of view.

There the effect of magnetic hysteresis was found to distort the current wave in such a way that the equivalent sine wave, that is, the sine wave of equal effective strength and equal power with the distorted wave, is in advance of the wave of magnetism by what is called the angle of hysteretic advance of phase α . Since the E.M.F. induced by the magnetism, or counter E.M.F. of self-induction, lags 90° behind the magnetism, it lags $90 + \alpha$ behind the current; that is, the self-induction in a circuit containing iron is not in quadrature with the current and thereby wattless, but lags more than 90° and thereby consumes power, so that the reactance has to be represented by $X = h - jx$, where h is what has been called the "effective hysteretic resistance."

A similar phenomenon takes place in alternators of variable reactance, or what is the same, variable magnetic reluctance.

207. Obviously, if the reactance or reluctance is variable, it will perform a complete cycle during the time the armature coil moves from one field pole to the next field pole, that is, during one-half wave of the main current. That is, in other words, the reluctance and reactance vary with twice the frequency of the alternating main current. Such a case is shown in Figs. 148 and 149. The impressed E.M.F., and thus at negligible resistance, the counter E.M.F., is represented by the sine wave E , thus the magnetism produced thereby is a sine wave M , 90° ahead of E . The reactance is represented by the sine wave x , varying with the double frequency of E , and shown in Fig. 148 to reach the maximum value during the rise of magnetism, in Fig. 149 during the decrease of magnetism. The current I required to produce the magnetism Φ is found from Φ and x in combination with the cycle of molecular magnetic friction of the material, and the power P is the product IE . As seen in Fig. 148, the positive part of P is larger than the

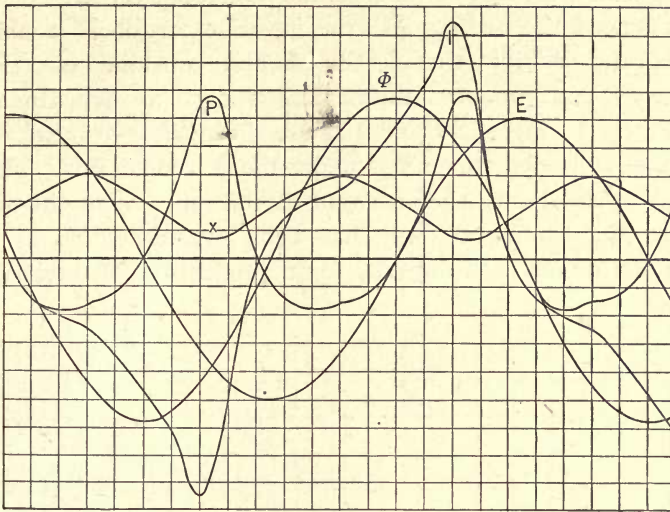


Fig. 148. Variable Reactance, Reaction Machine.

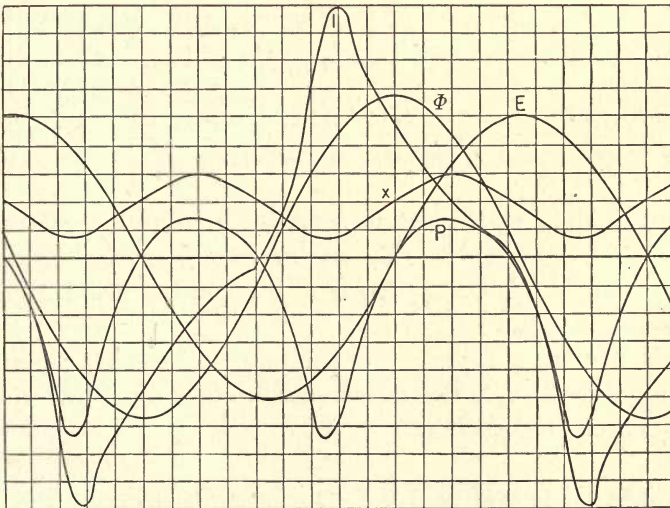


Fig. 149. Variable Reactance, Reaction Machine.

negative part ; that is, the machine produces electrical energy as generator. In Fig. 149 the negative part of P is larger than the positive ; that is, the machine consumes electrical energy and produces mechanical energy as synchronous motor. In Figs. 150 and 151 are given the two hysteretic cycles or looped curves Φ, I under the two conditions. They show that, due to the variation of reactance x , in the first case the hysteretic cycle has been overturned so as to represent not consumption, but production of electrical

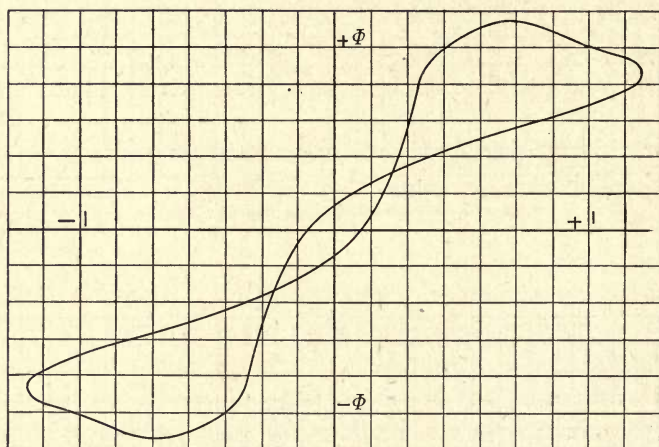


Fig. 150. Hysteretic Loop of Reaction Machine.

energy, while in the second case the hysteretic cycle has been widened, representing not only the electrical energy consumed by molecular magnetic friction, but also the mechanical output.

Hence, such a synchronous motor can be called "hysteresis motor," since the mechanical work is done by an extension of the loop of hysteresis.

208. It is evident that the variation of reluctance must be symmetrical with regard to the field poles ; that is, that the two extreme values of reluctance, maximum and mini-

imum, will take place at the moment where the armature coil stands in front of the field pole, and at the moment where it stands midway between the field poles.

The effect of this periodic variation of reluctance is a distortion of the wave of E.M.F., or of the wave of current, or of both. Here again, as before, the distorted wave can be replaced by the equivalent sine wave, or sine wave of equal effective intensity and equal power.

The instantaneous value of magnetism produced by the

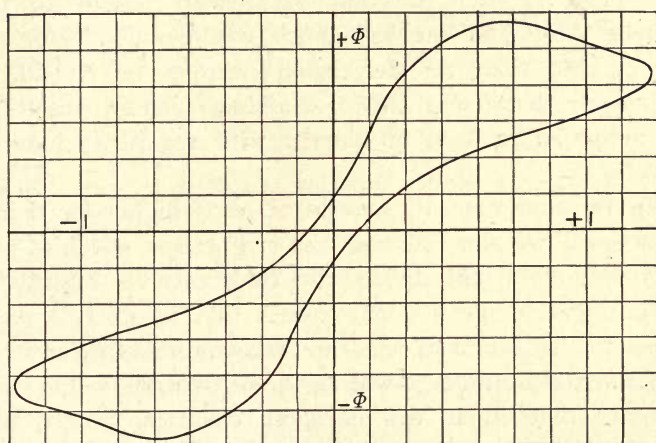


Fig. 151. Hysteretic Loop of Reaction Machine.

armature current — which magnetism induces in the armature conductor the E.M.F. of self-induction — is proportional to the instantaneous value of the current, divided by the instantaneous value of the reluctance. Since the extreme values of the reluctance coincide with the symmetrical positions of the armature with regard to the field poles, — that is, with zero and maximum value of the induced E.M.F., E_0 , of the machine, — it follows that, if the current is in phase or in quadrature with the E.M.F. E_0 , the reluctance wave is symmetrical to the current wave, and the wave of magnetism therefore symmetrical to the

current wave also. Hence the equivalent sine wave of magnetism is of equal phase with the current wave; that is, the E.M.F. of self-induction lags 90° behind the current, or is wattless.

Thus at no-phase displacement, and at 90° phase displacement, a reaction machine can neither produce electrical power nor mechanical power.

209. If, however, the current wave differs in phase from the wave of E.M.F. by less than 90° , but more than zero degrees, it is unsymmetrical with regard to the current wave, and the reluctance will be higher for rising current than for decreasing current, or it will be higher for decreasing than for rising current, according to the phase relation of current with regard to induced E.M.F., E_0 .

In the first case, if the reluctance is higher for rising, lower for decreasing, current, the magnetism, which is proportional to current divided by reluctance, is higher for decreasing than for rising current; that is, its equivalent sine wave lags behind the sine wave of current, and the E.M.F. or self-induction will lag more than 90° behind the current; that is, it will consume electrical power, and thereby deliver mechanical power, and do work as synchronous motor.

In the second case, if the reluctance is lower for rising, and higher for decreasing, current, the magnetism is higher for rising than for decreasing current, or the equivalent sine wave of magnetism leads the sine wave of the current, and the counter E.M.F. at self-induction lags less than 90° behind the current; that is, yields electric power as generator, and thereby consumes mechanical power.

In the first case the reactance will be represented by $X = h - jx$, similar as in the case of hysteresis; while in the second case the reactance will be represented by $X = -h - jx$.

210. The influence of the periodical variation of reactance will obviously depend upon the nature of the variation, that is, upon the shape of the reactance curve. Since, however, no matter what shape the wave has, it can always be dissolved in a series of sine waves of double frequency, and its higher harmonics, in first approximation the assumption can be made that the reactance or the reluctance vary with double frequency of the main current; that is, are represented in the form,

$$x = a + b \cos 2 \phi.$$

Let the inductance, or the coefficient of self-induction, be represented by —

$$\begin{aligned} L &= l + \phi \cos 2 \phi \\ &= l(1 + \gamma \cos 2 \phi) \end{aligned}$$

where γ = amplitude of variation of inductance.

Let

$\hat{\omega}$ = angle of lag of zero value of current behind maximum value of inductance L .

It is then, assuming the current as sine wave, or replacing it by the equivalent sine wave of effective intensity I , Current,

$$i = I\sqrt{2} \sin (\beta - \hat{\omega}).$$

The magnetism produced by this current is,

$$\Phi = \frac{L i}{n},$$

where n = number of turns.

Hence, substituted,

$$\Phi = \frac{l I \sqrt{2}}{n} \sin (\beta - \hat{\omega}) (1 + \gamma \cos 2 \beta),$$

or, expanded,

$$\Phi = \frac{l I \sqrt{2}}{n} \left\{ \left(1 - \frac{\gamma}{2}\right) \cos \hat{\omega} \sin \beta - \left(1 + \frac{\gamma}{2}\right) \sin \hat{\omega} \cos \beta \right\}$$

when neglecting the term of triple frequency, as wattless.

Thus the E.M.F. induced by this magnetism is,

$$\begin{aligned} e &= -n \frac{d\phi}{dt} \\ &= -2\pi N n \frac{d\phi}{d\beta} \end{aligned}$$

hence, expanded —

$$e = -2\pi N l I \sqrt{2} \left\{ \left(1 - \frac{\gamma}{2}\right) \cos \hat{\omega} \cos \beta + \left(1 + \frac{\gamma}{2}\right) \sin \hat{\omega} \sin \beta \right\}$$

and the effective value of E.M.F.,

$$\begin{aligned} E &= 2\pi N l I \sqrt{\left(1 - \frac{\gamma}{2}\right)^2 \cos^2 \hat{\omega} + \left(1 + \frac{\gamma}{2}\right)^2 \sin^2 \hat{\omega}} \\ &= 2\pi N l I \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2\hat{\omega}}. \end{aligned}$$

Hence, the apparent power, or the voltamperes —

$$\begin{aligned} P_0 &= IE = 2\pi N l I^2 \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2\hat{\omega}} \\ &= \frac{E^2}{2\pi N l \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2\hat{\omega}}}. \end{aligned}$$

The instantaneous value of power is

$$\begin{aligned} p &= ei \\ &= -4\pi N l I^2 \sin(\beta - \omega) \left\{ \left(1 - \frac{\gamma}{2}\right) \cos \omega \cos \beta + \right. \\ &\quad \left. \left(1 + \frac{\gamma}{2}\right) \sin \omega \sin \beta \right\}. \end{aligned}$$

and, expanded —

$$\begin{aligned} p &= -2\pi N l I^2 \left\{ \left(1 + \frac{\gamma}{2}\right) \sin 2\omega \sin^2 \beta - \left(1 - \frac{\gamma}{2}\right) \right. \\ &\quad \left. \sin 2\omega \cos^2 \beta + \sin 2\beta \left(\cos 2\omega - \frac{\gamma}{2}\right) \right\} \end{aligned}$$

Integrated, the effective value of power is

$$P = -\pi N l I^2 \gamma \sin 2\hat{\omega};$$

hence, negative ; that is, the machine consumes electrical, and produces mechanical, power, as synchronous motor, if $\hat{\omega} > 0$; that is, with lagging current.

Positive ; that is, the machine produces electrical, and consumes mechanical, power, as generator, if $\hat{\omega} < 0$; that is, with leading current.

The power factor is

$$f = \frac{P}{P} = \frac{\gamma \sin 2 \hat{\omega}}{2 \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2 \hat{\omega}}}$$

hence, a maximum, if,

$$\frac{df}{d\hat{\omega}} = 0 ;$$

or, expanded,

$$\cos 2 \hat{\omega} = \frac{1}{\gamma} + \frac{\gamma}{4} \pm \frac{1}{4} \sqrt{8 + \gamma^2}.$$

The power, P , is a maximum at given current, I , if

$$\sin 2 \hat{\omega} = 1 ;$$

that is,

$$\hat{\omega} = 45^\circ$$

at given E.M.F., E , the power is

$$P = - \frac{E^2 \gamma \sin 2 \hat{\omega}}{4 \pi N l \left(1 + \frac{\gamma^2}{4} - \gamma \cos 2 \hat{\omega} \right)} ;$$

hence, a maximum at

$$\frac{\delta P}{\delta \hat{\omega}} = 0 ;$$

or, expanded,

$$\cos 2 \hat{\omega} = \frac{\pm \gamma}{1 + \frac{\gamma^2}{4}}.$$

211. We have thus, at impressed E.M.F., E , and negligible resistance, if we denote the mean value of reactance,

$$x = 2 \pi N l.$$

Current

$$I = \frac{E}{x \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2 \hat{\omega}}}.$$

Voltamperes,

$$P_0 = \frac{E^2}{x \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2 \hat{\omega}}}.$$

Power,

$$P = -\frac{E^2 \gamma \sin 2 \hat{\omega}}{2 x \left(1 + \frac{\gamma^2}{4} - \gamma \cos 2 \hat{\omega}\right)}.$$

Power factor,

$$f = \cos (E, I) = \frac{\gamma \sin 2 \hat{\omega}}{2 \sqrt{1 + \frac{\gamma^2}{4} - \gamma \cos 2 \hat{\omega}}}.$$

Maximum power at

$$\cos 2 \hat{\omega} = \frac{\gamma}{1 + \frac{\gamma^2}{4}}.$$

Maximum power factor at

$$\cos 2 \hat{\omega} = \frac{1}{\gamma} + \frac{\gamma}{4} \pm \frac{1}{4} \sqrt{8 + \gamma^2}$$

$\hat{\omega} > 0$: synchronous motor, with lagging current,

$\hat{\omega} < 0$: generator, with leading current.

As an instance is shown in Fig. 152, with angle $\hat{\omega}$ as abscissæ, the values of current, power, and power factor, for the constants, —

$$E = 110$$

$$x = 3$$

$$\gamma = .8$$

hence,

$$I = \frac{41}{\sqrt{1.45 - \cos 2 \hat{\omega}}}$$

$$P = \frac{-2017 \sin 2 \hat{\omega}}{1.45 - \cos 2 \hat{\omega}}$$

$$f = \cos (E, I) = \frac{.447 \sin 2 \hat{\omega}}{\sqrt{1.45 - \cos 2 \hat{\omega}}}$$

As seen from Fig. 152, the power factor f of such a machine is very low — does not exceed 40 per cent in this instance.

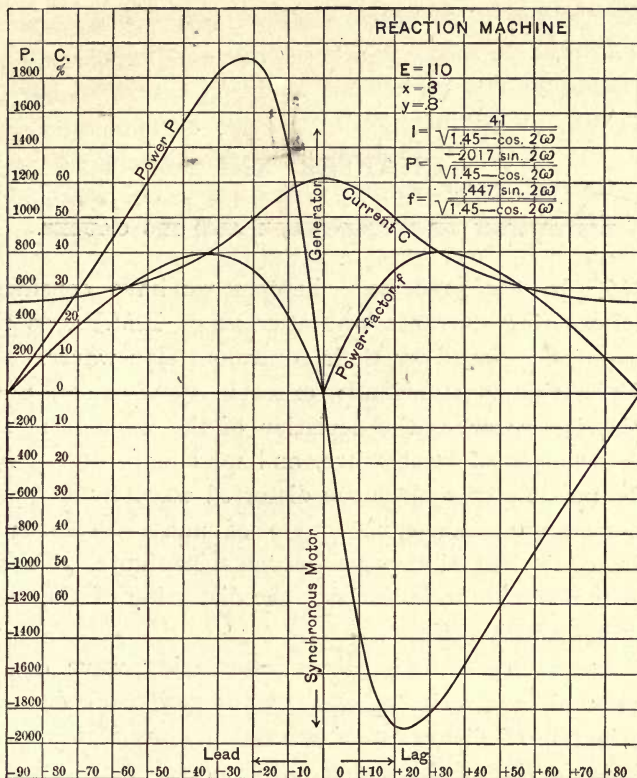


Fig. 152. Reaction Machine.

CHAPTER XXI.

DISTORTION OF WAVE-SHAPE AND ITS CAUSES.

212. In the preceding chapters we have considered the alternating currents and alternating E.M.Fs. as sine waves or as replaced by their equivalent sine waves.

While this is sufficiently exact in most cases, under certain circumstances the deviation of the wave from sine shape becomes of importance, and no longer, and it may not be possible to replace the distorted wave by an equivalent sine wave, since the angle of phase displacement of the equivalent sine wave becomes indefinite. Thus it becomes desirable to investigate the distortion of the wave, its causes and its effects.

Since, as stated before, any alternating wave can be represented by a series of sine functions of odd orders, the investigation of distortion of wave-shape resolves itself in the investigation of the higher harmonics of the alternating wave.

In general we have to distinguish between higher harmonics of E.M.F. and higher harmonics of current. Both depend upon each other in so far as with a sine wave of impressed E.M.F. a distorting effect will cause distortion of the current wave, while with a sine wave of current passing through the circuit, a distorting effect will cause higher harmonics of E.M.F.

213. In a conductor revolving with uniform velocity through a uniform and constant magnetic field, a sine wave of E.M.F. is induced. In a circuit with constant resistance and constant reactance, this sine wave of E.M.F. produces

a sine wave of current. Thus distortion of the wave-shape or higher harmonics may be due to: lack of uniformity of the velocity of the revolving conductor; lack of uniformity or pulsation of the magnetic field; pulsation of the resistance; or pulsation of the reactance.

The first two cases, lack of uniformity of the rotation or of the magnetic field, cause higher harmonics of E.M.F. at open circuit. The last, pulsation of resistance and reactance, causes higher harmonics only with a current flowing in the circuit, that is, under load.

Lack of uniformity of the rotation is of no practical interest as cause of distortion, since in alternators, due to mechanical momentum, the speed is always very nearly uniform.

Thus as causes of higher harmonics remain:

1st. Lack of uniformity and pulsation of the magnetic field, causing a distortion of the induced E.M.F. at open circuit as well as under load.

2d. Pulsation of the reactance, causing higher harmonics under load.

3d. Pulsation of the resistance, causing higher harmonics under load also.

Taking up the different causes of higher harmonics we have:—

Lack of Uniformity and Pulsation of the Magnetic Field.

214. Since most of the alternating-current generators contain definite and sharply defined field poles covering in different types different proportions of the pitch, in general the magnetic flux interlinked with the armature coil will not vary as simply sine wave, of the form:

$$\Phi \cos \beta,$$

but as a complex harmonic function.

However, with an armature of uniform magnetic reluctance, in general the distortion caused by the shape of the

field poles is small and negligible, as for instance the curves Fig. 153 and Fig. 154 show, which represent the no-load and full-load wave of E.M.F. of a three-phase multitooth alternator.

Even where noticeable, these harmonics can be considered together with the harmonics due to the varying reluctance of the magnetic circuit.

In ironclad alternators with few slots and teeth per pole, the passage of slots across the field poles causes a pulsation of the magnetic reluctance, or its reciprocal, the magnetic inductance of the circuit. In consequence thereof the magnetism per field pole, or at least that part of the magnetism passing through the armature, will pulsate with a frequency 2γ if γ = number of slots per pole.

Thus, in a machine with one slot per pole, the instantaneous magnetic flux interlinked with the armature conductors can be expressed by the equation :

$$\phi = \Phi \cos \beta \{1 + \epsilon \cos [2\beta - \omega]\}$$

where,

ϕ = average magnetic flux,

ϵ = amplitude of pulsation,

and

ω = phase of pulsation.

In a machine with γ slots per pole, the instantaneous flux interlinked with the armature conductors will be :

$$\phi = \Phi \cos \beta \{1 + \epsilon \cos [2\gamma\beta - \omega]\},$$

if the assumption is made that the pulsation of the magnetic flux follows a simple sine law, as can be done approximately.

In general the instantaneous magnetic flux interlinked with the armature conductors will be :

$$\phi = \Phi \cos \beta \{1 + \epsilon_1 \cos (2\beta - \hat{\omega}_1) + \epsilon_2 \cos (4\beta - \hat{\omega}_2) + \dots\},$$

where the terms ϵ_γ is predominating if γ = number of armature slots per pole.

This general equation includes also the effect of lack of uniformity of the magnetic flux.

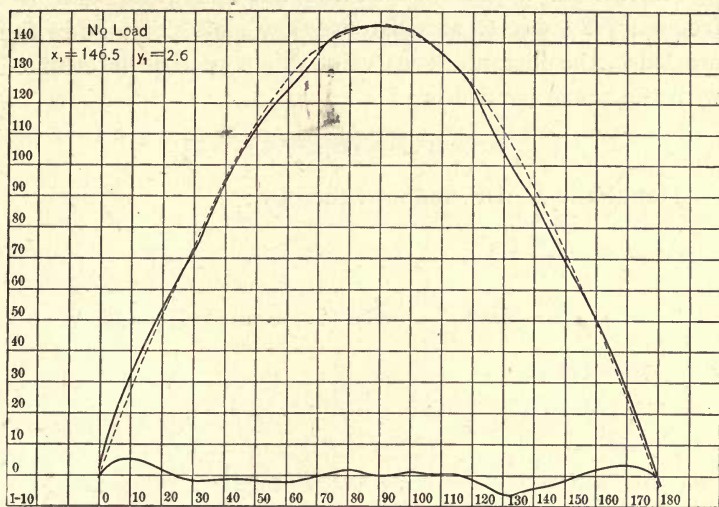


Fig. 153. No-load Wave of E.M.F. of Multitooth Three-phaser.

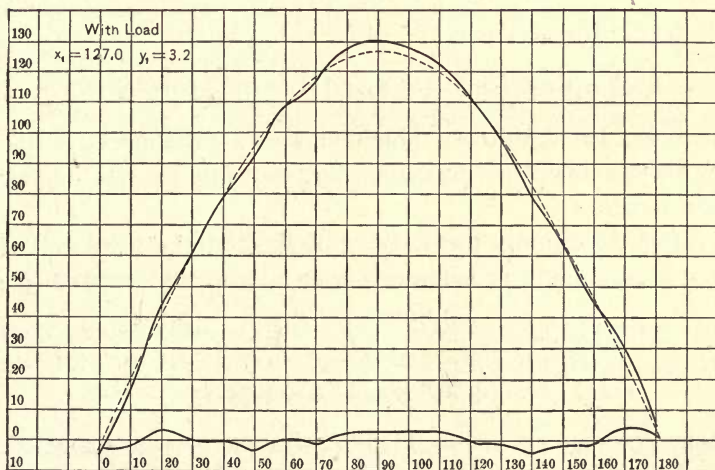


Fig. 154. Full-Load Wave of E.M.F. of Multitooth Three-phaser.

In case of a pulsation of the magnetic flux with the frequency 2γ , due to an existence of γ slots per pole in the armature, the instantaneous value of magnetism interlinked with the armature coil is :

$$\phi = \Phi \cos \beta \{1 + \epsilon \cos [2\gamma\beta - \hat{\omega}]\}.$$

Hence the E.M.F. induced thereby :

$$\begin{aligned} e &= -n \frac{d\phi}{dt} \\ &= -\sqrt{2} \pi N n \Phi \frac{d}{d\beta} \{\cos \beta (1 + \epsilon \cos [2\gamma\beta - \hat{\omega}])\}. \end{aligned}$$

And, expanded :

$$\begin{aligned} e &= \sqrt{2} \pi N n \Phi \left\{ \sin \beta + \epsilon \frac{2\gamma - 1}{2} \sin [(2\gamma - 1)\beta - \hat{\omega}] \right. \\ &\quad \left. + \epsilon \frac{2\gamma + 1}{2} \sin [(2\gamma + 1)\beta - \hat{\omega}] \right\}. \end{aligned}$$

Hence, the pulsation of the magnetic flux with the frequency 2γ , as due to the existence of γ slots per pole, introduces two harmonics, of the orders $(2\gamma - 1)$ and $(2\gamma + 1)$.

215. If $\gamma = 1$ it is :

$$e = \sqrt{2} \pi N n \Phi \left\{ \sin \beta + \frac{\epsilon}{2} \sin (\beta - \hat{\omega}) + \frac{3\epsilon}{2} \sin (3\beta - \hat{\omega}) \right\};$$

that is : In a unitooth single-phaser a pronounced triple harmonic may be expected, but no pronounced higher harmonics.

Fig. 155 shows the wave of E.M.F. of the main coil of a standard monocyclic alternator at no load, represented by :

$$\begin{aligned} e &= E \{ \sin \beta - .242 \sin (3\beta - 6.3) - .046 \sin (5\beta - 2.6) \\ &\quad + .068 \sin (7\beta - 3.3) - .027 \sin (9\beta - 10.0) - .018 \sin \\ &\quad (11\beta - 6.6) + .029 \sin (13\beta - 8.2) \}; \end{aligned}$$

hence giving a pronounced triple harmonic only, as expected.

If $\gamma = 2$, it is :

$$e = \sqrt{2} \pi N n \Phi \left\{ \sin \beta + \frac{3\epsilon}{2} \sin (3\beta - \hat{\omega}) + \frac{5\epsilon}{2} \sin (5\beta - \hat{\omega}) \right\}$$

the no-load wave of a unitooth quarter-phase machine, having pronounced triple and quintuple harmonics.

If $\gamma = 3$, it is:

$$e = \sqrt{2} \pi N n \Phi \left\{ \sin \beta + \frac{5\epsilon}{2} \sin (5\beta - \omega) + \frac{7\epsilon}{2} \sin (7\beta - \omega) \right\}.$$

That is: In a unitooth three-phaser, a pronounced quintuple and septuple harmonic may be expected, but no pronounced triple harmonic.

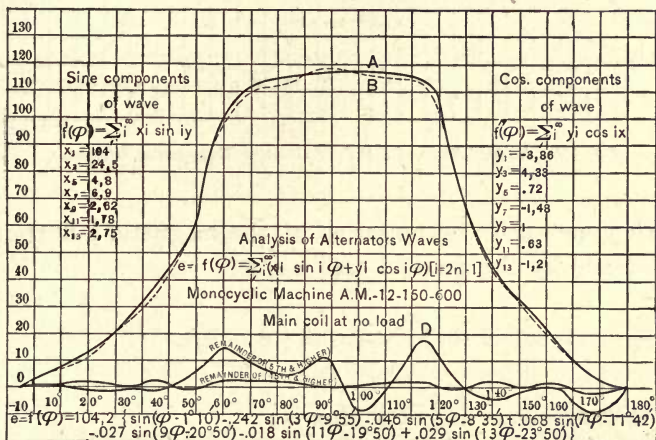


Fig. 155. No-load Wave of E.M.F. of Unitooth Monocyclic Alternator.

Fig. 156 shows the wave of E.M.F. of a standard unitooth three-phaser at no load, represented by:

$$e = E \{ \sin \beta - .12 \sin (3\beta - 2.3) - .23 \sin (5\beta - 1.5) + .134 \sin (7\beta - 6.2) - .002 \sin (9\beta + 27.7) - .046 \sin (11\beta - 5.5) + .031 \sin (13\beta - 61.5) \}.$$

Thus giving a pronounced quintuple and septuple and a lesser triple harmonic, probably due to the deviation of the field from uniformity, and deviation of the pulsation of reluctance from sine shape.

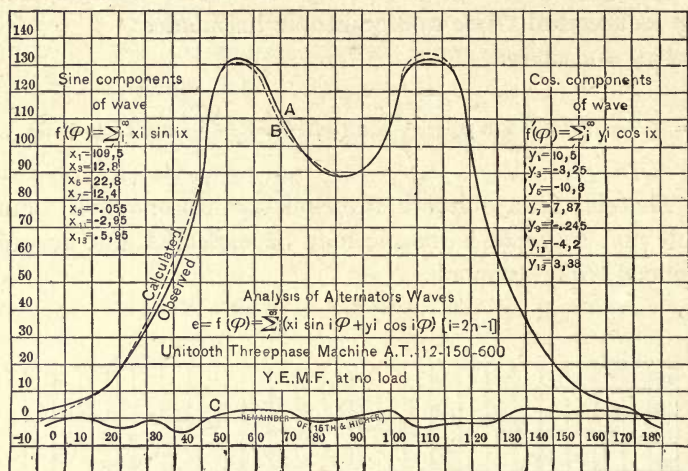


Fig. 156. No-load Wave of E.M.F. of Unitooth Three-phase Alternator.

In general, if the pulsation of the magnetic inductance is denoted by the general expression:

$$1 + \sum_{\gamma}^{\infty} \epsilon_{\gamma} \cos (2 \gamma \beta - \hat{\omega}_{\gamma}),$$

the instantaneous magnetic flux is:

$$\begin{aligned} \phi &= \Phi \cos \beta \left\{ 1 + \sum_{\gamma}^{\infty} \epsilon_{\gamma} \cos (2 \gamma \beta - \hat{\omega}_{\gamma}) \right\} \\ &= \Phi \left\{ \cos \beta + \frac{\epsilon_1}{2} \cos (\beta - \hat{\omega}_1) + \sum_{\gamma}^{\infty} \left[\frac{\epsilon_{\gamma}}{2} \cos ((2 \gamma + 1) \right. \right. \\ &\quad \left. \left. \beta - \hat{\omega}_{\gamma}) + \frac{\epsilon_{\gamma+1}}{2} \cos ((2 \gamma + 1) \beta - \hat{\omega}_{\gamma+1}) \right] \right\} \end{aligned}$$

hence, the E.M.F.

$$\begin{aligned} e &= \sqrt{2} \pi N n \Phi \left\{ \sin \beta + \frac{\epsilon_1}{2} \sin (\beta - \hat{\omega}_1) + \sum_{\gamma}^{\infty} \frac{2 \gamma + 1}{2} \right. \\ &\quad \left. [\epsilon_{\gamma} \sin ((2 \gamma + 1) \beta - \hat{\omega}_{\gamma}) + \epsilon_{\gamma+1} \sin ((2 \gamma + 1) \beta - \hat{\omega}_{\gamma+1})] \right\} \end{aligned}$$

Pulsation of Reactance.

216. The main causes of a pulsation of reactance are: magnetic saturation and hysteresis, and synchronous motion. Since in an ironclad magnetic circuit the magnetism is not proportional to the M.M.F., the wave of magnetism and thus the wave of E.M.F. will differ from the wave of current. As far as this distortion is due to the variation of permeability, the distortion is symmetrical and the wave of induced E.M.F. represents no power. The distortion caused by hysteresis, or the lag of the magnetism behind the M.M.F., causes an unsymmetrical distortion of the wave which makes the wave of induced E.M.F. differ by more than 90° from the current wave and thereby represents power, — the power consumed by hysteresis.

In practice both effects are always superimposed; that is, in a ferric inductance, a distortion of wave-shape takes place due to the lack of proportionality between magnetism and M.M.F. as expressed by the variation of the permeability in the hysteretic cycle.

This pulsation of reactance gives rise to a distortion consisting mainly of a triple harmonic. Such current waves distorted by hysteresis, with a sine wave of impressed E.M.F., are shown in Figs. 66 to 69, Chapter X., on Hysteresis. Inversely, if the current is a sine wave, the magnetism and the E.M.F. will differ from sine shape.

For further discussion of this distortion of wave-shape by hysteresis, Chapter X. may be consulted.

217. Distortion of wave-shape takes place also by the pulsation of reactance due to synchronous rotation, as discussed in chapter on Reaction Machines.

In Figs. 148 and 149, at a sine wave of impressed E.M.F., the distorted current waves have been constructed.

Inversely, if a sine wave of current,

$$i = I \cos \beta,$$

passes through a circuit of synchronously varying reactance; as for instance, the armature of a unitooth alternator or synchronous motor — or, more general, an alternator whose armature reluctance is different in different positions with regard to the field poles — and the reactance is expressed by

$$X = x \{1 + \epsilon \cos (2\beta - \hat{\omega})\};$$

or, more general,

$$X = x \left\{ 1 + \sum_1^{\infty} \epsilon_{\gamma} \cos (2\gamma\beta - \hat{\omega}_{\gamma}) \right\};$$

the wave of magnetism is

$$\begin{aligned} \phi &= \frac{X}{2\pi Nn} \cos \beta = \frac{x}{2\pi Nn} \left\{ \cos \beta + \sum_1^{\infty} \epsilon_{\gamma} \cos \beta \cos (2\gamma\beta - \hat{\omega}_{\gamma}) \right\} \\ &= \frac{x}{2\pi Nn} \left\{ \cos \beta + \frac{\epsilon_1}{2} \cos (\beta - \hat{\omega}_1) + \sum_1^{\infty} \left[\frac{\epsilon_{\gamma}}{2} \cos ((2\gamma + 1) \right. \right. \\ &\quad \left. \left. \beta - \hat{\omega}_{\gamma}) + \frac{\epsilon_{\gamma} + 1}{2} \cos ((2\gamma + 1)\beta - \hat{\omega}_{\gamma} + 1) \right] \right\}; \end{aligned}$$

hence the wave of induced E.M.F.

$$\begin{aligned} e &= -n \frac{d\phi}{dt} = -2\pi Nn \frac{d\phi}{d\beta} \\ &= x \left\{ \sin \beta + \frac{\epsilon_1}{2} \sin (\beta - \hat{\omega}_1) + \sum_1^{\infty} \frac{2\gamma + 1}{2} \left[\epsilon_{\gamma} \sin ((2\gamma + 1) \right. \right. \\ &\quad \left. \left. \beta - \hat{\omega}_{\gamma}) + \epsilon_{\gamma} + 1 \sin ((2\gamma + 1)\beta - \hat{\omega}_{\gamma} + 1) \right] \right\}; \end{aligned}$$

that is, the pulsation of reactance of frequency, 2γ , introduces two higher harmonics of the order $(2\gamma - 1)$, and $(2\gamma + 1)$.

$$\text{If } X = x \{1 + \epsilon \cos (2\beta - \omega)\},$$

$$\begin{aligned} \text{it is } \phi &= \frac{x}{2\pi Nn} \left\{ \cos \beta + \frac{\epsilon}{2} \cos (\beta - \hat{\omega}) + \frac{\epsilon}{2} \cos (3\beta - \hat{\omega}) \right\}; \\ e &= x \left\{ \sin \beta + \frac{\epsilon}{2} \sin (\beta - \hat{\omega}) + \frac{3\epsilon}{2} \sin (3\beta - \omega) \right\}. \end{aligned}$$

Since the pulsation of reactance due to magnetic saturation and hysteresis is essentially of the frequency, $2N$,

— that is, describes a complete cycle for each half-wave of current, — this shows why the distortion of wave-shape by hysteresis consists essentially of a triple harmonic.

The phase displacement between e and i , and thus the power consumed or produced in the electric circuit, depend upon the angle, $\hat{\omega}$, as discussed before.

218. In case of a distortion of the wave-shape by reactance, the distorted waves can be replaced by their equivalent sine waves, and the investigation with sufficient exactness for most cases be carried out under the assumption of sine waves, as done in the preceding chapters.

Similar phenomena take place in circuits containing polarization cells, leaky condensers, or other apparatus representing a synchronously varying negative reactance. Possibly dielectric hysteresis in condensers causes a distortion similar to that due to magnetic hysteresis.

Pulsation of Resistance.

219. To a certain extent the investigation of the effect of synchronous pulsation of the resistance coincides with that of reactance; since a pulsation of reactance, when unsymmetrical with regard to the current wave, introduces an energy component which can be represented by an "effective resistance."

Inversely, an unsymmetrical pulsation of the ohmic resistance introduces a wattless component, to be denoted by "effective reactance."

A typical case of a synchronously pulsating resistance is represented in the alternating arc.

The apparent resistance of an arc depends upon the current passing through the arc; that is, the apparent resistance of the arc = $\frac{\text{potential difference between electrodes}}{\text{current}}$ is high for small currents, low for large currents. Thus in an alternating arc the apparent resistance will vary during

every half-wave of current between a maximum value at zero current and a minimum value at maximum current, thereby describing a complete cycle per half-wave of current.

Let the effective value of current passing through the arc be represented by I .

Then the instantaneous value of current, assuming the current wave as sine wave, is represented by

$$i = \sqrt{2} \sin \beta;$$

and the apparent resistance of the arc, in first approximation, by

$$R = r(1 + \epsilon \cos 2\phi);$$

thus the potential difference at the arc is

$$\begin{aligned} e &= iR = I\sqrt{2}r \sin \phi (1 + \epsilon \cos 2\phi) \\ &= rI\sqrt{2} \left\{ \left(1 - \frac{\epsilon}{2}\right) \sin \phi + \frac{\epsilon}{2} \sin 3\phi \right\}. \end{aligned}$$

Hence the effective value of potential difference,

$$\begin{aligned} E &= rI\sqrt{\left(1 - \frac{\epsilon}{2}\right)^2 + \frac{\epsilon^2}{4}} \\ &= rI\sqrt{1 - \epsilon + \frac{\epsilon^2}{2}}. \end{aligned}$$

and the apparent resistance of the arc,

$$r_0 = \frac{E}{I} = r\sqrt{1 - \epsilon + \frac{\epsilon^2}{2}}.$$

The instantaneous power consumed in the arc is,

$$p = ie = 2rI^2 \left\{ \left(1 - \frac{\epsilon}{2}\right) \sin^2 \phi + \frac{\epsilon}{2} \sin \phi \sin 3\phi \right\}.$$

Hence the effective power,

$$P = rI^2 \left(1 - \frac{\epsilon}{2}\right).$$

The apparent power, or volt amperes consumed by the arc, is,

$$IE = rI^2 \sqrt{1 - \epsilon + \frac{\epsilon^2}{2}}.$$

thus the power factor of the arc,

$$f = \frac{P}{IE} = \frac{1 - \frac{\epsilon}{2}}{\sqrt{1 - \epsilon + \frac{\epsilon^2}{2}}}.$$

that is, less than unity.

220. We find here a case of a circuit in which the power factor—that is, the ratio of watts to volt amperes—differs from unity without any displacement of phase; that is, while current and E.M.F. are in phase with each other, but are distorted, the alternating wave cannot be replaced by an equivalent sine wave; since the assumption of equivalent sine wave would introduce a phase displacement,

$$\cos \hat{\omega} = f$$

of an angle, $\hat{\omega}$, whose sign is indefinite.

As an instance are shown, in Fig. 157 for the constants,

$$I = 12$$

$$r = 3$$

$$\epsilon = .9$$

the resistance,

$$R = 3 \{1 + .9 \cos 2 \beta\};$$

the current,

$$i = 17 \sin \beta;$$

the potential difference,

$$e = 28 (\sin \beta + .82 \sin 3 \beta).$$

In this case the effective E.M.F. is

$$E = 25.5;$$

the apparent resistance,

$$r_0 = 2.13;$$

the power,

$$P = 244;$$

the apparent power,

$$EI = 307;$$

the power factor,

$$f = .796.$$

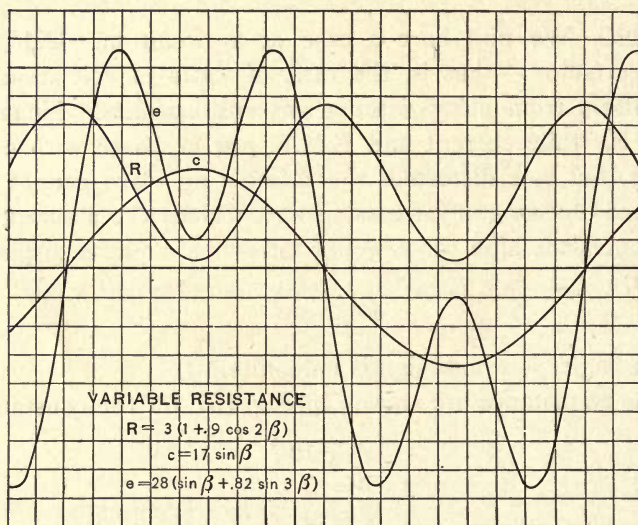


Fig. 157. Periodically Varying Resistance.

As seen, with a sine wave of current the E.M.F. wave in an alternating arc will become double-peaked, and rise very abruptly near the zero values of current. Inversely, with a sine wave of E.M.F. the current wave in an alternating arc will become peaked, and very flat near the zero values of E.M.F.

221. In reality the distortion is of more complex nature; since the pulsation of resistance in the arc does not follow

a simple sine law of double frequency, but varies much more abruptly near the zero value of current, making thereby the variation of E.M.F. near the zero value of current much more abruptly, or, inversely, the variation of current more flat.

A typical wave of potential difference, with a sine wave of current passing through the arc, is given in Fig. 158.*

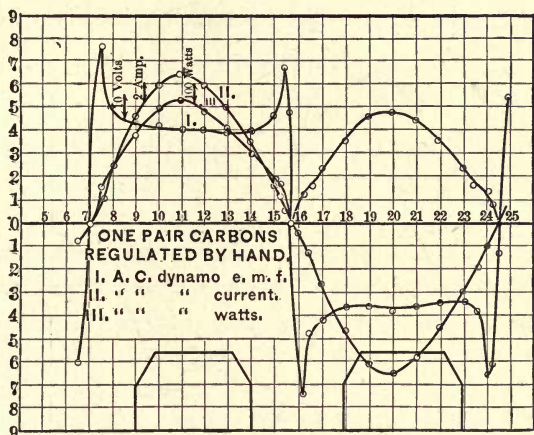


Fig. 158. Electric Arc.

222. The value of ϵ , the amplitude of the resistance pulsation, largely depends upon the nature of the electrodes and the steadiness of the arc, and with soft carbons and a steady arc is small, and the power factor f of the arc near unity. With hard carbons and an unsteady arc, ϵ rises greatly, higher harmonics appear in the pulsation of resistance, and the power factor f falls, being in extreme cases even as low as .6.

The conclusion to be drawn herefrom is, that photometric tests of alternating arcs are of little value, if, besides current and voltage, the power is not determined also by means of electro-dynamometers.

* From American Institute of Electrical Engineers, Transactions, 1890, p. 376. Tobey and Walbridge, on the Stanley Alternate Arc Dynamo.

CHAPTER XXII.

EFFECTS OF HIGHER HARMONICS.

223. To elucidate the variation in the shape of alternating waves caused by various harmonics, in Figs. 159 and

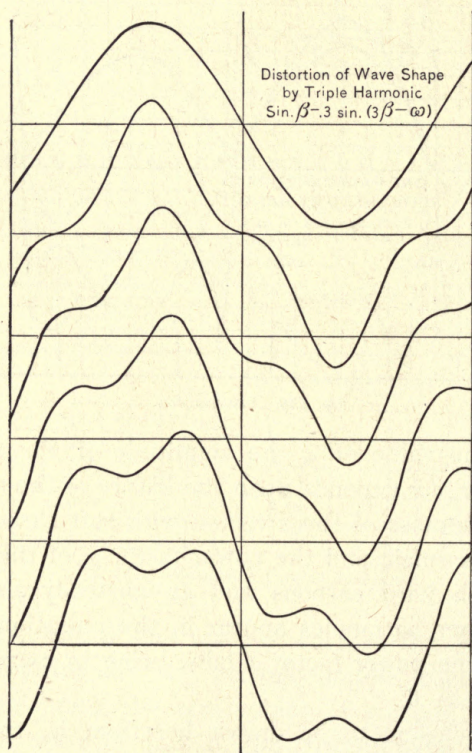


Fig. 159. Effect of Triple Harmonic.

160 are shown the wave-forms produced by the superposition of the triple and the quintuple harmonic upon the fundamental sine wave.

In Fig. 159 is shown the fundamental sine wave and the complex waves produced by the superposition of a triple harmonic of 30 per cent the amplitude of the fundamental, under the relative phase displacements of 0° , 45° , 90° , 135° , and 180° , represented by the equations :

$$\begin{aligned} & \sin \beta \\ & \sin \beta - .3 \sin 3 \beta \\ & \sin \beta - .3 \sin (3 \beta - 45^\circ) \\ & \sin \beta - .3 \sin (3 \beta - 90^\circ) \\ & \sin \beta - .3 \sin (3 \beta - 135^\circ) \\ & \sin \beta - .3 \sin (3 \beta - 180^\circ). \end{aligned}$$

As seen, the effect of the triple harmonic is in the first figure to flatten the zero values and point the maximum values of the wave, giving what is called a peaked wave. With increasing phase displacement of the triple harmonic, the flat zero rises and gradually changes to a second peak, giving ultimately a flat-top or even double-peaked wave with sharp zero. The intermediate positions represent what is called a saw-tooth wave.

In Fig. 160 are shown the fundamental sine wave and the complex waves produced by superposition of a quintuple harmonic of 20 per cent the amplitude of the fundamental, under the relative phase displacement of 0° , 45° , 90° , 135° , 180° , represented by the equations :

$$\begin{aligned} & \sin \beta \\ & \sin \beta - .2 \sin 5 \beta \\ & \sin \beta - .2 \sin (5 \beta - 45^\circ) \\ & \sin \beta - .2 \sin (5 \beta - 90^\circ) \\ & \sin \beta - .2 \sin (5 \beta - 135^\circ) \\ & \sin \beta - .2 \sin (5 \beta - 180^\circ). \end{aligned}$$

The quintuple harmonic causes a flat-topped or even double-peaked wave with flat zero. With increasing phase displacement, the wave becomes of the type called saw-tooth wave also. The flat zero rises and becomes a third peak, while of the two former peaks, one rises, the other

decreases, and the wave gradually changes to a triple-peaked wave with one main peak, and a sharp zero.

As seen, with the triple harmonic, flat-top or double-peak coincides with sharp zero, while the quintuple harmonic flat-top or double-peak coincides with flat zero.

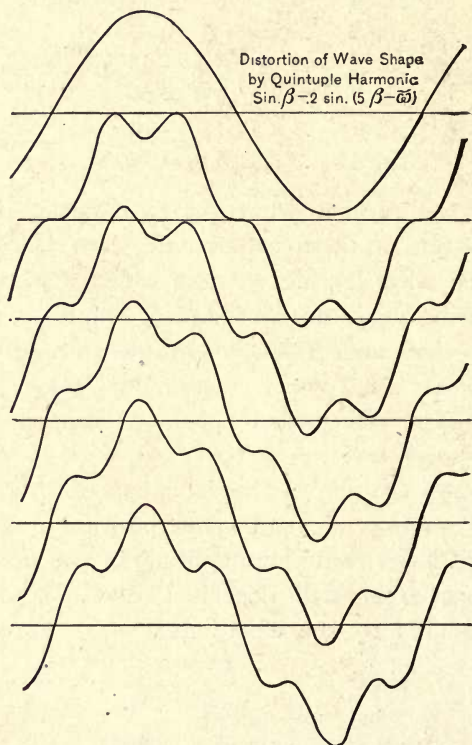


Fig. 160. Effect of Quintuple Harmonic.

Sharp peak coincides with flat zero in the triple, with sharp zero in the quintuple harmonic.

Thus in general, from simple inspection of the wave shape, the existence of these first harmonics can be discovered.

Some characteristic shapes of curves are shown in Fig. 161:

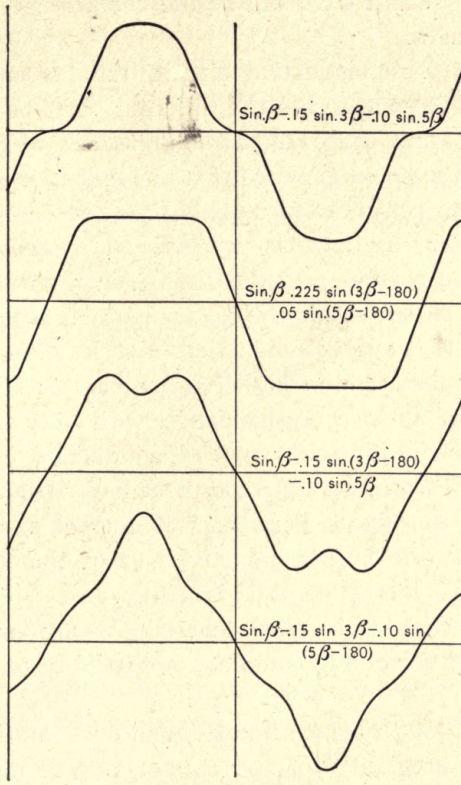


Fig. 161. Some Characteristic Wave Shapes.

Flat top with flat zero :

$$\sin \beta - .15 \sin 3\beta - .10 \sin 5\beta.$$

Flat top with sharp zero :

$$\sin \beta - .225 \sin (3\beta - 180^\circ) - .05 \sin (5\beta - 180^\circ).$$

Double peak, with sharp zero :

$$\sin \beta - .15 \sin (3\beta - 180^\circ) - .10 \sin 5\beta.$$

Sharp peak with sharp zero :

$$\sin \beta - .15 \sin 3\beta - .10 \sin (5\beta - 180^\circ).$$

224. Since the distortion of the wave-shape consists in the superposition of higher harmonics, that is, waves of higher frequency, the phenomena taking place in a circuit

supplied by such a wave will be the combined effect of the different waves.

Thus in a non-inductive circuit, the current and the potential difference across the different parts of the circuit are of the same shape as the impressed E.M.F. If self-induction is inserted in series to a non-inductive circuit, the self-induction consumes more E.M.F. of the higher harmonics, since the reactance is proportional to the frequency, and thus the current and the E.M.F. in the non-inductive part of the circuit shows the higher harmonics in a reduced amplitude. That is, self-induction in series to a non-inductive circuit reduces the higher harmonics or smooths out the wave to a closer resemblance with sine shape. Inversely, capacity in series to a non-inductive circuit consumes less E.M.F. at higher than at lower frequency, and thus makes the higher harmonics of current and of potential difference in the non-inductive part of the circuit more pronounced — intensifies the harmonics.

Self-induction and capacity in series may cause an increase of voltage due to complete or partial resonance.

225. In long-distance transmission over lines of noticeable inductance and capacity, rise of voltage due to resonance may under circumstances be expected with higher harmonics, as waves of higher frequency, while the fundamental wave is usually of too low a frequency to cause resonance.

An approximate estimate of the possible rise by resonance with various harmonics can be obtained by the investigation of a numerical instance. Let in a long-distance line, fed by step-up transformers:

The resistance drop in the transformers at full load = 1 per cent.

The inductance drop in the transformers at full load = 5 per cent with the fundamental wave.

The resistance drop in the line at full load = 10 per cent.

The inductance drop in the line at full load = 20 per cent with the fundamental wave.

The capacity or charging current of the line = 20 per cent of the full-load current I at the frequency of the fundamental.

The line capacity may approximately be represented by a condenser shunted across the middle of the line. The E.M.F. at the generator terminals E is assumed as maintained constant.

The E.M.F. consumed by the resistance of the circuit from generator terminals to condenser is

$$Ir = .06 E,$$

or,

$$r = .06 \frac{E}{I}.$$

The reactance E.M.F. between generator terminals and condenser is, for the fundamental frequency,

$$Ix = .15 E,$$

or,

$$x = .15 \frac{E}{I},$$

thus the reactance corresponding to the frequency $(2k - 1)N$ of the higher harmonic is :

$$x(2k - 1) = .15(2k - 1) \frac{E}{I}.$$

The capacity current at fundamental frequency is :

$$i = .2 I,$$

hence, at the frequency : $(2k - 1)N$:

$$i = .2(2k - 1) e' \frac{I}{E},$$

if :

e' = E.M.F. of the $(2k - 1)$ th harmonic at the condenser,

e = E.M.F. of the $(2k - 1)$ th harmonic at the generator terminals.

The E.M.F. at the condenser is : —

$$e' = \sqrt{e^2 - i^2 r^2} + ix(2k - 1)^2;$$

hence, substituted :

$$a = \frac{e'}{e} = \frac{1}{\sqrt{1 - .059856 (2k - 1)^2 + .0009 (2k - 1)^4}},$$

the rise of voltage by inductance and capacity.

Substituting :

	$k = 1$	2	3	4	5	6
or, $2k - 1 =$	1	3	5	7	9	11
it is, $a =$	1.03	1.36	3.76	2.18	.70	.38

That is, the fundamental will be increased at open circuit by 3 per cent, the triple harmonic by 36 per cent, the quintuple harmonic by 276 per cent, the septuple harmonic by 118 per cent, while the still higher harmonics are reduced.

The maximum possible rise will take place for :

$$\frac{da}{d(2k - 1)} = 0,$$

or,

$$k = 5.77.$$

That is, at a frequency :

$$N = 346.$$

and is :

$$a = 14.4.$$

That is, complete resonance will appear at a frequency between quintuple and septuple harmonic, and would raise the voltage at this particular frequency 14.4 fold.

If the voltage shall not exceed the impressed voltage by more than 100 per cent, even at coincidence of the maximum of the harmonic with the maximum of the fundamental,

the triple harmonic must be less than 70 per cent of the fundamental,

the quintuple harmonic must be less than 26.5 per cent of the fundamental,

the septuple harmonic must be less than 46 per cent of the fundamental.

The voltage will not exceed twice the normal, even at a frequency of complete resonance with the higher harmonic, if none of the higher harmonics amounts to more than 7 per cent. of the fundamental.

Herefrom it follows that the danger of resonance in high potential lines is in general greatly over-estimated.

226. The power developed by a complex harmonic wave in a non-inductive circuit is the sum of the powers of the individual harmonics. Thus if upon a sine wave of alternating E.M.F. higher harmonic waves are superposed, the effective E.M.F., and the power produced by this wave in a given circuit or with a given effective current, are increased. In consequence hereof alternators and synchronous motors of ironclad unitooth construction — that is, machines giving waves with pronounced higher harmonics — give with the same number of turns on the armature, and the same magnetic flux per field pole at the same frequency, a higher output than machines built to produce sine waves.

227. This explains an apparent paradox :

If in the three-phase star-connected generator with the magnetic field constructed as shown diagrammatically in Fig. 162, the magnetic flux per pole = M , the number of turns in series per circuit = n , the frequency = N , the E.M.F. between any two collector rings is :

$$E = \sqrt{2} \pi N 2 n \Phi 10^{-8}.$$

since $2n$ armature turns simultaneously interlink with the magnetic flux Φ .

The E.M.F. per armature circuit is :

$$e = \sqrt{2} \pi N n \Phi 10^{-8};$$

hence the E.M.F. between collector rings, as resultant of two E.M.Fs. e displaced by 60° from each other, is :

$$E = e \sqrt{3} = \sqrt{2} \pi N \sqrt{3} n \Phi 10^{-8};$$

while the same E.M.F. was found by direct calculation from number of turns, magnetic flux, and frequency to be equal to $2e$; that is the two values found for the same E.M.F. have the proportion $\sqrt{3} : 2 = 1 : 1.154$.

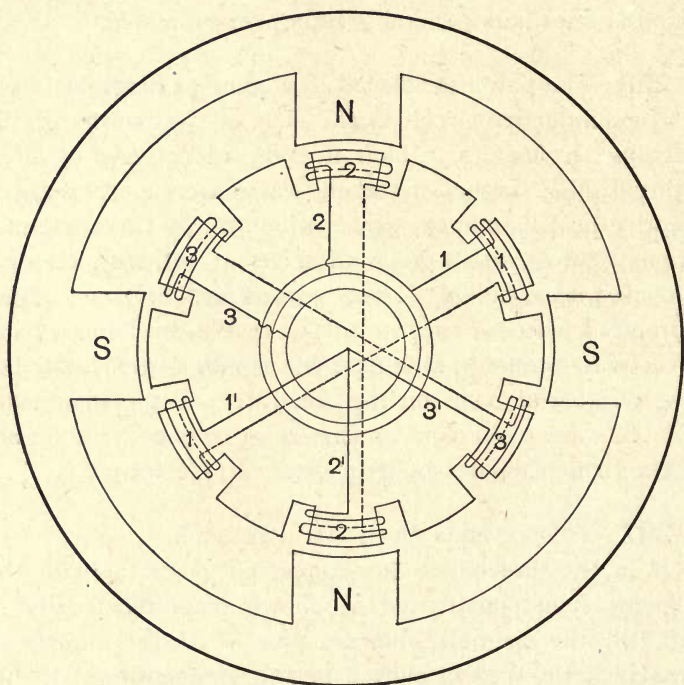


Fig. 162. Three-phase Star-connected Alternator.

This discrepancy is due to the existence of more pronounced higher harmonics in the wave e than in the wave $E = e \times \sqrt{3}$, which have been neglected in the formula :

$$e = \sqrt{2} \pi N n \Phi 10^{-8}.$$

Hence it follows that, while the E.M.F. between two collector rings in the machine shown diagrammatically in Fig. 162 is only $e \times \sqrt{3}$, by massing the same number of turns in one slot instead of in two slots, we get the E.M.F. $2e$ or 15.4 per cent higher E.M.F., that is, larger output.

It follows herefrom that the distorted E.M.F. wave of a unitooth alternator is produced by lesser magnetic flux per pole — that is, in general, at a lesser hysteretic loss in the armature or at higher efficiency — than the same effective E.M.F. would be produced with the same number of armature turns if the magnetic disposition were such as to produce a sine wave.

228. Inversely, if such a distorted wave of E.M.F. is impressed upon a magnetic circuit, as, for instance, a transformer, the wave of magnetism in the primary will repeat in shape the wave of magnetism interlinked with the armature coils of the alternator, and consequently, with a lesser maximum magnetic flux, the same effective counter E.M.F. will be produced, that is, the same power converted in the transformer. Since the hysteretic loss in the transformer depends upon the maximum value of magnetism, it follows that the hysteretic loss in a transformer is less with a distorted wave of a unitooth alternator than with a sine wave.

Thus with the distorted waves of unitooth machines, generators, transformers, and synchronous motors — and induction motors in so far as they are transformers — operate more efficiently.

229. From another side the same problem can be approached.

If upon a transformer a sine wave of E.M.F. is impressed, the wave of magnetism will be a sine wave also. If now upon the sine wave of E.M.F. higher harmonics, as sine waves of triple, quintuple, etc., frequency are superposed in such a way that the corresponding higher harmonic sine waves of magnetism do not increase the maximum value of magnetism, or even lower it by a coincidence of their negative maxima with the positive maximum of the fundamental, — in this case all the power represented by these higher harmonics of E.M.F. will be

transformed without an increase of the hysteretic loss, or even with a decreased hysteretic loss.

Obviously, if the maximum of the higher harmonic wave of magnetism coincides with the maximum of the fundamental, and thereby makes the wave of magnetism more pointed, the hysteretic loss will be increased more than in proportion to the increased power transformed, i.e., the efficiency of the transformer will be lowered.

That is : Some distorted waves of E.M.F. are transformed at a lesser, some at a larger, hysteretic loss than the sine wave, if the same effective E.M.F. is impressed upon the transformer.

The unitooth alternator wave belongs to the former class ; the waves derived from continuous-current machines, tapped at two equi-distant points of the armature, in general to the latter class.

230. Regarding the loss of energy by Foucault or eddy currents, this loss is not affected by distortion of wave shape, since the E.M.F. of eddy currents, as induced E.M.F., is proportional to the secondary E.M.F.; and thus at constant impressed primary E.M.F., the energy consumed by eddy currents bears a constant relation to the output of the secondary circuit, as obvious, since the division of power between the two secondary circuits — the eddy current circuit, and the useful or consumer circuit — is unaffected by wave-shape or intensity of magnetism.

231. In high potential lines, distorted waves whose maxima are very high above the effective values, as peaked waves, may be objectionable by increasing the strain on the insulation. It is, however, not settled yet beyond doubt whether the striking-distance of a rapidly alternating potential depends upon the maximum value or upon the effective value. Since disruptive phenomena do not

always take place immediately after application of the potential, but the time element plays an important part, it is possible that insulation-strain and striking-distance is, in a certain range, dependent upon the effective potential, and thus independent of the wave-shape.

In general, as conclusions may be derived that the importance of a proper wave-shape is generally greatly over-rated, but that in certain cases sine waves are desirable, in other cases certain distorted waves are preferable.

CHAPTER XXIII.

GENERAL POLYPHASE SYSTEMS.

232. A polyphase system is an alternating-current system in which several E.M.Fs. of the same frequency, but displaced in phase from each other, produce several currents of equal frequency, but displaced phases.

Thus any polyphase system can be considered as consisting of a number of single circuits, or branches of the polyphase system, which may be more or less interlinked with each other.

In general the investigation of a polyphase system is carried out by treating the single-phase branch circuits independently.

Thus all the discussions on generators, synchronous motors, induction motors, etc., in the preceding chapters, apply to single-phase systems as well as polyphase systems, in the latter case the total power being the sum of the powers of the individual or branch circuits.

If the polyphase system consists of n equal E.M.Fs. displaced from each other by $1/n$ of a period, the system is called a *symmetrical system*, otherwise an *unsymmetrical system*.

Thus the three-phase system, consisting of three equal E.M.Fs. displaced by one-third of a period, is a symmetrical system. The quarter-phase system, consisting of two equal E.M.Fs. displaced by 90° , or one-quarter of a period, is an unsymmetrical system.

233. The flow of power in a single-phase system is pulsating; that is, the watt curve of the circuit is a sine

wave of double frequency, alternating between a maximum value and zero, or a negative maximum value. In a poly-phase system the watt curves of the different branches of the system are pulsating also. Their sum, however, or the total flow of power of the system, may be either constant or pulsating. In the first case, the system is called a *balanced system*, in the latter case an *unbalanced system*.

The three-phase system and the quarter-phase system, with equal load on the different branches, are balanced systems; with unequal distribution of load between the individual branches both systems become unbalanced systems.

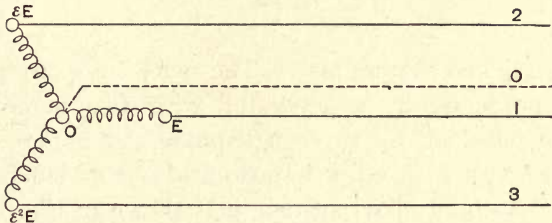


Fig. 163.

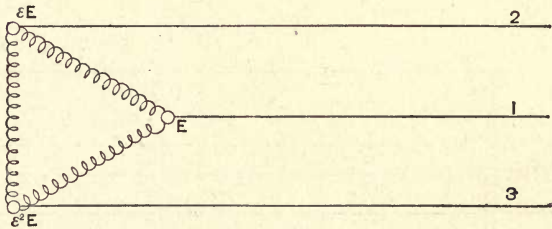


Fig. 164.

The different branches of a polyphase system may be either independent from each other, that is, without any electrical interconnection, or they may be interlinked with each other. In the first case, the polyphase system is called an *independent system*, in the latter case an *interlinked system*.

The three-phase system with star-connected or ring-connected generator, as shown diagrammatically in Figs. 163 and 164, is an interlinked system.

The four-phase system as derived by connecting four equidistant points of a continuous-current armature with four collector rings, as shown diagrammatically in Fig. 165,

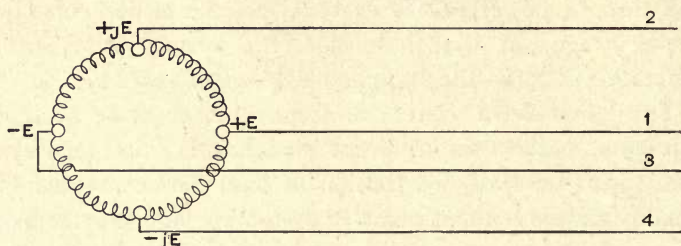


Fig. 165.

is an interlinked system also. The four-wire quarter-phase system produced by a generator with two independent armature coils, or by two single-phase generators rigidly connected with each other in quadrature, is an independent system. As interlinked system, it is shown in Fig. 166, as star-connected four-phase system.

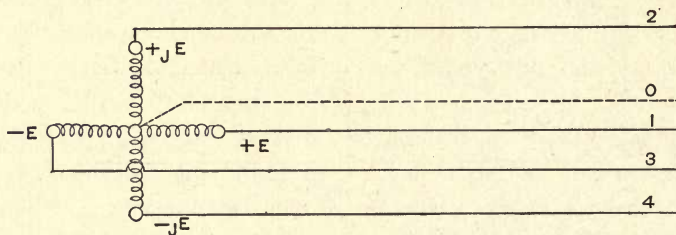


Fig. 166.

234. Thus, polyphase systems can be subdivided into:

Symmetrical systems and unsymmetrical systems.

Balanced systems and unbalanced systems.

Interlinked systems and independent systems.

The only polyphase systems which have found practical application are:

The three-phase system, consisting of three E.M.Fs. dis-

placed by one-third of a period, used exclusively as interlinked system.

The quarter-phase system, consisting of two E.M.Fs. in quadrature, and used with four wires, or with three wires, which may be either an interlinked system or an independent system.

CHAPTER XXIV.

SYMMETRICAL POLYPHASE SYSTEMS.

235. If all the E.M.Fs. of a polyphase system are equal in intensity, and differ from each other by the same angle of difference of phase, the system is called a symmetrical polyphase system.

Hence, a symmetrical n -phase system is a system of n E.M.Fs. of equal intensity, differing from each other in phase by $1/n$ of a period:

$$\begin{aligned} e_1 &= E \sin \beta; \\ e_2 &= E \sin \left(\beta - \frac{2\pi}{n} \right); \\ e_3 &= E \sin \left(\beta - \frac{4\pi}{n} \right); \\ &\vdots \\ e_n &= E \sin \left(\beta - \frac{2(n-1)\pi}{n} \right). \end{aligned}$$

The next E.M.F. is again:

$$e_1 = E \sin (\beta - 2\pi) = E \sin \beta.$$

In the polar diagram the n E.M.Fs. of the symmetrical n -phase system are represented by n equal vectors, following each other under equal angles.

Since in symbolic writing, rotation by $1/n$ of a period, or angle $2\pi/n$, is represented by multiplication with:

$$\cos \frac{2\pi}{n} + j \sin \frac{2\pi}{n} = \epsilon,$$

the E.M.Fs. of the symmetrical polyphase system are:

$$E;$$

$$\begin{aligned}
 E \left(\cos \frac{2\pi}{n} + j \sin \frac{2\pi}{n} \right) &= E \epsilon; \\
 E \left(\cos \frac{4\pi}{n} + j \sin \frac{4\pi}{n} \right) &= E \epsilon^2; \\
 \vdots & \\
 E \left(\cos \frac{2(n-1)\pi}{n} + j \sin \frac{2(n-1)\pi}{n} \right) &= E \epsilon^{n-1}.
 \end{aligned}$$

The next E.M.F. is again :

$$E (\cos 2\pi + j \sin 2\pi) = E \epsilon^n = E.$$

Hence, it is

$$\epsilon = \cos \frac{2\pi}{n} + j \sin \frac{2\pi}{n} = \sqrt[n]{1}.$$

Or in other words :

In a symmetrical n -phase system any E.M.F. of the system is expressed by :

$$\begin{aligned}
 &\epsilon^i E; \\
 \text{where :} &\quad \epsilon = \sqrt[n]{1}.
 \end{aligned}$$

236. Substituting now for n different values, we get the different symmetrical polyphase systems, represented by

$$\begin{aligned}
 &\epsilon^i E, \\
 \text{where,} &\quad \epsilon = \sqrt[n]{1} = \cos \frac{2\pi}{n} + j \sin \frac{2\pi}{n}.
 \end{aligned}$$

$$1.) \quad n = 1 \quad \epsilon = 1 \quad \epsilon^i E = E,$$

the ordinary single-phase system.

$$2.) \quad n = 2 \quad \epsilon = -1 \quad \epsilon^i E = E \text{ and } -E.$$

Since $-E$ is the return of E , $n = 2$ gives again the single-phase system.

$$3.) \quad n = 3 \quad \epsilon = \cos \frac{2\pi}{3} + j \sin \frac{2\pi}{3} = \frac{-1 + j\sqrt{3}}{2}$$

$$\epsilon^2 = \frac{-1 - j\sqrt{3}}{2}.$$

The three E.M.Fs. of the three-phase system are :

$$\epsilon^i E = E, \quad \frac{-1 + j\sqrt{3}}{2} E, \quad \frac{-1 - j\sqrt{3}}{2} E.$$

Consequently the three-phase system is the lowest symmetrical polyphase system.

$$4.) \quad n = 4, \quad \epsilon = \cos \frac{2\pi}{4} + j \sin \frac{2\pi}{4} = j, \quad \epsilon^2 = -1, \quad \epsilon^3 = -j.$$

The four E.M.Fs. of the four-phase system are :

$$\epsilon^i = E, \quad jE, \quad -E, \quad -jE.$$

They are in pairs opposite to each other :

$$E \text{ and } -E; \quad jE \text{ and } -jE.$$

Hence can be produced by two coils in quadrature with each other, analogous as the two-phase system, or ordinary alternating-current system, can be produced by one coil.

Thus the symmetrical quarter-phase system is a four-phase system.

Higher systems, as the quarter-phase or four-phase system, have not been used, and are of little practical interest.

237. A characteristic feature of the symmetrical n -phase system is that under certain conditions it can produce a M.M.F. of constant intensity.

If n equal magnetizing coils act upon a point under equal angular displacements in space, and are excited by the n E.M.Fs. of a symmetrical n -phase system, a M.M.F. of constant intensity is produced at this point, whose direction revolves synchronously with uniform velocity.

Let,

n' = number of turns of each magnetizing coil.

E = effective value of impressed E.M.F.

I = effective value of current.

Hence,

$\mathcal{F} = n'I =$ effective M.M.F. of one of the magnetizing coils.

Then the instantaneous value of the M.M.F. of the coil acting in the direction $2\pi i/n$ is:

$$\begin{aligned} f_i &= \mathfrak{F}\sqrt{2} \sin\left(\beta - \frac{2\pi i}{n}\right) \\ &= n' I \sqrt{2} \sin\left(\beta - \frac{2\pi i}{n}\right). \end{aligned}$$

The two rectangular components of this M.M.F. are:

$$\begin{aligned} f_i' &= f_i \cos \frac{2\pi i}{n} \\ &= n' I \sqrt{2} \cos \frac{2\pi i}{n} \sin\left(\beta - \frac{2\pi i}{n}\right) \end{aligned}$$

and

$$\begin{aligned} f_i'' &= f_i \sin \frac{2\pi i}{n} \\ &= n' I \sqrt{2} \sin \frac{2\pi i}{n} \sin\left(\beta - \frac{2\pi i}{n}\right). \end{aligned}$$

Hence the M.M.F. of this coil can be expressed by the symbolic formula:

$$f_i = n' I \sqrt{2} \sin\left(\beta - \frac{2\pi i}{n}\right) \left(\cos \frac{2\pi i}{n} + j \sin \frac{2\pi i}{n}\right).$$

Thus the total or resultant M.M.F. of the n coils displaced under the n equal angles is:

$$f = \sum_1^n f_i = n' I \sqrt{2} \sum_1^n \sin\left(\beta - \frac{2\pi i}{n}\right) \left(\cos \frac{2\pi i}{n} + j \sin \frac{2\pi i}{n}\right)$$

or, expanded:

$$\begin{aligned} f &= n' I \sqrt{2} \left\{ \sin \beta \sum_1^n \left(\cos^2 \frac{2\pi i}{n} + j \sin \frac{2\pi i}{n} \cos \frac{2\pi i}{n} \right) - \right. \\ &\quad \left. \cos \beta \sum_1^n \left(\sin \frac{2\pi i}{n} \cos \frac{2\pi i}{n} + j \sin^2 \frac{2\pi i}{n} \right) \right\}. \end{aligned}$$

It is, however:

$$\begin{aligned} \cos^2 \frac{2\pi i}{n} + j \sin \frac{2\pi i}{n} \cos \frac{2\pi i}{n} &= \frac{1}{2} \left(1 + \cos \frac{4\pi i}{n} + j \sin \frac{4\pi i}{n} \right) \\ &= \frac{1}{2} (1 + \epsilon^{2i}) \end{aligned}$$

$$\begin{aligned} \sin \frac{2\pi i}{n} \cos \frac{2\pi i}{n} + j \sin^2 \frac{2\pi i}{n} &= \frac{j}{2} \left(1 - \cos \frac{4\pi i}{n} - j \sin \frac{4\pi i}{n} \right) \\ &= \frac{1}{2} (1 - \epsilon^{2i}), \end{aligned}$$

and, since:

$$\sum_1^n \epsilon^{2i} = 0, \quad \sum_1^n \epsilon^{-2i} = 0,$$

as the sum of all the roots of $\sqrt[n]{1}$,

$$\text{it is,} \quad f = \frac{nn'I\sqrt{2}}{2} (\sin \beta + j \cos \beta).$$

or,

$$\begin{aligned} f &= \frac{nn'I}{\sqrt{2}} (\sin \beta + j \cos \beta) \\ &= \frac{n\mathfrak{F}}{\sqrt{2}} (\sin \beta + j \cos \beta); \end{aligned}$$

the symbolic expression of the M.M.F. produced by the n circuits of the symmetrical n -phase system, when exciting n equal magnetizing coils displaced in space under equal angles.

The absolute value of this M.M.F. is:

$$F = \frac{nn'I}{\sqrt{2}} = \frac{n\mathfrak{F}}{\sqrt{2}} = \frac{n\mathfrak{F}_{max}}{2}.$$

Hence constant and equal $n/\sqrt{2}$ times the effective M.M.F. of each coil or $n/2$ times the maximum M.M.F. of each coil.

The phase of the resultant M.M.F. at the time represented by the angle β is:

$$\tan \hat{\omega} = \cot \beta;$$

That is, the M.M.F. produced by a symmetrical n -phase system revolves with constant intensity:

$$F = \frac{n\mathfrak{F}}{\sqrt{2}};$$

and constant speed, in synchronism with the frequency of the system; and, if the reluctance of the magnetic circuit

is constant, the magnetism revolves with constant intensity and constant speed also, at the point acted upon symmetrically by the n M.M.Fs. of the n -phase system.

This is a characteristic feature of the symmetrical polyphase system.

238. In the three-phase system, $n = 3$, $F = 1.5 \mathcal{F}_{max}$ where \mathcal{F}_{max} is the maximum M.M.F. of each of the magnetizing coils.

In a symmetrical quarter-phase system, $n = 4$, $F = 2 \mathcal{F}_{max}$, where \mathcal{F}_{max} is the maximum M.M.F. of each of the four magnetizing coils, or, if only two coils are used, since the four-phase M.M.F. are opposite in phase by two, $F = \mathcal{F}_{max}$, where \mathcal{F}_{max} is the maximum M.M.F. of each of the two magnetizing coils of the quarter-phase system.

While the quarter-phase system, consisting of two E.M.Fs. displaced by one-quarter of a period, is by its nature an unsymmetrical system, it shares a number of features — as, for instance, the ability of producing a constant resultant M.M.F. — with the symmetrical system, and may be considered as one-half of a symmetrical four-phase system.

Such systems, of an even number of phases, consisting of one-half of a symmetrical system, are called hemisymmetrical systems.

CHAPTER XXV.

BALANCED AND UNBALANCED POLYPHASE SYSTEMS.

239. If an alternating E.M.F. :

$$e = E \sqrt{2} \sin \beta,$$

produces a current :

$$i = I \sqrt{2} \sin (\beta - \hat{\omega}),$$

where $\hat{\omega}$ is the angle of lag, the power is :

$$\begin{aligned} p &= ei = 2 EI \sin \beta \sin (\beta - \hat{\omega}) \\ &= EI (\cos \hat{\omega} - \sin (2\beta - \hat{\omega})), \end{aligned}$$

and the average value of power :

$$P = EI \cos \hat{\omega}.$$

Substituting this, the instantaneous value of power is found as :

$$p = P \left(1 - \frac{\sin (2\beta - \hat{\omega})}{\cos \hat{\omega}} \right).$$

Hence the power, or the flow of energy, in an ordinary single-phase alternating-current circuit is fluctuating, and varies with twice the frequency of E.M.F. and current, unlike the power of a continuous-current circuit, which is constant :

$$p = ei.$$

If the angle of lag $\hat{\omega} = 0$ it is :

$$p = P (1 - \sin 2\beta);$$

hence the flow of power varies between zero and $2P$, where P is the average flow of energy or the effective power of the circuit.

If the current lags or leads the E.M.F. by angle $\hat{\omega}$ the power varies between

$$P\left(1 - \frac{1}{\cos \hat{\omega}}\right); \quad \text{and} \quad P\left(1 + \frac{1}{\cos \hat{\omega}}\right);$$

that is, becomes negative for a certain part of each half-wave. That is, for a time during each half-wave, energy flows back into the generator, while during the other part of the half-wave the generator sends out energy, and the difference between both is the effective power of the circuit.

If $\hat{\omega} = 90^\circ$, it is:

$$p = EI \cos 2\beta;$$

that is, the effective power: $P = 0$, and the energy flows to and fro between generator and receiving circuit.

Under any circumstances, however, the flow of energy in the single-phase system is fluctuating at least between zero and a maximum value, frequently even reversing.

240. If in a polyphase system

e_1, e_2, e_3, \dots = instantaneous values of E.M.F.;

i_1, i_2, i_3, \dots = instantaneous values of current produced thereby;

the total flow of power in the system is:

$$p = e_1 i_1 + e_2 i_2 + e_3 i_3 + \dots$$

The average flow of power is:

$$P = E_1 I_1 \cos \hat{\omega}_1 + E_2 I_2 \cos \hat{\omega}_2 + \dots$$

The polyphase system is called a balanced system, if the flow of energy:

$$p = e_1 i_1 + e_2 i_2 + e_3 i_3 + \dots$$

is constant, and it is called an unbalanced system if the flow of energy varies periodically, as in the single-phase system; and the ratio of the minimum value to the maximum value of power is called the *balance factor of the system*.

Hence in a single-phase system on non-inductive circuit, that is, at no-phase displacement, the balance factor is zero; and it is negative in a single-phase system with lagging or leading current, and becomes = -1 , if the phase displacement is 90° — that is, the circuit is wattless.

241. Obviously, in a polyphase system the balance of the system is a function of the distribution of load between the different branch circuits.

A balanced system in particular is called a polyphase system, whose flow of energy is constant, if all the circuits are loaded equally with a load of the same character, that is, the same phase displacement.

242. All the symmetrical systems from the three-phase system upward are balanced systems. Many unsymmetrical systems are balanced systems also.

1.) Three-phase system :

Let

$$\begin{aligned} e_1 &= E \sqrt{2} \sin \beta, & \text{and } i_1 &= I \sqrt{2} \sin (\beta - \hat{\omega}); \\ e_2 &= E \sqrt{2} \sin (\beta - 120), & i_2 &= I \sqrt{2} \sin (\beta - \hat{\omega} - 120); \\ e_3 &= E \sqrt{2} \sin (\beta - 240), & i_3 &= I \sqrt{2} \sin (\beta - \hat{\omega} - 240); \end{aligned}$$

be the E.M.Fs. of a three-phase system, and the currents produced thereby.

Then the total flow of power is :

$$\begin{aligned} p &= 2 EI (\sin \beta \sin (\beta - \hat{\omega}) + \sin (\beta - 120) \sin (\beta - \hat{\omega} - 120) \\ &\quad + \sin (\beta - 240) \sin (\beta - \hat{\omega} - 240)) \\ &= 3 EI \cos \hat{\omega} = P, \text{ or constant.} \end{aligned}$$

Hence the symmetrical three-phase system is a balanced system.

2.) Quarter-phase system :

$$\begin{aligned} \text{Let } e_1 &= E \sqrt{2} \sin \beta, & i_1 &= I \sqrt{2} \sin (\beta - \hat{\omega}); \\ e_2 &= E \sqrt{2} \cos \beta, & i_2 &= I \sqrt{2} \cos (\beta - \hat{\omega}); \end{aligned}$$

be the E.M.Fs. of the quarter-phase system, and the currents produced thereby.

This is an unsymmetrical system, but the instantaneous flow of power is :

$$\begin{aligned} p &= 2 EI (\sin \beta \sin (\beta - \hat{\omega}) + \cos \beta \cos (\beta - \hat{\omega})) \\ &= 2 EI \cos \hat{\omega} = P, \text{ or constant.} \end{aligned}$$

Hence the quarter-phase system is an unsymmetrical balanced system.

3.) The symmetrical n -phase system, with equal load and equal phase displacement in all n branches, is a balanced system. For, let :

$$\begin{aligned} e_i &= E \sqrt{2} \sin \left(\beta - \frac{2 \pi i}{n} \right) = \text{E.M.F.}; \\ i_i &= I \sqrt{2} \sin \left(\beta - \hat{\omega} - \frac{2 \pi i}{n} \right) = \text{current} \end{aligned}$$

the instantaneous flow of power is :

$$\begin{aligned} p &= \sum_1^n e_i i_i \\ &= 2 EI \sum_1^n \sin \left(\beta - \frac{2 \pi i}{n} \right) \sin \left(\beta - \hat{\omega} - \frac{2 \pi i}{n} \right) \\ &= EI \left\{ \sum_1^n \cos \hat{\omega} - \sum_1^n \cos \left(2 \beta - \hat{\omega} - \frac{4 \pi i}{n} \right) \right\}; \end{aligned}$$

or

$$p = n EI = P, \text{ or constant.}$$

243. An unbalanced polyphase system is the so-called inverted three-phase system, derived from two branches of a three-phase system by transformation by means of two transformers, whose secondaries are connected in opposite direction with respect to their primaries. Such a system takes an intermediate position between the Edison three-wire system and the three-phase system. It shares with the latter the polyphase feature, and with the Edison three-

wire system the feature that the potential difference between the outside wires is higher than between middle wire and outside wire.

By such a pair of transformers the two primary E.M.Fs. of 120° displacement of phase are transformed into two secondary E.M.Fs. differing from each other by 60° . Thus in the secondary circuit the difference of potential between the outside wires is $\sqrt{3}$ times the difference of potential between middle wire and outside wire. At equal load on the two branches, the three currents are equal, and differ from each other by 120° , that is, have the same relative proportion as in a three-phase system. If the load on one branch is maintained constant, while the load of the other branch is reduced from equality with that in the first branch down to zero, the current in the middle wire first decreases, reaches a minimum value of 87 per cent of its original value, and then increases again, reaching at no load the same value as at full load.

The balance factor of the inverted three-phase system on non-inductive load is .333.

244. In Figs. 167 to 174 are shown the E.M.Fs. as e and currents as i in drawn lines, and the power as p in dotted lines, for :

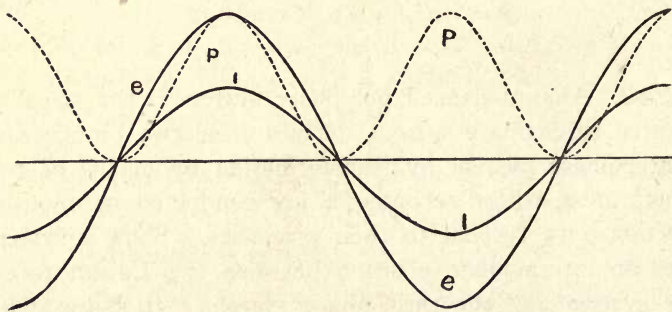


Fig. 167. Single-phase System on Non-inductive Load.

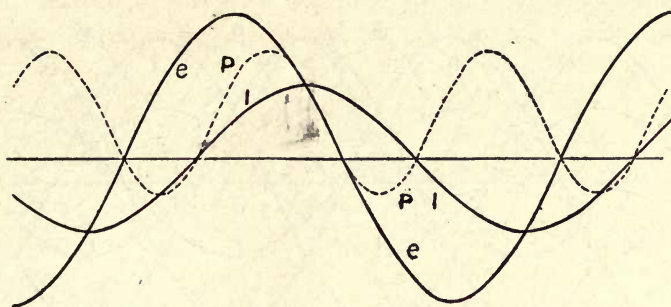


Fig. 168. Single-phase System on Inductive Load of 60° Lag.

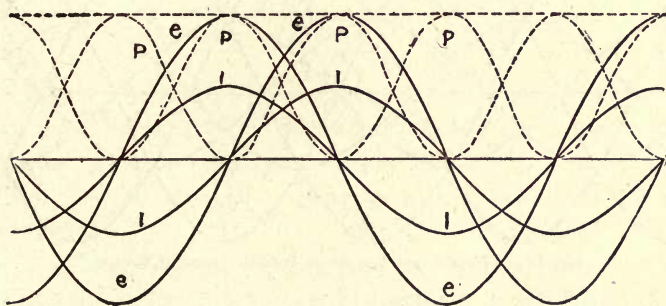


Fig. 169. Quarter-phase System on Non-inductive Load.

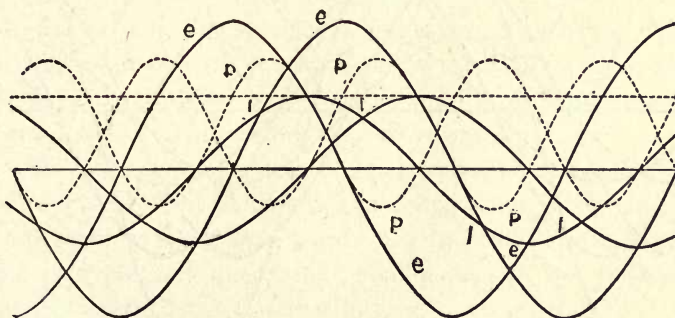


Fig. 170. Quarter-phase System on Inductive Load of 60° Lag.

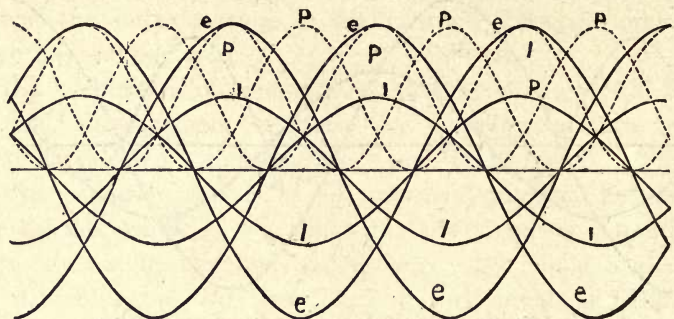


Fig. 171. Three-phase System on Non-inductive Load.

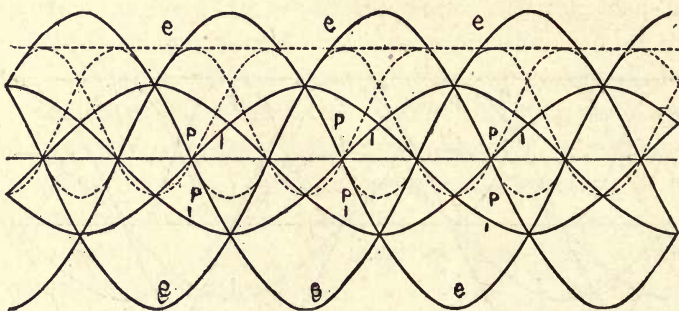


Fig. 172. Three-phase System on Inductive Load of 60° Lag.

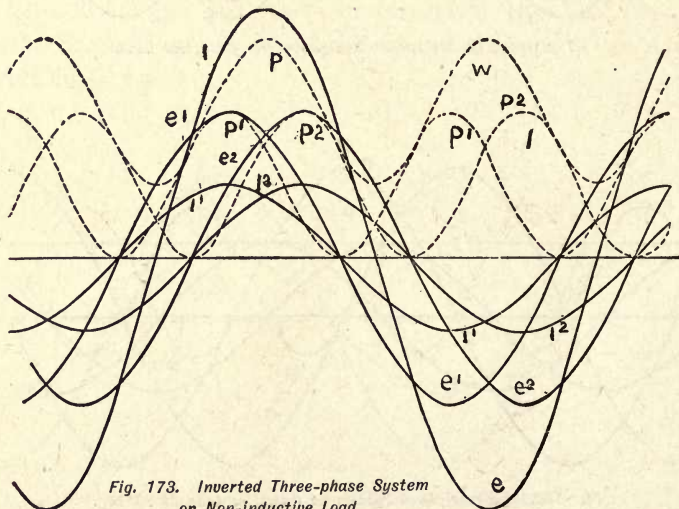


Fig. 173. Inverted Three-phase System on Non-inductive Load.

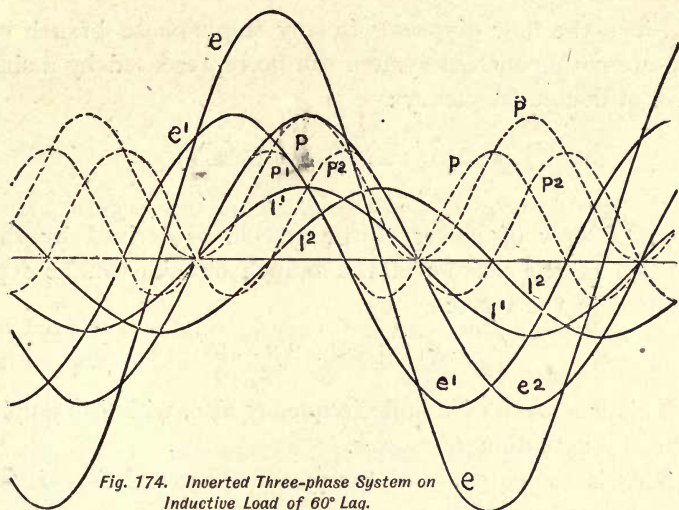


Fig. 174. Inverted Three-phase System on Inductive Load of 60° Lag.

245. The flow of power in an alternating-current system is a most important and characteristic feature of the system, and by its nature the systems may be classified into :

Monocyclic systems, or systems with a balance factor zero or negative.

Polycyclic systems, with a positive balance factor.

Balance factor -1 corresponds to a wattless circuit, balance factor zero to a non-inductive single-phase circuit, balance factor $+1$ to a balanced polyphase system.

246. In polar coördinates, the flow of power of an alternating-current system is represented by using the instantaneous flow of power as radius vector, with the angle β corresponding to the time as amplitude, one complete period being represented by one revolution.

In this way the power of an alternating-current system is represented by a closed symmetrical curve, having the zero point as quadruple point. In the monocyclic systems the zero point is quadruple nodal point ; in the polycyclic system quadruple isolated point.

Thus these curves are sextics,

Since the flow of power in any single-phase branch of the alternating-current system can be represented by a sine wave of double frequency :

$$p = P \left(1 - \frac{\sin (2\beta - \hat{\omega})}{\cos \hat{\omega}} \right).$$

the total flow of power of the system as derived by the addition of the powers of the branch circuits can be represented in the form :

$$p = P(1 + \epsilon \sin (2\beta - \hat{\omega}))$$

This is a wave of double frequency also, with ϵ as amplitude of fluctuation of power.

This is the equation of the power characteristics of the system in polar coördinates.

247. To derive the equation in rectangular coördinates we introduce a substitution which revolves the system of coördinates by an angle $\hat{\omega}/2$, so as to make the symmetry axes of the power characteristic of the coördinate axes.

$$p = \sqrt{x^2 + y^2},$$

$$\tan \left(\beta - \frac{\hat{\omega}}{2} \right) = \frac{y}{x}.$$

hence, $\sin (2\beta - \hat{\omega}) = 2 \sin \left(\beta - \frac{\hat{\omega}}{2} \right) \cos \left[\beta - \frac{\hat{\omega}}{2} \right] = \frac{2xy}{x^2 + y^2},$

substituted,

$$\sqrt{x^2 + y^2} = P \left\{ 1 + \frac{2\epsilon xy}{x^2 + y^2} \right\},$$

or, expanded :

$$(x^2 + y^2)^3 - P^2 (x^2 + y^2 + 2\epsilon xy)^2 = 0,$$

the sextic equation of the power characteristic.

Introducing :

$$a = (1 + \epsilon) P = \text{maximum value of power,}$$

$$b = (1 - \epsilon) P = \text{minimum value of power;}$$

it is
$$P = \frac{a + b}{2},$$

$$\epsilon = \frac{a - b}{a + b};$$

hence, substituted, and expanded :

$$(x^2 + y^2)^3 - \frac{1}{4} \{a(x + y)^2 + b(x - y)^2\}^2,$$

the equation of the power characteristic, with the *main power axes* a and b , and the balance factor: b/a .

It is thus :

Single-phase non-inductive circuit : $p = P(1 + \sin 2\phi)$,
 $b = 0$, $a = 2P$ —

$$(x^2 + y^2)^3 - P^2 + (x + y)^4 = 0, \quad b/a = 0.$$

Single-phase circuit, 60° lag : $p = P(1 + 2\sin 2\phi)$, $b = -P$, $a = +3P$

$$(x^2 + y^2)^3 - P^2(x^2 + y^2 + 4xy)^2 = 0, \quad b/a = -\frac{1}{3}.$$

Single-phase circuit, 90° lag : $p = EI \sin 2\phi$, $b = -EI$,
 $a = +EI$ —

$$(x^2 + y^2)^3 - (EI)^3(x^2 - y^2)^2, \quad b/a = -1.$$

Three-phase non-inductive circuit : $p = P$, $b = 1$, $a = 1$

$$x^2 + y^2 - P^2 = 0 : \text{circle. } b/a = +1.$$

Three-phase circuit, 60° lag : $p = P$, $b = 1$, $a = 1$

$$x^2 + y^2 - P^2 = 0 : \text{circle. } b/a = +1.$$

Quarter-phase non-inductive circuit : $p = P$, $b = 1$, $a = 1$

$$x^2 + y^2 - P^2 = 0 : \text{circle. } b/a = +1.$$

Quarter-phase circuit, 60° lag : $p = P$, $b = 1$, $a = 1$

$$x^2 + y^2 - P^2 = 0 : \text{circle. } b/a = +1.$$

Inverted three-phase non-inductive circuit :

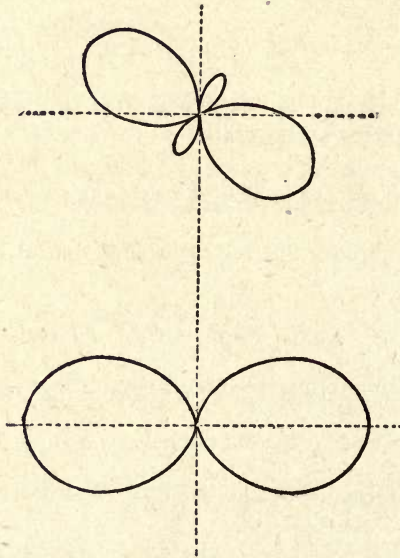
$$p = P \left(\frac{1 + \sin 2\phi}{2} \right), \quad b = \frac{1}{2} P, \quad a = \frac{3}{2} P$$

$$(x^2 + y^2)^3 - P^2 (x^2 + y^2 + xy)^2 = 0. \quad b/a = +\frac{1}{3}.$$

Inverted three-phase circuit 60° lag : $p = P(1 + \sin 2\phi)$,
 $b = 0, \quad a = 2P$

$$(x^2 + y^2)^3 - P^2 (x + y)^4 = 0. \quad b/a = 0.$$

a and b are called the main power axes of the alternating-current system, and the ratio b/a is the balance factor of the system.

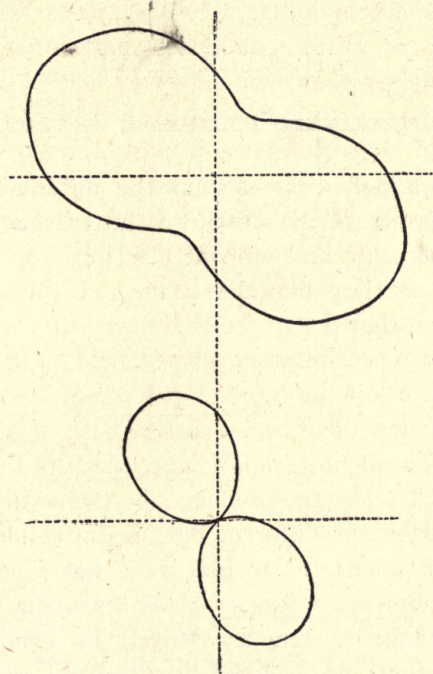


Figs. 175 and 176.

248. As seen, the flow of power of an alternating-current system is completely characterized by its two main power axes a and b .

The power characteristics in polar coördinates, corre-

sponding to the Figs. 167, 168, 173, and 174 are shown in Figs. 175, 176, 177, and 178.



Figs. 177 and 178.

The balanced quarter-phase and three-phase systems give as polar characteristics concentric circles.

CHAPTER XXVI.

INTERLINKED POLYPHASE SYSTEMS.

249. In a polyphase system the different circuits of displaced phases, which constitute the system, may either be entirely separate and without electrical connection with each other, or they may be connected with each other electrically, so that a part of the electrical conductors are in common to the different phases, and in this case the system is called an interlinked polyphase system.

Thus, for instance, the quarter-phase system will be called an independent system if the two E.M.Fs. in quadrature with each other are produced by two entirely separate coils of the same, or different but rigidly connected, armatures, and are connected to four wires which energize independent circuits in motors or other receiving devices. If the quarter-phase system is derived by connecting four equidistant points of a closed-circuit drum or ring-wound armature to the four collector rings, the system is an interlinked quarter-phase system.

Similarly in a three-phase system. Since each of the three currents which differ from each other by one-third of a period is equal to the resultant of the other two currents, it can be considered as the return circuit of the other two currents, and an interlinked three-phase system thus consists of three wires conveying currents differing by one-third of a period from each other, so that each of the three currents is a common return of the other two, and inversely.

250. In an interlinked polyphase system two ways exist of connecting apparatus into the system.

1st. The *star connection*, represented diagrammatically in Fig. 179. In this connection the n circuits excited by currents differ from each other by $1/n$ of a period, and are connected with their one end together into a neutral point or common connection, which may either be grounded or connected with other corresponding neutral points, or insulated.

In a three-phase system this connection is usually called a Y connection, from a similarity of its diagrammatical representation with the letter Y, as shown in Fig. 163.

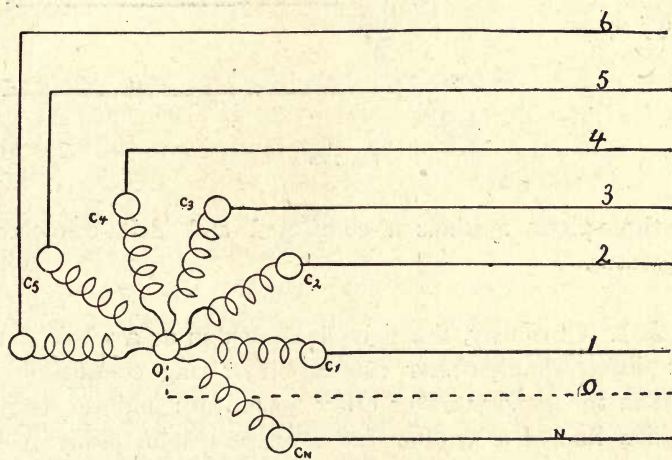


Fig. 179

2d. The *ring connection*, represented diagrammatically in Fig. 180, where the n circuits of the apparatus are connected with each other in closed circuit, and the corners or points of connection of adjacent circuits connected to the n lines of the polyphase system. In a three-phase system this connection is called the delta connection, from the similarity of its diagrammatic representation with the Greek letter Delta, as shown in Fig. 164.

In consequence hereof we distinguish between star-connected and ring-connected generators, motors, etc., or

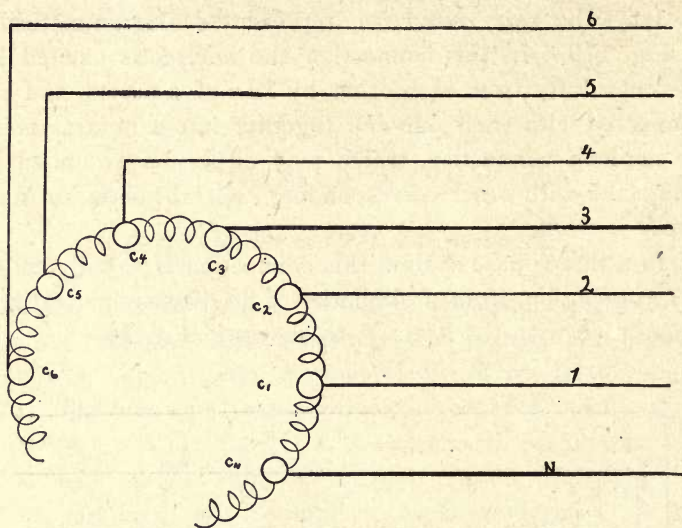


Fig. 180.

in three-phase systems Y-connected and delta-connected apparatus.

251. Obviously, the polyphase system as a whole does not differ, whether star connection or ring connection is used in the generators or other apparatus; and the transmission line of a symmetrical n -phase system always consists of n wires carrying current of equal strength, when balanced, differing from each other in phase by $1/n$ of a period. Since the line wires radiate from the n terminals of the generator, the lines can be considered as being in star connection.

The circuits of all the apparatus, generators, motors, etc., can either be connected in star connection, that is, between one line and a neutral point, or in ring connection, that is, between two lines.

In general some of the apparatus will be arranged in star connection, some in ring connection, as the occasion may require.

252. In the same way as we speak of star connection and ring connection of the circuits of the apparatus, the term star potential and ring potential, star current and ring current, etc., are used, whereby as star potential or in a three-phase circuit Y potential, the potential difference between one of the lines and the neutral point, that is, a point having the same difference of potential against all the lines, is understood; that is, the potential as measured by a voltmeter connected into star or Y connection. By ring or delta potential is understood the difference of potential between adjacent lines, as measured by a voltmeter connected between adjacent lines, in ring or delta connection.

In the same way the star or Y current is the current flowing from one line to a neutral point; the ring or delta current, the current flowing from one line to the other.

The current in the transmission line is always the star or Y current, and the potential difference between the line wires, the ring or delta potential.

Since the star potential and the ring potential differ from each other, apparatus requiring different voltages can be connected into the same polyphase mains, by using either star or ring connection. The total power of the polyphase system is equal to the sum of all the star or Y powers, or to the sum of all the ring or delta powers.

253. If in a generator with star-connected circuits, the E.M.F. per circuit = E , and the common connection or neutral point is denoted by zero, the potentials of the n terminals are :

$$E, \epsilon E, \epsilon^2 E \dots \epsilon^{n-1} E;$$

or in general : $\epsilon^i E$,

at the i^{th} terminal, where :

$$i = 0, 1, 2 \dots n - 1, \quad \epsilon = \cos \frac{2\pi}{n} + j \sin \frac{2\pi}{n} = \sqrt[n]{1}.$$

Hence the E.M.F. in the circuit from the i^{th} to the k^{th} terminal is :

$$E_{ki} = \epsilon^k E - \epsilon^i E = (\epsilon^k - \epsilon^i) E.$$

The E.M.F. between adjacent terminals i and $i + 1$ is :

$$(\epsilon^{i+1} - \epsilon^i) E = \epsilon^i (\epsilon - 1) E.$$

In a generator with ring-connected circuits, the E.M.F. per circuit :

$$\epsilon^i E$$

is the ring E.M.F., and takes the place of

$$\epsilon^i (\epsilon - 1) E;$$

while the E.M.F. between terminal and neutral point, or the star E.M.F., is :

$$\frac{\epsilon^i}{\epsilon - 1} E.$$

Hence in a star-connected generator with the E.M.F. E per circuit, it is :

Star E.M.F., $\epsilon^i E$.

Ring E.M.F., $\epsilon^i (\epsilon - 1) E$.

E.M.F. between terminal i and terminal k $(\epsilon^k - \epsilon^i) E$.

In a ring-connected generator with the E.M.F. E per circuit, it is :

Star E.M.F., $\frac{\epsilon^i}{\epsilon - 1} E$.

Ring E.M.F., $\epsilon^i E$.

E.M.F. between terminals i and k , $\frac{\epsilon^k - \epsilon^i}{\epsilon - 1} E$.

In a star-connected apparatus, the E.M.F. and the current per circuit have to be the star E.M.F. and the star current. In a ring-connected apparatus the E.M.F. and current per circuit have to be the ring E.M.F. and ring current.

In the generator of a symmetrical polyphase system, if :
 $\epsilon^i E$ are the E.M.Fs. between the n terminals and the neutral point, or star E.M.Fs.,

I_i = the currents issuing from terminal i over a line of the impedance Z_i (including generator impedance in star connection), we have :

Potential at end of line i :

$$\epsilon^i E - Z_i I_i.$$

Difference of potential between terminals k and i :

$$(\epsilon^k - \epsilon^i) E - (Z_k I_k - Z_i I_i),$$

where I_i is the star current of the system, Z_i the star impedance.

The ring potential at the end of the line between terminals i and k is E_{ik} , and it is :

$$E_{ik} = - E_{ki}.$$

If now I_{ik} denotes the current passing from terminal i to terminal k , and Z_{ik} impedance of the circuit between terminal i and terminal k , where :

$$I_{ik} = - I_{ki},$$

$$Z_{ik} = Z_{ki},$$

it is

$$E_{ik} = Z_{ik} I_{ik}.$$

If I_{io} denotes the current passing from terminal i to a ground or neutral point, and Z_{io} is the impedance of this circuit between terminal i and neutral point, it is :

$$E_{io} = \epsilon^i E - Z_i I_i = Z_{io} I_{io}.$$

254. We have thus, by Ohm's law and Kirchhoff's law :

If $\epsilon^i E$ is the E.M.F. per circuit of the generator, between the terminal i and the neutral point of the generator, or the star E.M.F.

I_i = the current issuing from the terminal i of the generator, or the star current.

Z_i = the impedance of the line connected to a terminal i of the generator, including generator impedance.

E_i = the E.M.F. at the end of line connected to a terminal i of the generator.

E_{ik} = the difference of potential between the ends of the lines i and k .

I_{ik} = the current passing from line i to line k .

Z_{ik} = the impedance of the circuit between lines i and k .

$I_{io}, I_{i00} \dots$ = the current passing from line i to neutral points 0, 00, \dots

$Z_{io}, Z_{i00} \dots$ = the impedance of the circuits between line i and neutral points 0, 00, \dots

It is then :

$$1.) \quad E_{ik} = -E_{ki}, \quad I_{ik} = -I_{ki}, \quad Z_{ik} = Z_{ki}, \quad I_{io} = -I_{oi}, \\ Z_{io} = Z_{oi}, \text{ etc.}$$

$$2.) \quad E_i = \epsilon^i E - Z_i I_i.$$

$$3.) \quad E_i = Z_{io} I_{io} = Z_{i00} I_{i00} = \dots$$

$$4.) \quad E_{ik} = E_k - E_i = (\epsilon^k - \epsilon^i) E - (Z_k I_k - Z_i I_i).$$

$$5.) \quad E_{ik} = Z_{ik} I_{ik}.$$

$$6.) \quad I_i = \sum_0^k I_{ik}.$$

7.) If the neutral point of the generator does not exist, as in ring connection, or is insulated from the other neutral points :

$$\sum_1^n I_i = 0;$$

$$\sum_1^n I_{io} = 0;$$

$$\sum_1^n I_{i00} = 0, \text{ etc.}$$

Where 0, 00, etc., are the different neutral points which are insulated from each other.

If the neutral point of the generator and all the other neutral points are grounded or connected with each other, it is :

$$\sum_1^n I_i = \sum_1^n (I_{io} + I_{i00} + \dots) \\ = \sum_1^n I_{io} + \sum_1^n I_{i00} + \dots$$

If the neutral point of the generator and all other neutral points are grounded, the system is called a grounded system. If the neutral points are not grounded, the system is an insulated polyphase system, and an insulated polyphase system with equalizing return, if all the neutral points are connected with each other.

8.) The power of the polyphase system is —

$$P = \sum_1^n \epsilon^i E I_i \cos \phi_i \text{ at the generator}$$

$$P = \sum_0^n \sum_i^n \frac{n}{i} E_{ik} I_{ik} \cos \phi_{ik} \text{ in the receiving circuits.}$$

CHAPTER XXVII.

TRANSFORMATION OF POLYPHASE SYSTEMS.

255. In transforming a polyphase system into another polyphase system, it is obvious that the primary system must have the same flow of power as the secondary system, neglecting losses in transformation, and that consequently a balanced system will be transformed again in a balanced system, and an unbalanced system into an unbalanced system of the same balance factor, since the transformer is an apparatus not able to store energy, and thereby to change the nature of the flow of power. The energy stored as magnetism, amounts in a well-designed transformer only to a very small percentage of the total energy. This shows the futility of producing symmetrical balanced polyphase systems by transformation from the unbalanced single-phase system without additional apparatus able to store energy efficiently, as revolving machinery.

Since any E.M.F. can be resolved into, or produced by, two components of given directions, the E.M.Fs. of any polyphase system can be resolved into components or produced from components of two given directions. This enables the transformation of any polyphase system into any other polyphase system of the same balance factor by two transformers only.

256. Let $E_1, E_2, E_3 \dots$ be the E.M.Fs. of the primary system which shall be transformed into —

$E'_1, E'_2, E'_3 \dots$ the E.M.Fs. of the secondary system.

Choosing two magnetic fluxes, $\bar{\phi}$ and $\bar{\phi}'$, of different

phases, as magnetic circuits of the two transformers, which induce the E.M.Fs., \bar{e} and \bar{e} , per turn, by the law of parallelogram the E.M.Fs., E_1, E_2, \dots can be dissolved into two components, \bar{E}_1 and \bar{E}_1, \bar{E}_2 and \bar{E}_2, \dots of the phases, \bar{e} and \bar{e} .

Then, —

$\bar{E}_1, \bar{E}_2, \dots$ are the counter E.M.Fs. which have to be induced in the primary polyphase circuits of the first transformer;

hence

$\bar{E}_1/\bar{e}, \bar{E}_2/\bar{e} \dots$ are the numbers of turns of the primary coils of the first transformer.

Analogously

$\bar{E}_1/\bar{e}, \bar{E}_2/\bar{e} \dots$ are the number of turns of the primary coils in the second transformer.

In the same manner as the E.M.Fs. of the primary system have been resolved into components in phase with \bar{e} and \bar{e} , the E.M.Fs. of the secondary system, E_1^1, E_2^1, \dots are produced from components, \bar{E}_1^1 and \bar{E}_1^1, \bar{E}_2^1 and \bar{E}_2^1, \dots in phase with \bar{e} and \bar{e} , and give as numbers of secondary turns, —

$\bar{E}_1^1/\bar{e}, \bar{E}_2^1/\bar{e}, \dots$ in the first transformer;

$\bar{E}_1^1/\bar{e}, \bar{E}_2^1/\bar{e}, \dots$ in the second transformer.

That means each of the two transformers \bar{m} and \bar{m} contains in general primary turns of each of the primary phases, and secondary turns of each of the secondary phases. Loading now the secondary polyphase system in any desired manner, corresponding to the secondary currents, primary currents will flow in such a manner that the total flow of power in the primary polyphase system is the same as the total flow of power in the secondary system, plus the loss of power in the transformers.

257. As an instance may be considered the transformation of the symmetrical balanced three-phase system

$$E \sin \beta, \quad E \sin (\beta - 120), \quad E \sin (\beta - 240),$$

in an unsymmetrical balanced quarter-phase system :

$$E' \sin \beta, \quad E' \sin (\beta - 90).$$

Let the magnetic flux of the two transformers be

$$\phi \cos \beta \quad \text{and} \quad \phi \cos (\beta - 90).$$

Then the E.M.Fs. induced per turn in the transformers are

$$e \sin \beta \quad \text{and} \quad e \sin (\beta - 90);$$

hence, in the primary circuit the first phase, $E \sin \beta$, will give, in the first transformer, E/e primary turns; in the second transformer, 0 primary turns.

The second phase, $E \sin (\beta - 120)$, will give, in the first transformer, $-E/2e$ primary turns; in the second transformer, $\frac{E \times \sqrt{3}}{2e}$ primary turns.

The third phase, $E \sin (\beta - 240)$, will give, in the first transformer, $-E/2e$ primary turns; in the second transformer, $\frac{-E \times \sqrt{3}}{2e}$ primary turns.

In the secondary circuit the first phase $E' \sin \beta$ will give in the first transformer: E'/e secondary turns; in the second transformer: 0 secondary turns.

The second phase: $E' \sin (\beta - 90)$ will give in the first transformer: 0 secondary turns; in the second transformer, E'/e secondary turns.

Or, if :

$$E = 5,000 \quad E' = 100, \quad e = 10.$$

	PRIMARY.			SECONDARY.		Phase.
	1st.	2d.	3d.	1st.	2d.	
first transformer	+ 500	- 250	- 250	10	0	
second transformer	0	+ 433	- 433	0	10	turns.

That means :

Any balanced polyphase system can be transformed by two transformers only, without storage of energy, into any other balanced polyphase system.

258. Transformation with a change of the balance factor of the system is possible only by means of apparatus able to store energy, since the difference of power between primary and secondary circuit has to be stored at the time when the secondary power is below the primary, and returned during the time when the primary power is below the secondary. The most efficient storing device of electric energy is mechanical momentum in revolving machinery. It has, however, the disadvantage of requiring attendance.

CHAPTER XXVIII.

COPPER EFFICIENCY OF SYSTEMS.

259. In electric power transmission and distribution, wherever the place of consumption of the electric energy is distant from the place of production, the conductors which transfer the current are a sufficiently large item to require consideration, when deciding which system and what potential is to be used.

In general, in transmitting a given amount of power at a given loss over a given distance, other things being equal, the amount of copper required in the conductors is inversely proportional to the square of the potential used. Since the total power transmitted is proportional to the product of current and E.M.F., at a given power, the current will vary inversely proportional to the E.M.F., and therefore, since the loss is proportional to the product of current-square and resistance, to give the same loss the resistance must vary inversely proportional to the square of the current, that is, proportional to the square of the E.M.F.; and since the amount of copper is inversely proportional to the resistance, other things being equal, the amount of copper varies inversely proportional to the square of the E.M.F. used.

This holds for any system.

Comparing now the different systems, as two-wire single-phase, single-phase three-wire, three-phase and quarter-phase, as basis of comparison equality of the potential is used.

Some systems, however, as for instance, the Edison three-wire system, or the inverted three-phase system, have

different potentials in the different circuits constituting the system, and thus the comparison can be made either —

1st. On the basis of equality of the maximum potential difference in the system; or

2d. On the basis of the minimum potential difference in the system, or the potential difference per circuit or phase of the system.

In low potential circuits, as secondary networks, where the potential is not limited by the insulation strain, but by the potential of the apparatus connected into the system, as incandescent lamps, the proper basis of comparison is equality of the potential per branch of the system, or per phase.

On the other hand, in long distance transmissions where the potential is not restricted by any consideration of apparatus suitable for a certain maximum potential only, but where the limitation of potential depends upon the problem of insulating the conductors against disruptive discharge, the proper comparison is on the basis of equality of the maximum difference of potential in the system; that is, equal maximum dielectric strain on the insulation.

The same consideration holds in moderate potential power circuits, in considering the danger to life from wires or high differences of potential.

Thus the comparison of different systems of long-distance transmission at high potential or power distribution for motors is to be made on the basis of equality of the maximum difference of potential existing in the system. The comparison of low potential distribution circuits for lighting on the basis of equality of the minimum difference of potential between any pair of wires connected to the receiving apparatus.

260. 1st. *Comparison on the basis of equality of the minimum difference of potential, in low potential lighting circuits:*

In the single-phase alternating-current circuit, if $e =$ E.M.F., $i =$ current, $r =$ resistance per line, the total power is $= ei$, the loss of power $2i^2r$.

Using, however, a three-wire system, the potential between outside wires and neutral being given $= e$, the potential between the outside wires is $= 2e$, that is, the distribution takes place at twice the potential, or only $\frac{1}{4}$ the copper is needed to transmit the same power at the same loss, if, as it is theoretically possible, the neutral wire has no cross-section. If therefore the neutral wire is made of the same cross-section with each of the outside wires, $\frac{3}{8}$ of the copper of the single-phase system is needed; if the neutral wire is $\frac{1}{2}$ the cross-section of each of the outside wires, $\frac{5}{16}$ of the copper is needed. Obviously, a single-phase five-wire system will be a system of distribution at the potential $4e$, and therefore require only $\frac{1}{16}$ of the copper of the single-phase system in the outside wires; and if each of the three neutral wires is of $\frac{1}{2}$ the cross-section of the outside wires, $\frac{7}{16} = 10.93$ per cent of the copper of a single-phase system.

Coming now to the three-phase system with the potential e between the lines as delta potential, if $i =$ the current per line or Y current, the current from line to line or delta current $= i_1 / \sqrt{3}$; and since three branches are used, the total power is $3ei_1 / \sqrt{3} = ei_1\sqrt{3}$. Hence if the same power has to be transmitted by the three-phase system as with the single-phase system, the three-phase line current must be $i_1 = i / \sqrt{3}$; hence if $r_1 =$ resistance of each of the three wires, the loss per wire is $i_1^2 r_1 = i^2 r_1 / 3$, and the total loss is $i^2 r_1$, while in the single-phase system it is $2i^2 r$. Hence, to get the same loss, it must be: $r_1 \leq r$, that is, each of the three three-phase lines has twice the resistance—that is, half the copper of each of the two single-phase lines; or in other words, the three-phase system requires three-fourths of the copper of the single-phase system of the same potential.

Introducing, however, a fourth neutral wire into the three-phase system, and connecting the lamps between the neutral wire and the three outside wires — that is, in Y connection — the potential between the outside wires or delta potential will be $= e \times \sqrt{3}$, since the Y potential $= e$; and the potential of the system is raised thereby from e to $e \sqrt{3}$; that is, only $\frac{1}{3}$ as much copper is required in the outside wires as before — that is $\frac{1}{4}$ as much copper as in the single-phase two-wire system. Making the neutral of the same cross-section as the outside wires, requires $\frac{1}{3}$ more copper, or $\frac{1}{3} = 33.3$ per cent of the copper of the single-phase system; making the neutral of half cross-section, requires $\frac{1}{4}$ more, or $\frac{3}{4} = 29.17$ per cent of the copper of the single-phase system. The system, however, now is a four-wire system.

The independent quarter-phase system with four wires is identical in efficiency to the two-wire single-phase system, since it is nothing but two independent single-phase systems in quadrature.

The four-wire quarter-phase system can be used as two independent Edison three-wire systems also, deriving therefrom the same saving by doubling the potential between the outside wires, and has in this case the advantage, that by interlinkage, the same neutral wire can be used for both phases, and thus one of the neutral wires saved.

In this case the quarter-phase system with common neutral of full cross-section requires $\frac{5}{8} = 31.25$ per cent, the quarter-phase system with common neutral of one-half cross-section requires $\frac{3}{4} = 28.125$ per cent, of the copper of the two-wire single-phase system.

In this case, however, the system is a five-wire system, and as such far inferior to the five-wire single-phase system.

Coming now to the quarter-phase system with common return and potential e per branch, denoting the current in the outside wires by i_2 , the current in the central wire is $i_2 \sqrt{2}$; and if the same current density is chosen for all

three wires, as the condition of maximum efficiency, and the resistance of each outside wire denoted by r_2 , the resistance of the central wire = $r_2/\sqrt{2}$, and the loss of power per outside wire is $i_2^2 r_2$, in the central wire $2 i_2^2 r_2 / \sqrt{2} = i_2^2 r_2 \sqrt{2}$; hence the total loss of power is $2 i_2^2 r_2 + i_2^2 r_2 \sqrt{2} = i_2^2 r_2 (2 + \sqrt{2})$. The power transmitted per branch is $i_2 e$, hence the total power $2 i_2 e$. To transmit the same power as by a single-phase system of power, $e i$, it must be $i_2 = i/2$; hence the loss, $\frac{i^2 r_2 (2 + \sqrt{2})}{4}$. Since this

loss shall be the same as the loss $2 i^2 r$ in the single-phase system, it must be $2 r = \frac{(2 + \sqrt{2})}{4}$, or $r_2 = \frac{8 r}{2 + \sqrt{2}}$.

Therefore each of the outside wires must be $\frac{2 + \sqrt{2}}{8}$ times as large as each single-phase wire, the central wire $\sqrt{2}$ times larger; hence the copper required for the quarter-phase system with common return bears to the copper required for the single-phase system the relation :

$$\frac{2(2 + \sqrt{2})}{8} + \frac{(2 + \sqrt{2})\sqrt{2}}{8} \div 2, \text{ or, } \frac{3 + 2\sqrt{2}}{8} \div 1, = 72.9$$

per cent of the copper of the single-phase system.

Hence the quarter-phase system with common return saves 2 per cent more copper than the three-phase system, but is inferior to the single-phase three-wire system.

The inverted three-phase system, consisting of two E.M.Fs. e at 60° displacement, and three equal currents i_3 in the three lines of equal resistance r_3 , gives the output $2 e i_3$, that is, compared with the single-phase system, $i_3 = i/2$. The loss in the three lines is $3 i_3^2 r_3 = \frac{3}{4} i^2 r_3$. Hence, to give the same loss $2 i^2 r$ as the single-phase system, it must be $r_3 = \frac{8}{3} r$, that is, each of the three wires must have $\frac{3}{8}$ of the copper cross-section of the wire in the two-wire single-phase system; or in other words, the inverted three-phase system requires $\frac{9}{16}$ of the copper of the two-wire single-phase system.

We get thus the result,

If a given power has to be transmitted at a given loss, and a given *minimum* potential, as for instance 110 volts for lighting, the amount of copper necessary is :

2 WIRES:	Single-phase system,	100.0
3 WIRES:	Edison three-wire single-phase system, neutral full section,	37.5
	Edison three-wire single-phase system, neutral half-section,	31.25
	Inverted three-phase system,	56.25
	Quarter-phase system with common return,	72.9
	Three-phase system,	75.0
4 WIRES:	Three-phase, with neutral wire, full section,	33.3
	Three-phase, with neutral wire, half-section,	29.17
	Independent quarter-phase system,	100.0
5 WIRES:	Edison five-wire, single-phase system, full neutral,	15.625
	Edison five-wire, single-phase system, half-neutral,	10.93
	Four-wire, quarter-phase, with common neutral, full section,	31.25
	Four-wire, quarter-phase, with common neutral, half-section,	28.125

We see herefrom, that in distribution for lighting — that is, with the same minimum potential, and with the same number of wires — the single-phase system is superior to any polyphase system.

The continuous-current system is equivalent in this comparison to the single-phase alternating-current system of the same effective potential, since the comparison is made on the basis of effective potential, and the power depends upon the effective potential also.

261. *Comparison on the Basis of Equality of the Maximum Difference of Potential in the System, in Long-Distance Transmission, Power Distribution, etc.*

Wherever the potential is so high as to bring the question of the strain on the insulation into consideration, or in other cases, to approach the danger limit to life, the proper comparison of different systems is on the basis of equality of maximum potential in the system.

Hence in this case, since the maximum potential is fixed, nothing is gained by three- or five-wire Edison systems. Thus, such systems do not come into consideration.

The comparison of the three-phase system with the single-phase system remains the same, since the three-phase system has the same maximum as minimum potential; that is:

The three-phase system requires three-fourths of the copper of the single-phase system to transmit the same power at the same loss over the same distance.

The four-wire quarter-phase system requires the same amount of copper as the single-phase system, since it consists of two single-phase systems.

In a quarter-phase system with common return, the potential between the outside wire is $\sqrt{2}$ times the potential per branch, hence to get the same maximum strain on the insulation — that is, the same potential e between the outside wires as in the single-phase system — the potential per branch will be $e/\sqrt{2}$, hence the current $i_4 = i/\sqrt{2}$, if i equals the current of the single-phase system of equal power, and $i_4 \sqrt{2} = i$ will be the current in the central wire.

Hence, if r_4 = resistance per outside wire, $r_4/\sqrt{2}$ = resistance of central wire, and the total loss in the system is:

$$2 i_4^2 r_4 + \frac{i_4^2 2 r_4}{\sqrt{2}} = i_4^2 r_4 (2 + \sqrt{2}) = i^2 r_4 \frac{(2 + \sqrt{2})}{2}.$$

Since in the single-phase system, the loss = $2 i^2 r$, it is :

$$r_4 = \frac{4 r}{2 + \sqrt{2}}.$$

That is, each of the outside wires has to contain $\frac{2 + \sqrt{2}}{4}$ times as much copper as each of the single-phase wires. The central wires have to contain $\frac{2 \times \sqrt{2}}{4} \sqrt{2}$ times as much copper; hence the total system contains $\frac{2(2 + \sqrt{2})}{4} + \frac{2 + \sqrt{2}}{4} \sqrt{2}$ times as much copper as each of the single-phase wires; that is, $\frac{3 + 2\sqrt{2}}{4}$ times the copper of the single-phase system.

Or, in other words,

A quarter-phase system with common return requires $\frac{3 + 2\sqrt{2}}{4} = 1.457$ times as much copper as a single-phase system of the same maximum potential, same power, and same loss.

Since the comparison is made on the basis of equal maximum potential, and the maximum potential of alternating system is $\sqrt{2}$ times that of a continuous-current circuit of equal effective potential, the alternating circuit of effective potential e compares with the continuous-current circuit of potential $e \sqrt{2}$, which latter requires only half the copper of the alternating system.

This comparison of the alternating with the continuous-current system is not proper however, since the continuous-current potential introduces, besides the electrostatic strain, an electrolytic strain on the dielectric which does not exist in the alternating system, and thus makes the action of the continuous-current potential on the insulation more severe than that of an equal alternating potential. Besides, at the voltages which came under consideration, the continuous current is excluded to begin with.

Thus we get :

If a given power is to be transmitted at a given loss, and a given *maximum* difference of potential in the system, that is, with the same strain on the insulation, the amount of copper required is :

2 WIRES : Single-phase system,	100.0
Continuous-current system,	50.0
3 WIRES : Three-phase system,	75.0
Quarter-phase system, with common return,	145.7
4 WIRES : Independent Quarter-phase system,	100.0

Hence the quarter-phase system with common return is practically excluded from long-distance transmission.

262. In a different way the same comparative results between single-phase, three-phase, and quarter-phase systems can be derived by resolving the systems into their single-phase branches.

The three-phase system of E.M.F. e between the lines can be considered as consisting of three single-phase circuits of E.M.F. $e/\sqrt{3}$, and no return. The single-phase system of E.M.F. e between lines as consisting of two single-phase circuits of E.M.F. $e/2$ and no return. Thus, the relative amount of copper in the two systems being inversely proportional to the square of E.M.F., bears the relation $(\sqrt{3}/e)^2 : (2/e)^2 = 3 : 4$; that is, the three-phase system requires 75 per cent of the copper of the single-phase system.

The quarter-phase system with four equal wires requires the same copper as the single-phase system, since it consists of two single-phase circuits. Replacing two of the four quarter-phase wires by one wire of the same cross-section as each of the wires replaced thereby, the current in this wire is $\sqrt{2}$ times as large as in the other wires, hence, the loss twice as large — that is, the same as in the two wires replaced by this common wire, or the total loss is not

changed — while 25 per cent of the copper is saved, and the system requires only 75 per cent of the copper of the single-phase system, but produces $\sqrt{2}$ times as high a potential between the outside wires. Hence, to give the same maximum potential, the E.M.Fs. of the system have to be reduced by $\sqrt{2}$, that is, the amount of copper doubled, and thus the quarter-phase system with common return of the same cross-section as the outside wires requires 150 per cent of the copper of the single-phase system. In this case, however, the current density in the middle wire is higher, thus the copper not used most economical, and transferring a part of the copper from the outside wire to the middle wire, to bring all three wires to the same current density, reduces the loss, and thereby reduces the amount of copper at a given loss, to 145.7 per cent of that of a single-phase system.

CHAPTER XXIX.

THREE-PHASE SYSTEM.

263. With equal load of the same phase displacement in all three branches, the symmetrical three-phase system offers no special features over those of three equally loaded single-phase systems, and can be treated as such; since the mutual reactions between the three-phases balance at equal distribution of load, that is, since each phase is acted upon by the preceding phase in an equal but opposite manner as by the following phase.

With unequal distribution of load between the different branches, the voltages and phase differences become more or less unequal. These unbalancing effects are obviously maximum, if some of the phases are fully loaded, others unloaded,

Let :

E = E.M.F. between branches 1 and 2 of a three-phaser.

Then :

$$\epsilon E = \text{E.M.F. between 2 and 3,}$$

$$\epsilon^2 E = \text{E.M.F. between 3 and 1,}$$

where,

$$\epsilon = \sqrt[3]{1} = \frac{-1 + j\sqrt{3}}{2}.$$

Let

Z_1, Z_2, Z_3 = impedances of the lines issuing from generator terminals 1, 2, 3,

and Y_1, Y_2, Y_3 = admittances of the consumer circuits connected between lines 2 and 3, 3 and 1, 1 and 2.

If then,

I_1, I_2, I_3 , are the currents issuing from the generator terminals into the lines, it is,

$$I_1 + I_2 + I_3 = 0. \quad (1)$$

If I_1', I_2, I_3' = currents flowing through the admittances Y_1, Y_2, Y_3 , from 2 to 3, 3 to 1, 1 to 2, it is,

$$\left. \begin{aligned} I_1 &= I_3' - I_2', \text{ or, } I_1 + I_2' - I_3' = 0 \\ I_2 &= I_1' - I_3', \text{ or, } I_2 + I_3' - I_1' = 0 \\ I_3 &= I_2' - I_1', \text{ or, } I_3 + I_1' - I_2' = 0 \end{aligned} \right\} \quad (2)$$

These three equations (2) added, give (1) as dependent equation.

At the ends of the lines 1, 2, 3, it is :

$$\left. \begin{aligned} E_1' &= E_1 - Z_2 I_2 + Z_3 I_3 \\ E_2' &= E_2 - Z_3 I_3 + Z_1 I_1 \\ E_3' &= E_3 - Z_1 I_1 + Z_2 I_2 \end{aligned} \right\} \quad (3)$$

the differences of potential, and

$$\left. \begin{aligned} I_1' &= E_1' Y_1 \\ I_2' &= E_2' Y_2 \\ I_3' &= E_3' Y_3 \end{aligned} \right\} \quad (4)$$

the currents in the receiver circuits.

These nine equations (2), (3), (4), determine the nine quantities : $I_1, I_2, I_3, I_1', I_2', I_3', E_1', E_2', E_3'$.

Equations (4) substituted in (2) give :

$$\left. \begin{aligned} I_1 &= E_3' Y_3 - E_2' Y_2 \\ I_2 &= E_1' Y_1 - E_3' Y_3 \\ I_3 &= E_2' Y_2 - E_1' Y_1 \end{aligned} \right\} \quad (5)$$

These equations (5) substituted in (3), and transposed, give,

since $\left. \begin{aligned} E_1 &= \epsilon E \\ E_2 &= \epsilon^2 E \\ E_3 &= E \end{aligned} \right\}$ as E.M.Fs. at the generator terminals.

$$\left. \begin{aligned} \epsilon E - E_1' (1 + Y_1 Z_2 + Y_1 Z_3) + E_2' Y_2 Z_3 + E_3' Y_3 Z_2 &= 0 \\ \epsilon^2 E - E_2' (1 + Y_2 Z_3 + Y_2 Z_1) + E_3' Y_3 Z_1 + E_1' Y_1 Z_3 &= 0 \\ E - E_3' (1 + Y_3 Z_1 + Y_3 Z_2) + E_1' Y_1 Z_2 + E_2' Y_2 Z_1 &= 0 \end{aligned} \right\} \quad (6)$$

as three linear equations with the three quantities E'_1 , E'_2 , E'_3 .

Substituting the abbreviations :

$$\left. \begin{aligned} D &= \begin{vmatrix} -(1 + Y_1 Z_2 + Y_1 Z_3), & Y_2 Z_3, & Y_3 Z_2 \\ Y_1 Z_3, & -(1 + Y_2 Z_3 + Y_2 Z_1), & Y_3 Z_1 \\ Y_1 Z_2, & Y_2 Z_1, & -(1 + Y_3 Z_1 + Y_3 Z_2) \end{vmatrix} \\ D_1 &= \begin{vmatrix} \epsilon, & Y_2 Z_3, & Y_3 Z_2 \\ \epsilon^2, & -(1 + Y_2 Z_3 + Y_2 Z_1), & Y_3 Z_1 \\ 1, & Y_2 Z_1, & -(1 + Y_3 Z_1 + Y_3 Z_2) \end{vmatrix} \\ D_2 &= \begin{vmatrix} -(1 + Y_1 Z_2 + Y_1 Z_3), & \epsilon, & Y_3 Z_2 \\ Y_1 Z_3, & \epsilon^2, & Y_3 Z_1 \\ Y_1 Z_2, & 1, & -(1 + Y_3 Z_1 + Y_3 Z_2) \end{vmatrix} \\ D_3 &= \begin{vmatrix} -(1 + Y_1 Z_2 + Y_1 Z_3), & Y_2 Z_3, & \epsilon \\ Y_1 Z_3, & -(1 + Y_2 Z_3 + Y_2 Z_1), & \epsilon^2 \\ Y_1 Z_2, & Y_2 Z_1, & 1 \end{vmatrix} \end{aligned} \right\} \quad (7)$$

it is :

$$\left. \begin{aligned} E'_1 &= D_1 / D \\ E'_2 &= D_2 / D \\ E'_3 &= D_3 / D \end{aligned} \right\} \quad (8)$$

$$\left. \begin{aligned} I'_1 &= \frac{Y_1 D_1}{D} \\ I'_2 &= \frac{Y_2 D_2}{D} \\ I'_3 &= \frac{Y_3 D_3}{D} \end{aligned} \right\} \quad (9)$$

$$\left. \begin{aligned} I_1 &= \frac{Y_3 D_3 - Y_2 D_2}{D} \\ I_2 &= \frac{Y_1 D_1 - Y_3 D_3}{D} \\ I_3 &= \frac{Y_2 D_2 - Y_1 D_1}{D} \end{aligned} \right\} \quad (10)$$

hence,

$$\left. \begin{aligned} E'_1 + E'_2 + E'_3 &= 0 \\ I_1 + I_2 + I_3 &= 0 \end{aligned} \right\} \quad (11)$$

264. SPECIAL CASES.

A. *Balanced System*

$$Y_1 = Y_2 = Y_3 = Y$$

$$Z_1 = Z_2 = Z_3 = Z.$$

Substituting this in (6), and transposing :

$$\left. \begin{aligned} E_1 &= \epsilon E \\ E_2 &= \epsilon^2 E \\ E_3 &= E \end{aligned} \right\} \begin{aligned} E_1' &= \frac{\epsilon E}{1 + 3YZ} \\ E_2' &= \frac{\epsilon^2 E}{1 + 3YZ} \\ E_3' &= \frac{E}{1 + 3YZ} \end{aligned} \right\} \quad (12)$$

$$\left. \begin{aligned} I_1' &= \frac{\epsilon EY}{1 + 3YZ} \\ I_2' &= \frac{\epsilon^2 EY}{1 + 3YZ} \\ I_3' &= \frac{EY}{1 + 3YZ} \end{aligned} \right\} \begin{aligned} I_1 &= \frac{\epsilon^2(\epsilon - 1)EY}{1 + 3YZ} \\ I_2 &= \frac{(\epsilon - 1)EY}{1 + 3YZ} \\ I_3 &= \frac{\epsilon(\epsilon - 1)EY}{1 + 3YZ} \end{aligned} \right\}$$

The equations of the symmetrical balanced three-phase system.

B. *One circuit loaded, two unloaded:*

$$Y_1 = Y_2 = 0, \quad Y_3 = Y$$

$$Z_1 = Z_2 = Z_3 = Z.$$

Substituted in equations (6) :

$$\left. \begin{aligned} \epsilon E - E_1' + E_3'YZ &= 0 \\ \epsilon^2 E - E_2' + E_3'YZ &= 0 \end{aligned} \right\} \text{unloaded branches.}$$

$$E - E_3'(1 + 2YZ) = 0, \text{ loaded branch.}$$

hence :

$$\left. \begin{aligned} E_1' &= \frac{E \{ \epsilon + (1 + 2\epsilon)YZ \}}{1 + 2YZ} \\ E_2' &= \frac{E \{ \epsilon^2 + (1 + 2\epsilon^2)YZ \}}{1 + 2YZ} \\ E_3' &= \frac{E}{1 + 2YZ} \end{aligned} \right\} \begin{array}{l} \text{unloaded;} \\ \text{loaded;} \end{array} \left. \begin{array}{l} \text{all three} \\ \text{E.M.Fs.} \\ \text{unequal.} \end{array} \right\} \quad (13)$$

$$\left. \begin{aligned} I'_1 &= I'_2 = 0 \\ I'_3 &= \frac{EY}{1 + 2YZ} \end{aligned} \right\} \quad (13)$$

$$\left. \begin{aligned} I_1 &= \frac{EY}{1 + 2YZ} \\ I_2 &= -\frac{EY}{1 + 2YZ} \\ I_3 &= 0 \end{aligned} \right\} \quad (13)$$

C. *Two circuits loaded, one unloaded.*

$$\begin{aligned} Y_1 &= Y_2 = Y, & Y_3 &= 0, \\ Z_1 &= Z_2 = Z_3 = Z. \end{aligned}$$

Substituting this in equations (6), it is :

$$\left. \begin{aligned} \epsilon E - E'_1(1 + 2YZ) + E'_2YZ &= 0 \\ \epsilon^2 E - E'_2(1 + 2YZ) + E'_1YZ &= 0 \end{aligned} \right\} \text{loaded branches.}$$

$$E - E'_3 + (E'_1 + E'_2)YZ = 0 \quad \text{unloaded branch.}$$

or, since :

$$\begin{aligned} (E'_1 + E'_2) &= -E'_3; \\ E - E'_3 - E'_3YZ &= 0, \end{aligned}$$

$$E'_3 = \frac{E}{1 + YZ}$$

thus :

$$\left. \begin{aligned} E'_1 &= \frac{E\epsilon\{1 + (2 + \epsilon)YZ\}}{1 + 4YZ + 3Y^2Z^2} \\ E'_2 &= \frac{E\epsilon^2\{1 + (2 + \epsilon^2)YZ\}}{1 + 4YZ + 3Y^2Z^2} \\ E'_3 &= \frac{E}{1 + YZ} \end{aligned} \right\} \begin{array}{l} \text{loaded branches.} \\ \text{unloaded branch.} \end{array} \quad (14)$$

As seen, with unsymmetrical distribution of load, all three branches become more or less unequal.

CHAPTER XXX.

QUARTER-PHASE SYSTEM.

265. In a three-wire quarter-phase system, or quarter-phase system with common return wire of both phases, let the two outside terminals and wires be denoted by 1 and 2, the middle wire or common return by 0.

It is then :

$$E_1 = E = \text{E.M.F. between 0 and 1 in the generator.}$$

$$E_2 = jE = \text{E.M.F. between 0 and 2 in the generator.}$$

Let :

- I_1 and $I_2 =$ currents in 1 and in 2,
- $I_0 =$ current in 0,
- Z_1 and $Z_2 =$ impedances of lines 1 and 2,
- $Z_0 =$ impedance of line 0.
- Y_1 and $Y_2 =$ admittances of circuits 0 to 1, and 0 to 2,
- I'_1 and $I'_2 =$ currents in circuits 0 to 1, and 0 to 2,
- E'_1 and $E'_2 =$ potential differences at circuit 0 to 1, and 0 to 2.

it is then, $I_1 + I_2 + I_0 = 0$ } (1)

or, $I_0 = -(I_1 + I_2)$ }

that is, I_0 is common return of I_1 and I_2 .

Further, let :

$$\left. \begin{aligned} E'_1 &= E - I_1 Z_1 + I_0 Z_0 = E - I_1 (Z_1 + Z_0) - I_2 Z_0 \\ E'_2 &= jE - I_2 Z_2 + I_0 Z_0 = jE - I_2 (Z_2 + Z_0) - I_1 Z_1 \end{aligned} \right\} (2)$$

and

$$\left. \begin{aligned} I_1 &= Y_1 E'_1 \\ I_2 &= Y_2 E'_2 \\ I_0 &= -(Y_1 E'_1 + Y_2 E'_2) \end{aligned} \right\} (3)$$

Substituting (3) in (2); and expanding :

$$\left. \begin{aligned} E_1' &= E \frac{1 + Y_2 Z_2 + Y_2 Z_0 (1 - j)}{(1 + Y_1 Z_0 + Y_1 Z_1)(1 + Y_2 Z_0 + Y_2 Z_2) - Y_1 Y_2 Z_0^2} \\ E_2' &= jE \frac{1 + Y_1 Z_1 + Y_1 Z_0 (1 + j)}{(1 + Y_1 Z_0 + Y_1 Z_1)(1 + Y_2 Z_0 + Y_2 Z_2) - Y_1 Y_2 Z_0^2} \end{aligned} \right\} (4)$$

Hence, the two E.M.Fs. at the end of the line are unequal in magnitude, and not in quadrature any more.

266. SPECIAL CASES :

A. *Balanced System.*

$$Z_1 = Z_2 = Z;$$

$$Z_0 = Z / \sqrt{2};$$

$$Y_1 = Y_2 = Y.$$

Substituting these values in (4), gives :

$$\left. \begin{aligned} E_1' &= E \frac{1 + \frac{1 + \sqrt{2} - j}{\sqrt{2}} YZ}{1 + \sqrt{2} (1 + \sqrt{2}) YZ + (1 + \sqrt{2}) Y^2 Z^2} \\ &= E \frac{1 + (1.707 - .707 j) YZ}{1 + 3.414 YZ + 2.414 Y^2 Z^2} \\ E_2' &= jE \frac{1 + \frac{1 + \sqrt{2} + j}{\sqrt{2}} YZ}{1 + \sqrt{2} (1 + \sqrt{2}) YZ + (1 + \sqrt{2}) Y^2 Z^2} \\ &= jE \frac{1 + (1.707 + .707 j) YZ}{1 + 3.414 YZ + 2.414 Y^2 Z^2} \end{aligned} \right\} (5)$$

Hence, the balanced quarter-phase system with common return is unbalanced with regard to voltage and phase relation, or in other words, even if in a quarter-phase system with common return both branches or phases are loaded equally, with a load of the same-phase displacement, nevertheless the system becomes unbalanced, and the two E.M.Fs. at the end of the line are neither equal in magnitude, nor in quadrature with each other.

B. One branch loaded, one unloaded.

$$Z_1 = Z_2 = Z;$$

$$Z_0 = Z\sqrt{2}.$$

a.) $Y_1 = 0, \quad Y_2 = Y.$

b.) $Y_1 = Y, \quad Y_2 = 0.$

Substituting these values in (4), gives :

$$\begin{aligned}
 a.) \quad E_1' &= E \frac{1 + YZ \frac{1 + \sqrt{2} - j}{\sqrt{2}}}{1 + YZ \frac{1 + \sqrt{2}}{\sqrt{2}}} \\
 &= E \left\{ \frac{1 - \frac{j}{1 + \sqrt{2} + \frac{\sqrt{2}}{YZ}}}{1} \right\} \\
 &= E \left\{ \frac{1 - \frac{j}{2.414 + \frac{1.414}{YZ}}}{1} \right\} \\
 E_2' &= jE \frac{1}{1 - YZ \frac{1 + \sqrt{2}}{\sqrt{2}}} \\
 &= jE \frac{1}{1 + 1.707 YZ}
 \end{aligned} \tag{6}$$

$$\begin{aligned}
 b.) \quad E_1' &= E \frac{1}{1 + YZ \frac{1 + \sqrt{2}}{\sqrt{2}}} \\
 &= E \frac{1}{1 + 1.707 YZ} \\
 E_2' &= jE \frac{1 + YZ \frac{1 + \sqrt{2} + j}{\sqrt{2}}}{1 + YZ \frac{1 + \sqrt{2}}{\sqrt{2}}} \\
 &= jE \left\{ \frac{1 + \frac{j}{1 + \sqrt{2} + \frac{\sqrt{2}}{YZ}}}{1} \right\} \\
 &= jE \left\{ \frac{1 + \frac{j}{2.414 + \frac{1.414}{YZ}}}{1} \right\}
 \end{aligned} \tag{7}$$

These two E.M.Fs. are unequal, and not in quadrature with each other.

But the values in case *a.*) are different from the values in case *b.*)

That means :

The two phases of a three-wire quarter-phase system are unsymmetrical, and the leading phase 1 reacts upon the lagging phase 2 in a different manner than 2 reacts upon 1.

It is thus undesirable to use a three-wire quarter-phase system, except in cases where the line impedances Z are negligible.

In all other cases, the four-wire quarter-phase system is preferable, which essentially consists of two independent single-phase circuits, and is treated as such.

Obviously, even in such an independent quarter-phase system, at unequal distribution of load, unbalancing effects may take place.

If one of the branches or phases is loaded differently from the other, the drop of voltage and the shift of the phase will be different from that in the other branch; and thus the E.M.Fs. at the end of the lines will be neither equal in magnitude, nor in quadrature with each other.

With both branches however loaded equally, the system remains balanced in voltage and phase, just like the three-phase system under the same conditions.

Thus the four-wire quarter-phase system and the three-phase system are balanced with regard to voltage and phase at equal distribution of load, but are liable to become unbalanced at unequal distribution of load; the three-wire quarter-phase system is unbalanced in voltage and phase, even at equal distribution of load.

APPENDICES.

APPENDIX I.

ALGEBRA OF COMPLEX IMAGINARY QUANTITIES.

INTRODUCTION.

267. The system of numbers, of which the science of algebra treats, finds its ultimate origin in experience. Directly derived from experience, however, are only the absolute integral numbers; fractions, for instance, are not directly derived from experience, but are abstractions expressing relations between different classes of quantities. Thus, for instance, if a quantity is divided in two parts, from one quantity two quantities are derived, and denoting these latter as halves expresses a relation, namely, that two of the new kinds of quantities are derived from, or can be combined to one of the old quantities.

268. Directly derived from experience is the *operation of counting* or of *numeration*.

$$a, a + 1, a + 2, a + 3 \dots$$

Counting by a given number of integers :

$$a + \underbrace{1 + 1 + 1 \dots + 1}_{b \text{ integers}} = c$$

introduces the operation of *addition*, as multiple counting :

$$a + b = c.$$

It is,

$$a + b = b + a,$$

that is, the terms of addition, or addenda, are interchangeable.

Multiple addition of the same terms :

$$\underbrace{a + a + a + \dots + a}_{b \text{ equal numbers}} = c$$

introduces the operation of *multiplication* :

$$a \times b = c.$$

It is,

$$a \times b = b \times a,$$

that is, the terms of multiplication, or factors, are interchangeable.

Multiple multiplication of the same factors :

$$\underbrace{a \times a \times a \times \dots \times a}_{b \text{ equal numbers}} = c$$

introduces the operation of *involution* :

$$a^b = c$$

Since a^b is not equal to b^a ,

the terms of involution are not interchangeable.

269. The reverse operation of addition introduces the operation of *subtraction* :

$$\begin{array}{l} \text{If} \quad \quad \quad a + b = c, \\ \text{it is} \quad \quad c - b = a. \end{array}$$

This operation cannot be carried out in the system of absolute numbers, if :

$$b > c.$$

Thus, to make it possible to carry out the operation of subtraction under any circumstances, the system of absolute numbers has to be expanded by the introduction of the *negative number* :

$$-a = (-1) \times a,$$

where

$$(-1)$$

is the negative unit.

Thereby the system of numbers is subdivided in the

positive and negative numbers, and the operation of subtraction possible for all values of subtrahend and minuend.

or
$$(-1) \times (-1) = 1;$$

that is, the negative unit is defined by :

$$(-1)^2 = 1.$$

270. The reverse operation of multiplication introduces the operation of *division* :

If
$$a \times b = c.$$
 then
$$\frac{c}{b} = a.$$

In the system of integral numbers this operation can only be carried out, if b is a factor of c .

To make it possible to carry out the operation of division under any circumstances, the system of integral numbers has to be expanded by the introduction of the *fraction* :

$$\frac{c}{b} = c \times \left(\frac{1}{b}\right),$$

where
$$\frac{1}{b}$$

is the integer fraction, and is defined by :

$$\left(\frac{1}{b}\right) \times b = 1.$$

271. The reverse operation of involution introduces two new operations, since in the involution :

$$a^b = c,$$

the quantities a and b are not reversible.

Thus
$$\sqrt[b]{c} = a, \text{ the } \textit{evolution}.$$

$$\log_a c = b, \text{ the } \textit{logarithmation}.$$

The operation of evolution of terms c , which are not complete powers, makes a further expansion of the system

of numbers necessary, by the introduction of the *irrational number* (endless decimal fraction), as for instance :

$$\sqrt{2} = 1.414213.$$

272. The operation of evolution of negative quantities c with even exponents b , as for instance

$$\sqrt[b]{-a}$$

makes a further expansion of the system of numbers necessary, by the introduction of the *imaginary unit*.

$$\text{Thus} \quad \sqrt[b]{-a} = \sqrt[b]{-1} \times \sqrt[b]{a}.$$

where : $\sqrt{-1}$ is denoted by j .

Thus, the imaginary unit j is defined by :

$$j^2 = -1.$$

By addition and subtraction of real and imaginary units, compound numbers are derived of the form :

$$a + jb,$$

which are denoted as *complex imaginary numbers*.

No further system of numbers is introduced by the operation of evolution.

The operation of logarithmation introduces the irrational and imaginary and complex imaginary numbers also, but no further system of numbers.

273. Thus, starting from the absolute integral numbers of experience, by the two conditions :

1st. Possibility of carrying out the algebraic operations and their reverse operations under all conditions,

2d. Permanence of the laws of calculation, the expansion of the system of numbers has become necessary, into

Positive and negative numbers,

Integral numbers and fractions,

Rational and irrational numbers,

Real and imaginary numbers and complex imaginary numbers.

Therewith closes the field of algebra, and all the algebraic operations and their reverse operations can be carried out irrespective of the values of terms entering the operation.

Thus within the range of algebra no further extension of the system of numbers is necessary or possible, and the most general number is

$$a + jb.$$

where a and b can be integers or fractions, positive or negative, rational or irrational.

ALGEBRAIC OPERATIONS WITH COMPLEX IMAGINARY QUANTITIES.

274. Definition of imaginary unit:

$$j^2 = -1.$$

Complex imaginary number:

$$A = a + jb.$$

Substituting:

$$a = r \cos \beta$$

$$b = r \sin \beta,$$

it is

$$A = r (\cos \beta + j \sin \beta),$$

where

$$r = \sqrt{a^2 + b^2}.$$

$$\tan \beta = \frac{b}{a},$$

r = vector,

β = amplitude of complex imaginary number A .

Substituting:

$$\cos \beta = \frac{e^{j\beta} + e^{-j\beta}}{2}$$

$$\sin \beta = \frac{e^{j\beta} - e^{-j\beta}}{2j}.$$

it is

$$A = r e^{j\beta},$$

where $e = \lim_{n \rightarrow \infty} \left(1 + \frac{1}{n}\right)^n = \sum_{k=0}^{\infty} \frac{1}{1 \times 2 \times 3 \times \dots \times k}$

is the basis of the natural logarithms.

Conjugate numbers:

$$a + jb = r (\cos \beta + j \sin \beta) = r e^{j\beta}$$

and $a - jb = r (\cos [-\beta] + j \sin [-\beta]) = r e^{-j\beta}$

it is $(a + jb)(a - jb) = a^2 + b^2 = r^2$.

Associate numbers:

$$a + jb = r (\cos \beta + j \sin \beta) = r e^{j\beta}$$

and $b + ja = r \left(\cos \left[\frac{\pi}{2} - \beta \right] + j \sin \left[\frac{\pi}{2} - \beta \right] \right) = r e^{j \left(\frac{\pi}{2} - \beta \right)}$;

it is $(a + jb)(b + ja) = j(a^2 + b^2) = jr^2$.

If $a + jb = a' + jb'$,

it is

$$a = a'$$

$$b = b'.$$

If $a + jb = 0$;

it is

$$a = 0,$$

$$b = 0.$$

275. Addition and Subtraction:

$$(a + jb) \pm (a' + jb') = (a \pm a') + j(b \pm b').$$

Multiplication:

$$(a + jb)(a' + jb') = (aa' - bb') + j(ab' + ba')$$

or $r (\cos \beta + j \sin \beta) \times r' (\cos \beta' + j \sin \beta') = rr' (\cos [\beta + \beta'] + j \sin [\beta + \beta'])$;

or $r e^{j\beta} \times r' e^{j\beta'} = rr' e^{j(\beta + \beta')}$.

Division:

Expansion of complex imaginary fraction, for rationalization of denominator or numerator, by multiplication with the conjugate quantity:

$$\begin{aligned} \frac{a + jb}{a' + jb'} &= \frac{(a + jb)(a' - jb')}{(a' + jb')(a' - jb')} = \frac{(aa' + bb') + j(bb' - a'a')}{a'^2 + b'^2} \\ &= \frac{(a + jb)(a - jb)}{(a' + jb')(a - jb)} = \frac{a^2 + b^2}{(aa' + bb') + j(ab' - ba')} \end{aligned}$$

or, $\frac{r(\cos \beta + j \sin \beta)}{r'(\cos \beta' + j \sin \beta')} = \frac{r}{r'} (\cos [\beta - \beta'] + j \sin [\beta - \beta'])$;

or, $\frac{r e^{j\beta}}{r' e^{j\beta'}} = \frac{r}{r'} e^{j(\beta - \beta')}$.

involution:

$$\begin{aligned} (a + jb)^n &= \{r(\cos \beta + j \sin \beta)\}^n = \{r e^{j\beta}\}^n \\ &= r^n (\cos n\beta + j \sin n\beta) = r^n e^{jn\beta}. \end{aligned}$$

evolution:

$$\begin{aligned} \sqrt[n]{a + jb} &= \sqrt[n]{r(\cos \beta + j \sin \beta)} = \sqrt[n]{r e^{j\beta}} \\ &= \sqrt[n]{r} \left(\cos \frac{\beta}{n} + j \sin \frac{\beta}{n} \right) = \sqrt[n]{r} e^{j\frac{\beta}{n}} \end{aligned}$$

276. Roots of the Unit:

$$\sqrt[2]{1} = +1, \quad -1;$$

$$\sqrt[3]{1} = +1, \quad \frac{-1 + j\sqrt{3}}{2}, \quad \frac{-1 - j\sqrt{3}}{2};$$

$$\sqrt[4]{1} = +1, \quad -1, \quad +j, \quad -j;$$

$$\begin{aligned} \sqrt[8]{1} = +1, \quad -1, \quad +j, \quad -j, \quad \frac{+1 + j\sqrt{2}}{2}, \quad \frac{+1 - j\sqrt{2}}{2}, \quad \frac{-1 + j\sqrt{2}}{2}, \\ \frac{-1 - j\sqrt{2}}{2}; \end{aligned}$$

$$\sqrt[n]{1} = \cos \frac{2\pi k}{n} + j \sin \frac{2\pi k}{n} = e^{\frac{2\pi jk}{n}}, \quad k = 0, 1, 2, \dots, n - 1.$$

277. Rotation:

In the complex imaginary plane, multiplication with

$$\sqrt[n]{1} = \cos \frac{2\pi}{n} + j \sin \frac{2\pi}{n} = e^{\frac{2\pi j}{n}}$$

means rotation, in positive direction, by $1/n$ of a revolution,

multiplication with (-1) means reversal, or rotation by 180° ,
multiplication with $(+j)$ means positive rotation by 90° ,
multiplication with $(-j)$ means negative rotation by 90° .

278. *Complex imaginary plane :*

While the positive and negative numbers can be represented by the points of a line, the complex imaginary numbers are represented by the points of a plane, with the horizontal axis as real axis, the vertical axis as imaginary axis. Thus all

the positive real numbers are represented by the points of half axis OA towards the right ;

the negative real numbers are represented by the points of half axis $\overline{OA'}$ towards the left ;

the positive imaginary numbers are represented by the points of half axis \overline{OB} upwards ;

the negative imaginary numbers are represented by the points of half axis $\overline{OB'}$ downwards ;

the complex imaginary numbers are represented by the points outside of the coördinate axes.

APPENDIX II.

OSCILLATING CURRENTS.

INTRODUCTION.

279. An electric current varying periodically between constant maximum and minimum values, — that is, in equal time intervals repeating the same values, — is called an alternating current if the arithmetic mean value equals zero; and is called a pulsating current if the arithmetic mean value differs from zero.

Assuming the wave as a sine curve, or replacing it by the equivalent sine wave, the alternating current is characterized by the period or the time of one complete cyclic change, and the amplitude or the maximum value of the current. Period and amplitude are constant in the alternating current.

A very important class are the currents of constant period, but geometrically varying amplitude; that is, currents in which the amplitude of each following wave bears to that of the preceding wave a constant ratio. Such currents consist of a series of waves of constant length, decreasing in amplitude, that is in strength, in constant proportion. They are called oscillating currents in analogy with mechanical oscillations, — for instance of the pendulum, — in which the amplitude of the vibration decreases in constant proportion.

Since the amplitude of the oscillating current varies, constantly decreasing, the oscillating current differs from

the alternating current in so far that it starts at a definite time, and gradually dies out, reaching zero value theoretically at infinite time, practically in a very short time, short even in comparison with the time of one alternating half-wave. Characteristic constants of the oscillating current are the period T or frequency $N = 1/T$, the first amplitude and the ratio of any two successive amplitudes, the latter being called the decrement of the wave. The oscillating current will thus be represented by the product of

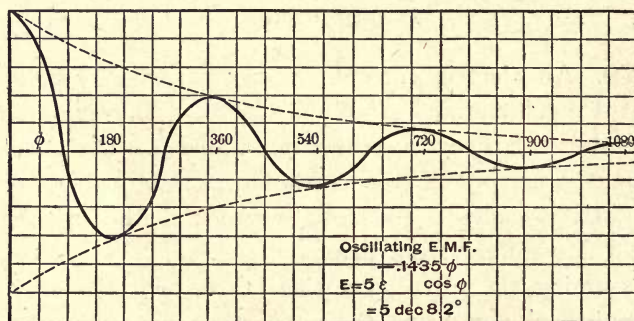


Fig. 181.

a periodic function, and a function decreasing in geometric proportion with the time. The latter is the exponential function A^{f-gt} .

280. Thus, the general expression of the oscillating current is

$$I = A^{f-gt} \cos(2\pi Nt - \hat{\omega}),$$

since

$$A^{f-gt} = A^f A^{-gt} = i \epsilon^{-bt}.$$

Where ϵ = basis of natural logarithms, the current may be expressed

$$I = i \epsilon^{-bt} \cos(2\pi Nt - \hat{\omega}) = c \epsilon^{-a\phi} \cos(\phi - \hat{\omega}),$$

where $\phi = 2\pi Nt$; that is, the period is represented by a complete revolution.

In the same way an oscillating electromotive force will be represented by

$$E = e \epsilon_i^{-a\phi} \cos(\phi - \hat{\omega}).$$

Such an oscillating electromotive force for the values

$$e = 5, \quad a = .1435 \text{ or } \epsilon^{-2\pi a} = .4, \quad \hat{\omega} = 0,$$

is represented in rectangular coördinates in Fig. 181, and in polar coördinates in Fig. 182. As seen from Fig. 181, the oscillating wave in rectangular coördinates is tangent to the two exponential curves,

$$y = \pm e \epsilon^{-a\phi}.$$

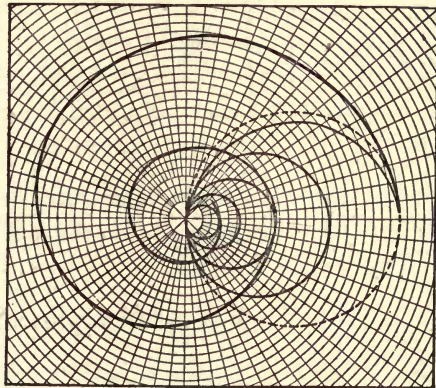


Fig. 182

281. In polar coördinates, the oscillating wave is represented in Fig. 182 by a spiral curve passing the zero point twice per period, and tangent to the exponential spiral,

$$y = \pm e \epsilon^{-a\phi}.$$

The latter is called the envelope of a system of oscillating waves of which one is shown separately, with the same constants as Figs. 181 and 182, in Fig. 183. Its character-

istic feature is: The angle which any concentric circle makes with the curve $y = e\epsilon^{-a\phi}$, is

$$\tan \alpha = \frac{dy}{y d\phi} = -a,$$

which is, therefore, constant; or, in other words: "The envelope of the oscillating current is the exponential spiral, which is characterized by a constant angle of intersection

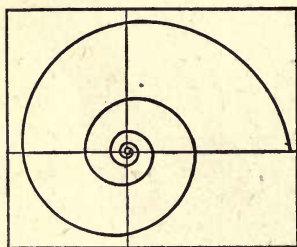


Fig. 183.

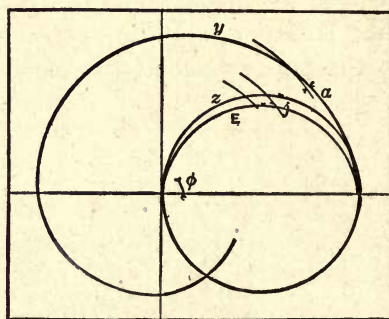


Fig. 184.

with all concentric circles or all radii vectores." The oscillating current wave is the product of the sine wave and the exponential spiral.

282. In Fig. 184 let $y = e\epsilon^{-a\phi}$ represent the exponential spiral;

let $z = e \cos (\phi - a)$

represent the sine wave;

and let $E = e\epsilon^{-a\phi} \cos (\phi - \omega)$

represent the oscillating wave.

We have then

$$\begin{aligned} \tan \beta &= \frac{dE}{E d\phi} \\ &= \frac{-\sin (\phi - \hat{\omega}) - a \cos (\phi - \hat{\omega})}{\cos (\phi - \hat{\omega})} \\ &= -\{\tan (\phi - \hat{\omega}) + a\}; \end{aligned}$$

that is, while the slope of the sine wave, $z = e \cos (\phi - \hat{\omega})$, is represented by

$$\tan \gamma = - \tan (\phi - \hat{\omega}),$$

the slope of the exponential spiral $y = e \epsilon^{-a\phi}$ is

$$\tan \alpha = - a = \text{constant.}$$

That of the oscillating wave $E = e \epsilon^{-a\phi} \cos (\phi - \hat{\omega})$ is

$$\tan \beta = - \{ \tan (\phi - \hat{\omega}) + a \}.$$

Hence, it is increased over that of the alternating sine wave by the constant a . The ratio of the amplitudes of two consequent periods is

$$A = \frac{E_{2\pi}}{E_0} = \epsilon^{-2\pi a}.$$

A is called the numerical decrement of the oscillating wave, a the exponential decrement of the oscillating wave, α the angular decrement of the oscillating wave. The oscillating wave can be represented by the equation

$$E = e \epsilon^{-\phi \tan \alpha} \cos (\phi - \hat{\omega}).$$

In the instance represented by Figs. 181 and 182, we have $A = .4$, $a = .1435$, $\alpha = 8.2^\circ$.

Impedance and Admittance.

283. In complex imaginary quantities, the alternating wave

$$z = e \cos (\phi - \hat{\omega})$$

is represented by the symbol

$$E = e (\cos \hat{\omega} + j \sin \hat{\omega}) = e_1 + j e_2.$$

By an extension of the meaning of this symbolic expression, the oscillating wave $E = e \epsilon^{-a\phi} \cos (\phi - \hat{\omega})$ can be expressed by the symbol

$$E = e (\cos \hat{\omega} + j \sin \hat{\omega}) \text{ dec } a = (e_1 + j e_2) \text{ dec } a,$$

where $a = \tan \alpha$ is the exponential decrement, α the angular decrement, $\epsilon^{-2\pi a}$ the numerical decrement.

Inductance.

284. Let r = resistance, L = inductance, and $x = 2\pi NL$ = reactance.

In a circuit excited by the oscillating current,

$$I = i\epsilon^{-a\phi} \cos(\phi - \hat{\omega}) = i(\cos \hat{\omega} + j \sin \hat{\omega}) \operatorname{dec} a = (i_1 + j i_2) \operatorname{dec} a,$$

where $i_1 = i \cos \hat{\omega}$, $i_2 = i \sin \hat{\omega}$, $a = \tan \alpha$.

We have then,

The electromotive force consumed by the resistance r of the circuit

$$E_r = r I \operatorname{dec} a.$$

The electromotive force consumed by the inductance L of the circuit,

$$E_x = L \frac{dI}{dt} = 2\pi NL \frac{dI}{d\phi} = x \frac{dI}{d\phi}.$$

$$\begin{aligned} \text{Hence } E_x &= -x i \epsilon^{-a\phi} \{\sin(\phi - \hat{\omega}) + a \cos(\phi - \hat{\omega})\} \\ &= -\frac{x i \epsilon^{-a\phi}}{\cos \alpha} \sin(\phi - \hat{\omega} + \alpha). \end{aligned}$$

Thus, in symbolic expression,

$$\begin{aligned} E_x &= -\frac{x i}{\cos \alpha} \{-\sin(\hat{\omega} - \alpha) + j \cos(\hat{\omega} - \alpha)\} \operatorname{dec} a \\ &= -x i (a + j) (\cos \hat{\omega} + j \sin \hat{\omega}) \operatorname{dec} a; \end{aligned}$$

that is, $E_x = -x I (a + j) \operatorname{dec} a$.

Hence the apparent reactance of the oscillating current circuit is, in symbolic expression,

$$X = x (a + j) \operatorname{dec} a.$$

Hence it contains an energy component ax , and the impedance is

$$Z = (r - X) \operatorname{dec} a = \{r - x(a + j)\} \operatorname{dec} a = (r - ax - jx) \operatorname{dec} a.$$

Capacity.

285. Let r = resistance, C = capacity, and $x_c = 1/2\pi C$ = capacity reactance. In a circuit excited by the oscillating

current I , the electromotive force consumed by the capacity C is

$$E_x = \frac{1}{C} \int I dt = \frac{1}{2\pi N C} \int I d\phi = k \int I d\phi;$$

or, by substitution,

$$\begin{aligned} E_x &= x \int i \epsilon^{-a\phi} \cos(\phi - \hat{\omega}) d\phi \\ &= \frac{x}{1+a^2} i \epsilon^{-a\phi} \{\sin(\phi - \hat{\omega}) - a \cos(\phi - \hat{\omega})\} \\ &= \frac{x i \epsilon^{-a\phi}}{(1+a^2) \cos a} \sin(\phi - \hat{\omega} - a); \end{aligned}$$

hence, in symbolic expression,

$$\begin{aligned} E_x &= \frac{x i}{(1+a^2) \cos a} \{-\sin(\hat{\omega} + a) + j \cos(\hat{\omega} + a)\} \text{dec } a \\ &= \frac{x i}{1+a^2} (a + j) (\cos \hat{\omega} + j \sin \hat{\omega}) \text{dec } a; \end{aligned}$$

hence,

$$E_x = \frac{x}{1+a^2} (-a + j) I \text{dec } a;$$

that is, the apparent capacity reactance of the oscillating circuit is, in symbolic expression,

$$C = \frac{x_c}{1+a^2} (-a + j) \text{dec } a.$$

286. We have then :

In an oscillating current circuit of resistance r , inductive reactance x , and capacity reactance x_c , with an exponential decrement a , the apparent impedance, in symbolic expression, is :

$$\begin{aligned} Z &= \left\{ r - x(a + j) + \frac{x_c}{1+a^2} (-a + j) \right\} \text{dec } a, \\ &= \left\{ r - a \left(x + \frac{x_c}{1+a^2} \right) - j \left(x - \frac{x_c}{1+a^2} \right) \right\} \text{dec } a, \\ &= r_a - j x_a; \end{aligned}$$

and, absolute,

$$z_a = \sqrt{r_a^2 + x_a^2}$$

$$= \sqrt{\left[r - a \left(x + \frac{x_c}{1 + a^2} \right) \right]^2 + \left[x - \frac{x_c}{1 + a^2} \right]^2}$$

Admittance.

287. Let $I = i\epsilon^{-a\phi} \cos(\phi - \hat{\omega}) = \text{current}$.

Then from the preceding discussion, the electromotive force consumed by resistance r , inductive reactance x , and capacity reactance x_c , is

$$E = ie^{-a\phi} \left\{ \cos(\phi - \hat{\omega}) \left[r - ax - \frac{a}{1 + a^2} x_c \right] - \sin(\phi - \hat{\omega}) \left[x - \frac{x_c}{1 + a^2} \right] \right\}$$

$$= iz_a \epsilon^{-a\phi} \cos(\phi - \hat{\omega} + \delta),$$

where $\tan \delta = \frac{x - \frac{x_c}{1 + a^2}}{r - ax - \frac{a}{1 + a^2} x_c}$,

$$z_a = \sqrt{\left(x - \frac{x_c}{1 + a^2} \right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c \right)^2};$$

substituting $\hat{\omega} + \delta$ for $\hat{\omega}$, and $e = iz_a$ we have

$$E = e \epsilon^{-a\phi} \cos(\phi - \hat{\omega}),$$

$$I = \frac{e}{z_a} \epsilon^{-a\phi} \cos(\phi - \hat{\omega} - \delta)$$

$$= e \epsilon^{-a\phi} \left\{ \frac{\cos \delta}{z_a} \cos(\phi - \hat{\omega}) + \frac{\sin \delta}{z_a} \sin(\phi - \hat{\omega}) \right\};$$

hence in complex quantities,

$$E = e (\cos \hat{\omega} + j \sin \hat{\omega}) \text{ dec } a,$$

$$I = E \left\{ \frac{\cos \delta}{z_a} + j \frac{\sin \delta}{z_a} \right\} \text{ dec } a;$$

or, substituting,

$$I = E \left\{ \frac{r - ax - \frac{a}{1 + a^2} x_c}{\left(x - \frac{x_c}{1 + a^2}\right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c\right)^2} + j \frac{x - \frac{x_c}{1 + a^2}}{\left(x - \frac{x_c}{1 + a^2}\right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c\right)^2} \right\} \text{ dec a.}$$

288. Thus in complex quantities, for oscillating currents, we have : conductance,

$$g = \frac{r - ax - \frac{a}{1 + a^2} x_c}{\left(x - \frac{x_c}{1 + a^2}\right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c\right)^2};$$

susceptance,

$$b = \frac{x - \frac{x_c}{1 + a^2}}{\left(x - \frac{x_c}{1 + a^2}\right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c\right)^2};$$

admittance, in absolute values,

$$y = \sqrt{g^2 + b^2} = \frac{1}{\sqrt{\left(x - \frac{x_c}{1 + a^2}\right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c\right)^2}};$$

in symbolic expression,

$$Y = g + jb = \frac{\left(r - ax - \frac{a}{1 + a^2} x_c\right) + j \left(x - \frac{x_c}{1 + a^2}\right)}{\left(x - \frac{x_c}{1 + a^2}\right)^2 + \left(r - ax - \frac{a}{1 + a^2} x_c\right)^2}.$$

Since the impedance is

$$Z = \left(r - ax - \frac{a}{1 + a^2} x_c\right) - j \left(x - \frac{x_c}{1 + a^2}\right) = r_a - j x_a,$$

we have

$$Y = \frac{1}{Z}; \quad y = \frac{1}{z_a}; \quad g = \frac{r_a}{z_a^2}; \quad b = \frac{x_a}{z_a^2};$$

that is, the same relations as in the complex quantities in alternating-current circuits, except that in the present case all the constants r_a , x_a , z_a , g , z , y , depend upon the decrement a .

Circuits of Zero Impedance.

289. In an oscillating-current circuit of decrement a , of resistance r , inductive reactance x , and capacity reactance x_c , the impedance was represented in symbolic expression by

$$Z = r_a - jx_a = \left(r - ax - \frac{a}{1 + a^2} x_c \right) - j \left(x - \frac{x_c}{1 + a^2} \right),$$

or numerically by

$$z = \sqrt{r_a^2 + x_a^2} = \sqrt{\left(r - ax - \frac{a}{1 + a^2} x_c \right)^2 + \left(x - \frac{x_c}{1 + a^2} \right)^2}.$$

Thus the inductive reactance x , as well as the capacity reactance x_c , do not represent wattless electromotive forces as in an alternating-current circuit, but introduce energy components of negative sign

$$-ax - \frac{a}{1 + a^2} x_c;$$

that means,

“In an oscillating-current circuit, the counter electromotive force of self-induction is not in quadrature behind the current, but lags less than 90° , or a quarter period; and the charging current of a condenser is less than 90° , or a quarter period, ahead of the impressed electromotive force.”

290. In consequence of the existence of negative energy components of reactance in an oscillating-current circuit, a phenomenon can exist which has no analogy in an alternating-current circuit; that is, under certain conditions the total impedance of the oscillating-current circuit can equal zero:

$$Z = 0.$$

In this case we have

$$r - ax - \frac{a}{1 + a^2} x_c = 0; \quad x - \frac{x_c}{1 + a^2} = 0,$$

substituting in this equation

$$x = 2\pi NL; x_c = \frac{1}{2\pi NC};$$

and expanding, we have

$$a = \frac{1}{\sqrt{\frac{4L}{r^2C} - 1}};$$

$$2\pi N = \frac{r}{2L} \sqrt{\frac{4L}{r^2C} - 1} = \frac{r}{2aL}.$$

That is,

“If in an oscillating-current circuit, the decrement

$$a = \frac{1}{\sqrt{\frac{4L}{r^2C} - 1}},$$

and the frequency $N = r/4\pi aL$, the total impedance of the circuit is zero; that is, the oscillating current, when started once, will continue without external energy being impressed upon the circuit.”

291. The physical meaning of this is: “If upon an electric circuit a certain amount of energy is impressed and then the circuit left to itself, the current in the circuit will become oscillating, and the oscillations assume the frequency $N = r/4\pi aL$, and the decrement

$$a = \frac{1}{\sqrt{\frac{4L}{r^2C} - 1}}$$

That is, the oscillating currents are the phenomena by which an electric circuit of disturbed equilibrium returns to equilibrium.

This feature shows the origin of the oscillating currents, and the means to produce such currents by disturbing the equilibrium of the electric circuit; for instance, by the discharge of a condenser, by make and break of the circuit, by sudden electrostatic charge, as lightning, etc. Obviously, the most important oscillating currents are

those flowing in a circuit of zero impedance, representing oscillating discharges of the circuit. Lightning strokes usually belong to this class.

Oscillating Discharges.

292. The condition of an oscillating discharge is $Z = 0$, that is,

$$a = \frac{1}{\sqrt{\frac{4L}{r^2 C} - 1}}, \quad 2\pi N = \frac{r}{2aL} = \frac{r}{2L} \sqrt{\frac{4L}{r^2 C} - 1}.$$

If $r = 0$, that is, in a circuit without resistance, we have $a = 0$, $N = 1/2\pi\sqrt{LC}$; that is, the currents are alternating with no decrement, and the frequency is that of resonance.

If $4L/r^2 C - 1 < 0$, that is, $r > 2\sqrt{L/C}$, a and N become imaginary; that is, the discharge ceases to be oscillatory. An electrical discharge assumes an oscillating nature only, if $r < 2\sqrt{L/C}$. In the case $r = 2\sqrt{L/C}$ we have $a = \infty$, $N = 0$; that is, the current dies out without oscillation.

From the foregoing we have seen that oscillating discharges, — as for instance the phenomena taking place if a condenser charged to a given potential is discharged through a given circuit, or if lightning strikes the line circuit, — is defined by the equation: $Z = 0$ dec a .

Since

$$I = (i_1 + j i_2) \text{ dec } a, \quad E_r = I r \text{ dec } a,$$

$$E_x = -x I (a + j) \text{ dec } a, \quad E_{xc} = \frac{x_c}{1 + a^2} I (-a + j) \text{ dec } a,$$

we have

$$r - ax - \frac{a}{1 + a^2} x_c = 0,$$

$$-x + \frac{x_c}{1 + a^2} = 0;$$

hence, by substitution,

$$E_{xc} = x I (-a + j) \text{ dec } a.$$

The two constants, i_1 and i_2 , of the discharge, are determined by the initial conditions, that is, the electromotive force and the current at the time $t = 0$.

293. Let a condenser of capacity C be discharged through a circuit of resistance r and inductance L . Let e = electromotive force at the condenser in the moment of closing the circuit, that is, at the time $t = 0$ or $\phi = 0$. At this moment the current is zero; that is,

$$I = j i_2, \quad i_1 = 0.$$

Since $E_{xc} = x I(-a + j) \operatorname{dec} a = e$ at $\phi = 0$,

$$\text{we have } x i_2 \sqrt{1 + a^2} = e \text{ or } i_2 = \frac{e}{x \sqrt{1 + a^2}}.$$

Substituting this, we have,

$$I = j \frac{e}{x \sqrt{1 + a^2}} \operatorname{dec} a, \quad E_r = j e \frac{r}{x \sqrt{1 + a^2}} \operatorname{dec} a,$$

$$E_x = \frac{e}{\sqrt{1 + a^2}} (1 - j a) \operatorname{dec} a, \quad E_{xc} = - \frac{e}{\sqrt{1 + a^2}} (1 + j a) \operatorname{dec} a,$$

the equations of the oscillating discharge of a condenser of initial voltage e .

Since $x = 2 \pi N L$,

$$a = \frac{1}{\sqrt{\frac{4L}{r^2 C} - 1}}$$

$$2 \pi N = \frac{r}{2 a L},$$

we have

$$x = \frac{r}{2 a} = \frac{r}{2} \sqrt{\frac{4L}{r^2 C} - 1};$$

hence, by substitution,

$$I = j e \sqrt{\frac{C}{L}} \operatorname{dec} a, \quad E_r = j e r \sqrt{\frac{C}{L}} \operatorname{dec} a,$$

$$E_x = \frac{e r}{2} \sqrt{\frac{C}{L}} \left(\sqrt{\frac{4L}{r^2 C} - 1} - j \right) \operatorname{dec} a,$$

$$E_k = -\frac{er}{2} \sqrt{\frac{C}{L}} \left(\sqrt{\frac{4L}{r^2 C} - 1} + j \right) \text{dec } a,$$

$$a = \frac{1}{\sqrt{\frac{4L}{r^2 C} - 1}}, \quad N = \frac{r \sqrt{\frac{4L}{r^2 C} - 1}}{4\pi L}$$

the final equations of the oscillating discharge, in symbolic expression.

Oscillating Current Transformer.

294. As an instance of the application of the symbolic method of analyzing the phenomena caused by oscillating currents, the transformation of such currents may be investigated. If an oscillating current is produced in a circuit including the primary of a transformer, oscillating currents will also flow in the secondary of this transformer. In a transformer let the ratio of secondary to primary turns be p . Let the secondary be closed by a circuit of total resistance, $r_1 = r_1' + r_1''$, where $r_1' =$ external, $r_1'' =$ internal, resistance. The total inductance $L_1 = L_1' + L_1''$, where $L_1' =$ external, $L_1'' =$ internal, inductance; total capacity, C_1 . Then the total admittance of the secondary circuit is

$$Y_1 = (g_1 + j b_1) \text{dec } a = \frac{1}{\left(r_1 - a x_1 - \frac{a}{1 + a^2} x_{e1} \right) - j \left(x_1 - \frac{x_c}{1 + a^2} \right)},$$

where $x_1 = 2\pi N L_1 =$ inductive reactance; $x_{e1} = 1/2\pi N C =$ capacity reactance. Let $r_0 =$ effective hysteric resistance, $L_0 =$ inductance; hence, $x_0 = 2\pi N L_0 =$ reactance; hence,

$$Y_0 = g_0 + j b_0 = \frac{1}{(r_0 - a x_0) - j x_0} = \text{admittance}$$

of the primary exciting circuit of the transformer; that is, the admittance of the primary circuit at open secondary circuit.

As discussed elsewhere, a transformer can be considered as consisting of the secondary circuit supplied by the impressed electromotive force over leads, whose impedance is

equal to the sum of primary and secondary transformer impedance, and which are shunted by the exciting circuit, outside of the secondary, but inside of the primary impedance.

Let r = resistance ; L = inductance ; C = capacity ; hence,

$$x = 2 \pi N L = \text{inductive reactance,}$$

$x_c = 1 / 2 \pi N C$ = capacity reactance of the total primary circuit, including the primary coil of the transformer. If $E'_1 = E_1 \text{ dec } \alpha$ denotes the electromotive force induced in the secondary of the transformer by the mutual magnetic flux ; that is, by the oscillating magnetism interlinked with the primary and secondary coil, we have $I_1 = E_1 Y_1 \text{ dec } \alpha$ = secondary current.

Hence, $I'_1 = p I_1 \text{ dec } \alpha = p E' Y_1 \text{ dec } \alpha$ = primary load current, or component of primary current corresponding to secondary current. Also, $I_0 = \frac{1}{p} E'_1 Y_0 \text{ dec } \alpha$ = primary exciting current ; hence, the total primary current is

$$I = I'_1 + I_0 = \frac{E'_1}{p} \{ Y_0 + p^2 Y_1 \} \text{ dec } \alpha.$$

$E' = \frac{E'_1}{p} \text{ dec } \alpha$ = induced primary electromotive force.

Hence the total primary electromotive force is

$$E = (E' + IZ) \text{ dec } \alpha = \frac{E'_1}{p} \{ 1 + Z Y_0 + p^2 Z Y_1 \} \text{ dec } \alpha.$$

In an oscillating discharge the total primary electromotive force $E = 0$; that is,

$$1 + Z Y_0 + p^2 Z Y_1 = 0 ;$$

or, the substitution

$$1 + \frac{\left(r - a x - \frac{a}{1 + a^2} x_c \right) - j \left(x - \frac{x_c}{1 + a^2} \right)}{(r_0 - a x_0) - j x_0} + p^2 \frac{\left(r - a x - \frac{a}{1 + a^2} x_c \right) - j \left(x - \frac{x_c}{1 + a^2} \right)}{\left(r_1 - a x_1 - \frac{a}{1 + a^2} x_{c1} \right) - j \left(x_1 - \frac{x_{c1}}{1 + a^2} \right)} = 0.$$

Substituting in this equation, $x = 2\pi NC$, $x_c = 1/2\pi NC$, etc., we get a complex imaginary equation with the two constants a and N . Separating this equation in the real and the imaginary parts, we derive two equations, from which the two constants a and N of the discharge are calculated.

295. If the exciting current of the transformer is negligible, — that is, if $Y_0 = 0$, the equation becomes essentially simplified, —

$$1 + p^2 \frac{\left(r - ax - \frac{a}{1+a^2} x_c \right) - j \left(x - \frac{x_c}{1+a^2} \right)}{\left(r_1 - ax_1 - \frac{a}{1+a^2} x_{c1} \right) - j \left(x_1 - \frac{x_{c1}}{1+a^2} \right)} = 0;$$

that is,

$$\begin{aligned} \left(r_1 - ax_1 - \frac{a}{1+a^2} x_{c1} \right) + p^2 \left(r - ax - \frac{a}{1+a^2} x_c \right) &= 0; \\ \left(x_1 - \frac{x_{c1}}{1+a^2} \right) + p^2 \left(x - \frac{x_c}{1+a^2} \right) &= 0; \end{aligned}$$

or, combined, —

$$\begin{aligned} (r_1 - 2ax_1) + p^2(r - 2ax) &= 0, \\ r_1 + p^2r &= 2a(x_1 + p^2x), \\ x_{c1} + p^2x_c &= (1+a^2)(x_1 + p^2x). \end{aligned}$$

Substituting for x_1 , x , x_{c1} , x_c , we have

$$\begin{aligned} a &= \frac{1}{\sqrt{\frac{4(L_1 + p^2L)}{(r_1 + p^2r)^2(C_1 + p^2C)} - 1}}, \\ 2\pi N &= \frac{r_1 + p^2r}{2a(L_1 + p^2L)} \\ &= \frac{r_1 + p^2r}{2(L_1 + p^2L)} \sqrt{\frac{4(L_1 + p^2L)}{(r_1 + p^2r)^2(C_1 + p^2C)} - 1}. \\ E &= \frac{E_1'}{p} \{1 + p^2ZY_1\} \operatorname{dec} a, \\ I &= pE_1' Y_1 \operatorname{dec} a, \\ I_1 &= E_1' Y_1 \operatorname{dec} a, \end{aligned}$$

the equations of the oscillating-current transformer, with E_1' as parameter.

INDEX.

	PAGE		PAGE
Advance Angle , of eddy currents . . .	130	Capacity load, effect on alternator	
hysteretic, of ironclad circuit . . .	123	field characteristic	239
Admittance, Chap. VII.	52, 53	of line, approximation	152, 153
absolute, of ironclad circuit . . .	122	Characteristic, field, of alternator . .	240
combination in parallel	57	magnetic, true and apparent . . .	113
combination in series	57	wave-shapes	336
primary, of transformer	178	Charging current of transmission lines,	
Air-gap in magnetic circuit	124	magnitude	151
in magnetic circuit, in its action		Coefficient, of eddy currents	133, 131
on the hysteretic distortion . .	111	of hysteresis	116
Algebra of complex imaginary quantities,		Combination of admittances in parallel	
Appendix I.	401	57
Alternating wave.	11	of conductances	52
Alternators, synchronizing, Chap.		of impedances in series	53
XVII.	248	of resistances	52
Ambiguity of vectors	43	of sine waves, by parallelogram or	
Amplitude or maximum value of wave, .	7	polygon on vectors	21, 22
Analytic method of treating synchronous		of sine waves in symbolic expression	
motor	275	38
Apparent impedance of transformer . .	182	Commutator motors, Chap. XIX.	291
Approximations of line capacity, 152, 153		Commutator, sparking at, in series	
Arc, power factor of	331	and shunt motor	306
pulsating, resistance of	329	Comparison of systems regarding copper	
Armature resistance of induction motor,		efficiency, Chap. XXVIII	380
effect on starting torque	226	Compensation of line drop by shunted	
Asynchronous motor, see induction motor.		susceptance	97
Average value of wave.	11	for lagging currents by shunted	
Balanced polyphase system ,		condensance	72
Chap. XXV.	356, 357, 347	Complete resonance in transmission	
quarter-phase system, equations . .	396	lines	340
three-phase system, equations . . .	393	Complex harmonic wave	9
Balance factor of polyphase system . .	357	Complex imaginary quantities, Appendix	
unchanged by transformation of		I.	401
polyphase system	376	Condensance or capacity reactance . .	5
Balance of polyphase system, in topographic		reactance for constant potential,	
representation	46	constant current transformation . .	76
Capacity	5	shunted, compensation for lagging	
effect on higher harmonics	337	current	72
		shunted, control of receiver voltage	
		in transmission lines	96

	PAGE		PAGE
Condensance, symbolic or complex imaginary representation	40	Disruptive phenomena	147
Condenser current of transmission lines, magnitude	151	Distortion of wave-shape and eddy currents, Chap. XXI.	320
Conductance, Chap. VII.	52, 53	Distortion of wave-shape by arc	329
combination of	52	causing decrease of hysteresis	343
effective	104	causing increase of hysteresis	343
of magnetic hysteresis	119	in reaction machines	312
of mutual inductance	142	of current wave by hysteresis	107
equivalent, of eddy currents	130	by quintuple harmonic	335
of receiver circuit supplied over in- ductive line	89	by triple harmonic	335
Conductor, eddy currents in	138	Distributed capacity, approximation, 152, 153	
Constant current alternator	246	complete investigation	155
Constant current, constant potential transformation	76	instance and particular cases	162
Constant potential regulation, of al- ternator	245	Divided circuit, equivalent to alternat- ing-current transformer	183
Constants, electric, of magnetic circuit containing iron	125	Double transformation	186
of alternating-current transformer, 190		Eddy currents , Chap. XI.	129, 106
Control of receiver potential in trans- mission lines by shunted sus- ceptance	97	not affected by wave-shape	344
Converter, see transformer.		Effect, see power, and output.	
Converter motor, see induction motor.		Effective resistance and reactance, Chap. X.	104
Coördinates, rectangular and polar	19	resistance, reactance, conductance, susceptance	104
Copper efficiency of polyphase sys- tems, Chap. XXVIII.	380	resistance	2, 6
Counter E.M.F. and component of impressed E.M.F.	24	value of wave	11, 14
Creeping, magnetic	114	Efficiency of constant potential, con- stant current transformation by resistance reactance	81
Cross currents, between synchronizing alternators	249	Electro-magnetic induction, law of, Chap. III.	16
Cross flux, magnetic, of transformer, 167, 194		Electro-magnetism, as source of re- actance	
Current, minimum, at given power, in synchronous motor	282	Electrostatic hysteresis, see dielectric hysteresis.	
Cycles, magnetic, of hysteresis	107	induction, or influence.	147
Delta connection of three-phase sys- tem	369	Energy components of current and of E.M.F.	148
current of three-phase system	371	component of reactance	309
potential of three-phase system	371	equation of alternating currents	23
Demagnetizing effect of eddy currents, 136		Equations, of alternator	238
Dielectric hysteresis	144, 105	of general alternating-current trans- former	195
Dielectric hysteretic admittance, im- pedance, etc.	145	Equivalent sine wave	320, 111, 115
Dielectric hysteretic lag angle	145	Exciting current of transformer	169
Displacement of phase, maximum, in synchronous motor	284	Field characteristic of alternator	240
		Flow of power in single-phase system, 356 in polyphase system	357, 360
		Flux of alternating-current generator, 234	

	PAGE
Flux, pulsation of, in alternating-current generator	234
Foucault currents, Chap. xi	129, 106
Fourier series, univalent function of time	7
Four-phase, see quarter-phase.	
Four-wire quarter-phase system, see independent quarter-phase system.	
Frequency of wave	7
Frequency setter, with induction generator	230
Friction, molecular	105
Fundamental wave, or first harmonic,	8
General alternating-current transformer. Chap. xiv.	193, 195
Generator action of general alternating-current transformer	203
Generator, alternating-current, Chap. xvi.	234
induction	229
on unbalanced load, in topographic representation	48
polar diagram on non-inductive, inductive, and capacity circuit,	28
quarter-phase, in topographic representation	49
three-phase, on balanced load, in topographic representation	46
Graphic method, disadvantage for numerical calculation	33
of induction motor	213
of synchronous motor	258
Graphic representation, Chap. iv.	19
Harmonics, even	8
first	8
higher, effect of, Chap. xxii.	334
causing resonance in transmission lines	338
effect of self-induction and capacity	338
of distorted wave	111
or overtones	8
Hedgehog transformer	169
Hunting of parallel running alternators	249
Hysteresis, coefficient of	116
decrease due to distorted wave	343
dielectric	105, 144

	PAGE
Hysteresis, effect of, on electric circuit, conclusions	127
increase due to distorted wave	343
magnetic	105, 106
motor	312
Hysteretic advance of phase	115
energy current	115
energy current of transformer	170
loss, curve of	114
Imaginary quantities, complex, Appendix I.	401
Impedance	2, 5
apparent, of transformer	182
combination in parallel	57
combination in series	53
in series to circuit	68
in symbolic or complex imaginary representation	39
internal, of transformer	178
Increase of output in transmission lines, by shunted susceptance	100
Independent polyphase system	347
quarter-phase system	398
Induced E.M.F., derivation of formula,	16
Inductance, introduction and derivation of formula	18
mutual and self	142
Induction, electrostatic, or influence	146
generator	229
motor as special case of general alternating-current transformer,	200, 207
motor, Chap. xv.	207
motor, graphic method	213
motor, numerical instance	230
motor, symbolic method	208
Inductive line, maximum power supplied over	87
feeding non-inductive, inductive and capacity circuit, graphic,	23, 26, 27
maximum efficiency of transmitted power	93
supplying non-inductive receiver circuit	84
symbolic method	40
Inductive load, effect on alternator field characteristic	239
Influence or electrostatic induction	146
Instantaneous values of wave, Chap. ii.	11

	PAGE		PAGE
Insulation strain in high potential line, due to distorted wave-shape	344	Maximum output, or power, of alter- nator	247
Integral values of wave, Chap. II.	11	of induction motor	222
Internal impedance of transformer	178	of synchronous motor	279
Intensity of wave	20	supplied over inductive line	87
Interlinked polyphase systems, Chap. xxvi.	368, 347	Maximum rise of potential in receiver circuit fed by inductive line	101
quarter-phase system	395	torque of induction motor	219
Inverted three-phase system, as unbal- anced system	359	value of wave	11
flow of power	363	Mean value of wave	12
Ironclad inductance	124	Mechanical power of induction motor, 216, 218	
magnetic circuit	106	of general alternating-current trans- former	201, 202
Iron wire	133, 135	Minimum current at given power in synchronous motor	282
J , introduction as a symbol	36	Molecular friction	105
definition as $\sqrt{-1}$	37	Monocyclic systems	363
Joule's Law of alternating circuits	6	power characteristic	363
of continuous currents	1	Monophase, see single-phase.	
Kirchhoff's Laws of alternating cir- cuits	6, 22	Motor action of general alternating- current transformer	203
in symbolic or complex imaginary representation	40	commutator, Chap. XIX.	291
of continuous current circuits	1	repulsion	291
Lag angle of dielectric hysteresis	145	series	300
demagnetizing alternator and mag- netizing synchronous motor	235	shunt	305
Laminated iron	131, 135	synchronous, Chap. XVIII.	258
Lead, magnetizing alternator and de- magnetizing synchronous motor	235	Mutual flux of transformer	195
Leakage	106	inductance	142
current of transformer	169	induction of transformers	167
Light running of synchronous motor, 280		Non-inductive load , effect on alterna- tor field characteristic	239
Line capacity, approximation	152, 153	receiver circuit supplied over in- ductive line	84
complete investigation	155	Non-synchronous Motor, see induc- tion motor.	
Line, inductive, feeding non-inductive, inductive and capacity circuit, graphic	23, 26, 27	Ohm's Law of alternating-current circuit	2, 5
load characteristic of	95	of continuous currents	1
symbolic method	41	Oscillating currents and E.M.Fs., Appendix II.	409
Load characteristic of transmission line	95	Output of general alternating-current transformer	201, 202
Loop, hysteretic	107	increase of, in transmission lines by shunted susceptance	100
Magnetic hysteresis	105, 106	maximum of alternator	247
Magnetizing current	115	maximum of non-inductive receiver circuit supplied over inductive line	85
of transformer	170	maximum of synchronous motor	279
Magneto-motive force of alternating- current generator	234		
resultant of symmetrical polyphase system	352		

	PAGE		PAGE
Output of receiver circuit supplied		Pulsation of flux of alternate-current	
over inductive line	87	generator	234
Overtones or higher harmonics	8	Pulsation of magnetic flux distorting	
see power		the wave-shape	324
Parallelogram of vectors or sine		of reactance distorting the wave-	
waves	21	shape	328
Parallel operation of alternators,		of reluctance distorting the wave-	
Chap. xvii.	248	shape	327
Period of a wave	7	of resistance distorting the wave-	
Phase of a wave	7, 20	shape	329
Phase displacement, maximum, in		Quarter-phase system, Chap. xxx.	
synchronous motor	284	395, 348, 352	
Phase relation of current in alternator,		as balanced system	358
reacting on field	235	copper efficiency	380
Polar coördinates	19	equations	395
Polar diagram of transformer	170	flow of power	361
Polarization, equivalent to capacity, 5, 147		resultant M.M.F. of	355
Polycyclic systems	363	transformation to three-phase	378
power characteristic	363	with common return, unbalancing, 50	
Polygon of sine waves	22	Quintuple harmonic, distortion of	
Polyphase systems, general,		wave-shape by	335
Chap. xxiii.	346	Reactance, capacity, or condensance, 5	
interlinked, Chap. xxvi.	368	and resistance of transmission lines,	
power characteristic	363	Chap. ix.	83
symmetrical, Chap. xxiv.	350	as component of impedance	2
balance factor of	357	capacity in symbolic representation 40	
transformation of, Chap. xxvii.	376	condensance for constant potential,	
Power axes of alternating-current sys-		constant current transformation, 76	
tem	366	effective, Chap. x.	104
characteristics of alternating-cur-		in series to circuit	61
rent systems	363, 364	in symbolic representation	38
characteristics of synchronous mo-		introduction and derivation of for-	
tor	278	mula	17
equation of alternating circuits	6	magnetic	4
equation of continuous currents	1	synchronous, of alternator	238
factor of arc	331	synchronous, of synchronous mo-	
factor of series motor	307	tor	290
flow of, in single-phase system	356	variable in reaction machines, 309, 310	
in polyphase system	357, 360	Reaction of lead or lag in alternator	
of complex harmonic wave	341	and synchronous motor	236
of general alternating-current trans-		machines, Chap. xx.	308
former	201, 202	machines, distortion of wave-shape, 312	
of induction motor	217, 219	machines, equations	315
maximum, of alternator	247	Reactive component of pulsating re-	
maximum, of induction motor	222	sistance	329
of repulsion motor	298	Rectangular coördinates	19
of synchronous motor	303	of vectors in graphic representation	
see output.		by polar diagram	35
Primary admittance of transformer	178	Reduction of transformer to divided	
Pulsating wave	11	circuit	182

	PAGE		PAGE
Regulation of alternator for constant potential	245	Self-induction, E.M.F. of	3
Reluctance of magnetic circuit of alternator	234	of transformer	167, 194
variable in reaction machines, 309, 310		Series motor	300
Repulsion motor	291	equations of	301
equations	296	phase displacement	303
power of	298	power	303
Resistance, combination of	52	Series operation of alternators	250
and reactance of transmission lines, Chap. IX.	83	Sheet iron	131, 135
as component of impedance	2	Shunted condensation, compensation for lagging current	72
effective, Chap. X.	104, 2, 6	Shunt motor	300, 305
in series to circuit	58	Sine wave, equivalent	111, 115
in symbolic representation	38	as simplest wave	6
of induction motor armature, affecting starting torque	226	in polar coordinates	20
Resolving sine waves in symbolic expression	38	Single-phase system	351
Resonance	65	copper efficiency	380
by higher harmonics	115	flow of power	356, 360
by higher harmonics in transmission lines	338	power characteristic	363
complete, in transmission lines	340	Slip of general alternating-current transformer	195
in transmission lines	101	in induction motor	207
Resultant magnetic flux of alternator, 234		Sparking in series and shunt motors	306
Ring connection of interlinked polyphase system	368	Star connection of interlinked polyphase system	368
of polyphase system	347	of polyphase system	347
Ring current of interlinked polyphase system	371	Star current of interlinked polyphase system	371
Ring potential of interlinked polyphase system	371	Star potential of interlinked polyphase system	371
Rise of potential, maximum, in receiver circuit fed by inductive line	101	Starting resistance of induction motor, torque of induction motor	227 224
Rotation of vectors	36	Susceptance, Chap. VII.	52, 53
Ruhmkorff coil, wave-shape	9	effective	104
Screening effect of eddy currents in iron	129	effective of mutual inductance	143
of eddy current	136	of receiver circuit supplied over inductive line, as varying output	88
of electric conductor	138	shunted, controlling receiver voltage in transmission line	96
Secondary load on its action on hysteretic distortion	111	Symbolic method, Chap. V.	33
Self-inductance	3	applied to transformer	178
and mutual inductance	142	representation	208
of alternator	237	Symmetrical polyphase system, Chap. XXIV.	350, 346
Self-induction, coefficient of, or self-inductance	3	Synchronizing alternators, Chap. XVII.	248
effect of higher harmonics	337	as condensation or inductance	147
		Synchronizing power of alternators, 250, 254, 256	
		Synchronism of induction motor	228
		running near, of induction motor, 228	

	PAGE		PAGE
Synchronous motor, Chap. XVIII.	258	Transformer, symbolic method	178
analytic method	275	Transmission line, load characteristic,	95
discussion of results	288	resistance and reactance, Chap. IX.,	83
fundamental equations	276	resonance by higher harmonics	338
graphic method	258	Trigonometric calculation and graphic	
maximum output	279	representation	34
power characteristic	278	Triple harmonic, distortion of wave-	
Synchronous reactance of alternator	238	shape	334
of synchronous motor	290	Two-phase, see quarter-phase.	
Three-phase generator on balanced		Unbalanced polyphase system,	
load	46	Chap. xxv.	356, 347
on unbalanced load	48	quarter-phase system, equations	396
Three-phase system, Chap. XXIX.,	300, 348, 351	three-phase system, equations, 390, 393	
as balanced system	358	Unbalancing of quarter-phase system	
copper efficiency	380	with common return	50
flow of power	362	of three-phase generator or system	
inverted, as unbalanced system	359	on unequal load	48
flow of power	352	Unequal current distribution in con-	
resultant M.M.F.	355	ductor	139
topographic representation	44	Uniformity of speed as condition of	
transformation to quarter-phase	378	parallel operation of alternators, 248	
Three-phase system, unbalanced,	390	Univalent function of time and Fou-	
equations	390	rier series	7
Three-wire system, copper efficiency	381	Unsymmetrical polyphase system	346
Time-constant	3	Variable reactance and reluctance in	
Torque of induction motor	216	alternators	309, 310
maximum, of induction motor	219	Variation of receiver potential in	
starting, of induction motor	224	transmission lines by shunted	
Transformation, constant potential,		susceptance	96
constant current	76	Vectors	19
double	186	ambiguity of	43
from three-phase to quarter-phase		Wattless component of current and	
and inversely	378	of E.M.F.	148
of polyphase systems, Chap. XXVII., 376		Wave-shape, characteristic	336
Transformer, Chap. XIII.	167	distortion and its causes,	
constants on non-inductive load	190	Chap. XXI.	320
equations	195	distortion by arc	329
equivalent to divided circuit, 183, 184		distortion by quintuple harmonics, 335	
general alternating-current,		distortion by triple harmonics	335
Chap. XIV.	193	distortion causing decrease of hys-	
magnetic cross-flux	194	teresis	343
motor, see induction motor.		distortion causing increase of hys-	
numerical instance	191	teresis	343
phase difference in secondary and		distortion in reaction machines	312
in primary	31	Wire, iron	133, 135
polar diagram	170, 28, 31	Y connection of three-phase system	369
stationary, as special case of gen-		Y current of three-phase system	371
eral alternating-current trans-		Y potential of three-phase system	371
former	199		

THIRD EDITION, GREATLY ENLARGED.

A DICTIONARY OF Electrical Words, Terms, and Phrases.

By EDWIN J. HOUSTON, PH.D. (Princeton),

AUTHOR OF

*Advanced Primers of Electricity ; Electricity One Hundred
Years Ago and To-day, etc., etc., etc.*

**Cloth. 667 large octavo pages, 582 Illustrations.
Price, \$5.00.**

Some idea of the scope of this important work and of the immense amount of labor involved in it, may be formed when it is stated that it contains definitions of about 6000 distinct words, terms, or phrases. The dictionary is not a mere word-book; the words, terms, and phrases are invariably followed by a short, concise definition, giving the sense in which they are correctly employed, and a general statement of the principles of electrical science on which the definition is founded. Each of the great classes or divisions of electrical investigation or utilization comes under careful and exhaustive treatment; and while close attention is given to the more settled and hackneyed phraseology of the older branches of work, the newer words and the novel departments they belong to are not less thoroughly handled. Every source of information has been referred to, and while libraries have been ransacked, the note-book of the laboratory and the catalogue of the ware-room have not been forgotten or neglected. So far has the work been carried in respect to the policy of inclusion that the book has been brought down to date by means of an appendix, in which are placed the very newest words, as well as many whose rareness of use had consigned them to obscurity and oblivion. As one feature, an elaborate system of cross-references has been adopted, so that it is as easy to find the definitions as the words, and *aliases* are readily detected and traced. The typography is excellent, being large and bold, and so arranged that each word catches the eye at a glance by standing out in sharp relief from the page.

Copies of this or any other electrical book published will be sent by mail, POST-AGE PREPAID, to any address in the world, on receipt of price.

**The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.**

Elementary Electro-Technical Series.

BY

EDWIN J. HOUSTON, PH.D.,

AND

A. E. KENNELLY, Sc.D.

Alternating Electric Currents.	Electric Incandescent Lighting.
Electric Heating.	Electric Motor.
Electromagnetism.	Electric Street Railways.
Electricity in Electro-Therapeutics.	Electric Telephony.
Electric Arc Lighting.	Electric Telegraphy.

Cloth. Price per volume, \$1.00.

The publication of this series of elementary electro-technical treatises on applied electricity has been undertaken to meet a demand which is believed to exist on the part of the public and others for reliable information regarding such matters in electricity as cannot be readily understood by those not specially trained in electro-technics. The general public, students of elementary electricity and the many interested in the subject from a financial or other indirect connection, as well as electricians desiring information in other branches than their own, will find in these works precise and authoritative statements concerning the several branches of applied electrical science of which the separate volumes treat. The reputation of the authors and their recognized abilities as writers, are a sufficient guarantee for the accuracy and reliability of the statements contained. The entire issue, though published in a series of ten volumes, is nevertheless so prepared that each book is complete in itself and can be understood independently of the others. The volumes are profusely illustrated, printed on a superior quality of paper, and handsomely bound in covers of a special design.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world on receipt of price.

The W. J. Johnston Company, Publishers,

253 BROADWAY, NEW YORK.

Electrical Power Transmission.

By LOUIS BELL, PH.D.

Uniform in size with "The Electric Railway in Theory and Practice." Price, \$2.50.

The plan of the work is similar to that of "The Electric Railway in Theory and Practice," the treatment of the subject being non-mathematical and not involving on the part of the reader a knowledge of the purely scientific theories relating to electrical currents. The book is essentially practical in its character, and while primarily an engineering treatise, is also intended for the information of those interested in electrical transmission of power, financially or in a general way. The author has a practical acquaintance with the problems met with in the electrical transmission of energy from his connection with many of the most important installations yet made in America, and in these pages the subject is developed for the first time with respect to its practical aspects as met with in actual work. The first two chapters review the fundamental principles relating to the generation and distribution of electrical energy, and in the three succeeding ones their methods of application with both continuous and alternating currents are described. The sixth chapter gives a general discussion of the methods of transformation, the various considerations applying to converters and rotary transformers being developed and these apparatus described. In the chapter on prime movers various forms of water-wheels, gas and steam engines are discussed with respect to their applicability to the purpose in view, and in the chapter on hydraulic development the limitations that decide the commercial availability of water power for electrical transmission of power are pointed out in detail. The five succeeding chapters deal with practical design and with construction work—the power-house, line, and centres of distribution being taken up in turn. The chapter on the latter subject will be found of particular value, as it treats for the first time in a thorough and practical manner one of the most difficult points in electrical transmission. The chapter on commercial data contains the first information given as to costs, and will, therefore, be much appreciated by engineers and others in deciding as to the commercial practicability of proposed transmission projects. This is the first work covering the entire ground of the electrical transmission of power that has been written by an engineer of wide practical experience in all of the details included in the subject, and thus forms a valuable and much-needed addition to electrical engineering literature.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world, on receipt of price.

The W. J. Johnston Company, Publishers,

253 BROADWAY, NEW YORK.

THIRD EDITION. EXTENSIVELY REVISED AND ENLARGED.

THE ELECTRIC RAILWAY

IN THEORY AND PRACTICE.

BY O. T. CROSBY AND DR. LOUIS BELL.

Large Octavo. Profusely Illustrated. Price, \$2.50.

Few technical books have met with so wide an appreciation as "The Electric Railway," which has had the distinction of being accepted throughout the world as the standard authority on the subject of which it treats. The advances in electric traction made since the second edition of the work have been so notable, that the authors, in undertaking the preparation of a new edition, found it necessary to practically rewrite the book, so that the present edition conforms to the very latest knowledge on the subject, both in the domain of theory and of practice. The original purpose of the book has, however, been strictly adhered to—namely, to place before those interested in electric railways, whether in a technical, financial or general way, the principles upon which electric traction is founded and the standard methods employed in their application. In view of the probable application in the near future of alternating currents to electric traction, the present edition includes their consideration in this relation, thus largely extending the value of the treatise. The recent developments in electric locomotives and high-speed electric traction, and the application of electricity to elevated railways and to passenger traffic on steam roads, are in this work considered for the first time connectedly with reference to their engineering and commercial aspects. In the first section of the book are developed the fundamental principles of electricity upon which the apparatus and methods of operation are based. The following section is devoted to prime movers, steam, hydraulic and gas—the modern gas engine here receiving the full treatment which its growing importance calls for. The remainder of the work is devoted to the engineering, practical and commercial features of electric traction, all of the factors that enter being considered from the standpoint of the best practice, and the more important ones elaborated in detail. The plan of the book, in fact, includes the consideration of everything relating to the electrical and mechanical principles and details which enter into electric railway design, construction and operation, the whole being treated from the engineering and commercial standpoint, and without the use of mathematics or resort to purely scientific theory.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world on receipt of price.

The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.

PRACTICAL CALCULATION
OF
Dynamo=Electric Machines.

A MANUAL FOR ELECTRICAL AND MECHANICAL ENGINEERS, AND A TEXT-BOOK FOR STUDENTS OF ELECTRO-TECHNICS.

BY

ALFRED E. WIENER, E.E., M.E.,

Member of the American Institute of Electrical Engineers.

Cloth, Illustrated. Price, \$2.50.

Based upon the practical data and tests of nearly two hundred of the best modern dynamos, including the machines used at the recent World's Fair and those in the largest and most modern central-stations, a complete and entirely practical method of dynamo-calculations is developed. Differing from the usual text-book methods, in which the application of the various formulas requires more or less experience in dynamo-design, the present treatise gives such practical information in the form of original tables and formulas derived from the result of practical machines of American as well as European make, comprising all the usual types of field-magnets and armatures, and ranging through all commercial sizes. The book contains nearly a hundred of such tables, giving the values of the various constants, etc., which enter into the formulas of dynamo-design, and for all capacities, from one-tenth to 2000 kilowatts, for high and slow speed, for bipolar and multipolar fields, and for smooth and toothed drum and ring armatures. Although intended as a text-book for students and a manual for practical dynamo-designers, any one possessing but a fundamental knowledge of algebra will be able to apply the information contained in the book to the calculation and design of any kind of a continuous-current dynamo.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world on receipt of the price.

The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.

THIRD EDITION.

ALTERNATING CURRENTS.

An Analytical and Graphical Treatment for Students
and Engineers.

By FREDERICK BEDELL, PH.D.,

AND

A. C. CREHORE, PH.D.

Cloth. 325 pages, 112 Illustrations. Price, \$2.50.

The present work is the first book that treats the subject of alternating currents in a connected, logical, and complete manner. The principles are gradually and logically developed from the elementary experiments upon which they are based, and in a manner so clear and simple as to make the book easily read by any one having even a limited knowledge of the mathematics involved. By this method the student becomes familiar with every step of the process of development, and the mysteries usually associated with the theory of alternating currents are found to be rather the result of unsatisfactory treatment than due to any inherent difficulty. The first fourteen chapters contain the analytical development, commencing with circuits containing resistance and self-induction only, resistance and capacity only, and proceeding to more complex circuits containing resistance, self-induction, and capacity, and resistance and distributed capacity. A feature is the numerical calculations given as illustrations. The remaining chapters are devoted to the graphical consideration of the same subjects, enabling a reader with little mathematical knowledge to follow the authors, and with extensions to cases that are better treated by the graphical than by the analytical method.

CONTENTS.

Part I. Analytical Treatment.—Chapter I. Introductory to Circuits Containing Resistance and Self-induction.—Chapter II. On Harmonic Functions.—Chapter III. Circuits Containing Resistance and Self-induction.—Chapter IV. Introductory to Circuits Containing Resistance and Capacity.—Chapter V. Circuits Containing Resistance and Capacity.—Chapters VI, VII, VIII, IX, X, XI. Circuits Containing Resistance, Self-induction, and Capacity.—Chapters XII, XIII. Circuits Containing Distributed Capacity and Self-induction.

Part II. Graphical Treatment.—Chapters XIV, XV, XVI, XVII. Circuits Containing Resistance and Self-induction.—Chapters XVIII, XIX. Circuits Containing Resistance and Capacity.—Chapter XX. Circuits Containing Resistance, Self-induction, and Capacity.

Appendix A. Relation between Practical and C. G. S. Limits.—**Appendix B.** Some Mechanical and Electrical Analogies.—**Appendix C.** System of Notation Adopted.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world, on receipt of price.

The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.

Electrodynamic Machinery.

BY

EDWIN J. HOUSTON, PH.D.,

AND

A. E. KENNELLY, Sc.D.

Cloth. 322 Pages. 232 Illustrations. Price, \$2.50.

The advent of the commercially perfected dynamo has marked such an era in electric progress, that the desire naturally exists on the part of students generally, and of electrical engineers in particular, to grasp thoroughly the principles underlying its constitution and operation. While excellent treatises on dynamo-electric machinery are in existence, yet a want has been experienced of a book which shall approach the subject, not from the mathematical standpoint, but from an engineering standpoint, and especially from such an engineering standpoint as would arise in actual working with the apparatus. A book of this latter type will be found in the present work, which is the outcome of a series of articles on the same subject by these authors appearing in the *Electrical World* during 1894-1895. Electrodynamic Machinery, as it is described in this volume, is limited to the consideration of continuous-current apparatus. The authors have endeavored to explain thoroughly the principles involved by the use of as simple mathematics as the case will permit. In order to fix these principles in the mind of the student, and to test his understanding of the same, they have been accompanied by numerous examples taken from practical work, so that a student who will intelligently follow the treatment found in these pages will obtain a grasp of the subject that it would be very difficult for him to obtain otherwise without personal experience. For this reason it is believed that the book will serve as a text-book on continuous-current dynamo-electric machinery for electric-engineering students of all grades.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world, on receipt of price.

The W. J. Johnston Company, Publishers,

253 BROADWAY, NEW YORK.

ALTERNATING CURRENTS OF ELECTRICITY:

Their Generation, Measurement, Distribution, and Application.

By GIBERT KAPP, M.I.C.E., M.I.E.E.

(Authorized American Edition.)

With an Introduction by William Stanley, Jr.

Cloth. 164 pages, 37 Illustrations, and 2 plates. \$1.00.

The rapid development of alternating currents and the great part they are destined to play in the transmission of power have caused an increased interest in the subject, but unfortunately it has heretofore been presented in such a manner as to be beyond the reach of readers without a mathematical education. In the present work, the principles are developed in a simple manner that can be followed by any reader, and the various applications are sketched in a broad and instructive way that renders their understanding an easy task. The few mathematical formulas in the book are confined to appendices. Several chapters treat of various forms of alternating motors, especial attention being paid to the explanation and discussion of multiphase motors. This difficult subject is treated so lucidly that the reader is enabled to form as clear an idea of these new forms of motors as of the simpler continuous current machines. The treatment throughout is thoroughly practical, and the data and discussion on the design and construction of apparatus are invaluable to the electrician and designer. To the student and the general public this work will be a particular boon, bringing within their grasp a subject of the greatest importance and interest.

CONTENTS.

Introduction by William Stanley, Jr.—Chap. I. Introductory.—Chap. II. Measurement of Pressure, Current, and Power.—Chap. III. Conditions of Maximum Power.—Chap. IV. Alternating-current Machines.—Chap. V. Mechanical Construction of Alternators.—Chap. VI. Description of Some Alternators.—Chap. VII. Transformers.—Chap. VIII. Central Stations and Distribution of Power.—Chap. IX. Examples of Central Stations.—Chap. X. Parallel Coupling of Alternators.—Chap. XI. Alternating-current Motors.—Chap. XII. Self-starting Motors.—Chap. XIII. Multiphase Currents.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world, on receipt of price.

The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.

EXPERIMENTS WITH
Alternate Currents
Of High Potential and High Frequency.

By NIKOLA TESLA.

Cloth. 156 pages, with Portrait and 35 Illustrations.

Price, \$1.00.

Since the discovery of the telephone few researches in electricity have created as widespread an interest as those of Nikola Tesla into alternate currents of high potential and high frequency. Mr. Tesla was accorded the unusual honor of an invitation to repeat his experiments before distinguished scientific bodies of London and Paris, and the lecture delivered before the Institution of Electrical Engineers, London, is here presented in book-form. The field opened up, to which this book acts as a guide, is one in which the future may develop results of the most remarkable character, and perhaps lead to an entire revision of our present scientific conceptions, with correspondingly broad practical results. The currents of enormously high frequency and voltage generated by Mr. Tesla developed properties previously entirely unsuspected, and which produced phenomena of startling character. No injurious effects were experienced when the human body was subjected to the highest voltages generated. Lamps with only one conductor were rendered incandescent, and others with no connection whatever to the conducting circuit glowed when merely brought into proximity to the same. The book in which Mr. Tesla describes his marvellous experiments is one that every one who takes an interest in electricity or its future should read. The subject is popularly treated, and as the author is the master of a simple and agreeable style the book is fascinating reading. A portrait and biographical sketch of the author is included.

Copies of this or any other electrical book published will be sent by mail, POSTAGE PREPAID, to any address in the world, on receipt of price.

The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.

PUBLICATIONS

OF

THE W. J. JOHNSTON COMPANY.

The Electrical World. An Illustrated Weekly Review of Current Progress in Electricity and its Practical Applications. Annual subscription.....	\$3.00
General Index to The Electrical World, 1883-1896 (<i>In Press</i>).....	8.00
Atkinson, Philip, Ph.D. The Elements of Static Electricity.....	1.50
Bedell, Frederick, Ph.D., and Crehore, Albert C., Ph.D. Alternating Currents.....	2.50
Bell, Dr. Louis. Electrical Transmission of Power.....	2.50
Cox, Frank P., B.S. Continuous-Current Dynamos and Motors.....	2.00
Crosby, O. T., and Bell, Dr. Louis. The Electric Railway in Theory and Practice.....	2.50
Davis, Charles M. Standard Tables for Electric Wiremen.....	1.00
Foster, H. A. Central-Station Bookkeeping.....	2.50
Gerard's Electricity. Translated under the direction of Dr. Louis Duncan. With chapters by Messrs. Duncan, Steinmetz, Kennelly and Hutchinson.....	2.50
Hering, Carl. Universal Wiring Computer.....	1.00
“ “ Recent Progress in Electric Railways.....	1.00
“ “ Electricity at the Paris Exposition of 1889.....	2.00
“ “ Tables of Equivalents of Units of Measurement.....	.50
Hopkinson, John, F.R.S. Original Papers on Dynamo Machinery and Allied Subjects.....	1.00
Houston, Edwin J., Ph.D. Electrical Measurements.....	1.00
“ “ “ Electricity and Magnetism.....	1.00
“ “ “ Electricity 100 Years Ago and To-Day.....	1.00
“ “ “ Electrical Transmission of Intelligence.....	1.00
“ “ “ Dictionary of Electrical Words, Terms and Phrases.....	5.00
Houston, Edwin J., and Kennelly, A. E. The Electric Motor.....	1.00
“ “ “ “ “ Electric Heating.....	1.00
“ “ “ “ “ Magnetism.....	1.00
“ “ “ “ “ The Electric Telephone.....	1.00
“ “ “ “ “ Electric Telegraphy.....	1.00
“ “ “ “ “ Electric Arc Lighting.....	1.00
“ “ “ “ “ Electric Street Railways.....	1.00

Houston, Edwin J., and Kennelly, A. E.	Electrodynamic Machinery.....	\$2.50
“ “ “ “ “	Electric Incandescent Lighting.....	1.00
“ “ “ “ “	Alternating Electrical Currents.....	1.00
“ “ “ “ “	Electricity in Electro-Therapeutics..	1.00
Johnston's Electrical and Street Railway Directory, Published annually....		5.00
Kapp, Gisbert.	Alternating Currents of Electricity.....	1.00
Lightning Flashes and Electric Dashes (Humorous Sketches, Illustrated).....		1.50
Lockwood, T. D.	Practical Information for Telephonists.....	1.00
Martin, T. C., and Wetzler, Joseph.	The Electric Motor and its Applications..	3.00
Player, William, Jr., and Davis, Minor.	The Quadruplex.....	1.50
Merrill, E. A.	Electric Lighting Specifications.....	1.50
“	Reference Book of Tables and Formulæ for Electric Railway Engineers.	1.00
Parham and Shedd.	Shop and Road Testing of Dynamos and Motors. (<i>In Press</i>).	2.00
Parkhurst, Lieut. C. D.	Dynamo and Motor Building for Amateurs.....	1.00
Perry, Nelson W.	Electric Railway Motors.....	1.00
Proceedings of the National Conference of Electricians.....		.75
Reid, James D.	The Telegraph in America.....	7.00
Steinmetz, C. P.	Theory and Calculation of Alternating-Current Phenomena.	2.50
Tesla, Nikola.	Experiments with Alternating Currents of High Potential and High Frequency.....	1.00
Thompson, Prof. Silvanus P.	Lectures on the Electromagnet.....	1.00
Wiener, Alfred E.	Practical Calculation of Dynamo-Electric Machines.....	2.50
Wheeler, Schuyler S.	Chart of Wire Gauges.....	1.00

All the books here mentioned are bound in cloth, and with hardly an exception are handsomely and copiously illustrated.

Copies of these or of any other electrical works published will be mailed to any address in the world, POSTAGE PREPAID, on receipt of price:

The W. J. Johnston Company, Publishers,

253 BROADWAY, NEW YORK.

THE PIONEER ELECTRICAL JOURNAL OF AMERICA.



READ WHEREVER THE ENGLISH LANGUAGE IS SPOKEN.

THE ELECTRICAL WORLD

is the largest, most handsomely illustrated, and most widely circulated electrical journal in the world.

It should be read not only by every ambitious electrician anxious to rise in his profession, but by every intelligent American.

It is noted for its ability, enterprise, independence and honesty. For thoroughness, candor and progressive spirit it stands in the foremost rank of special journalism.

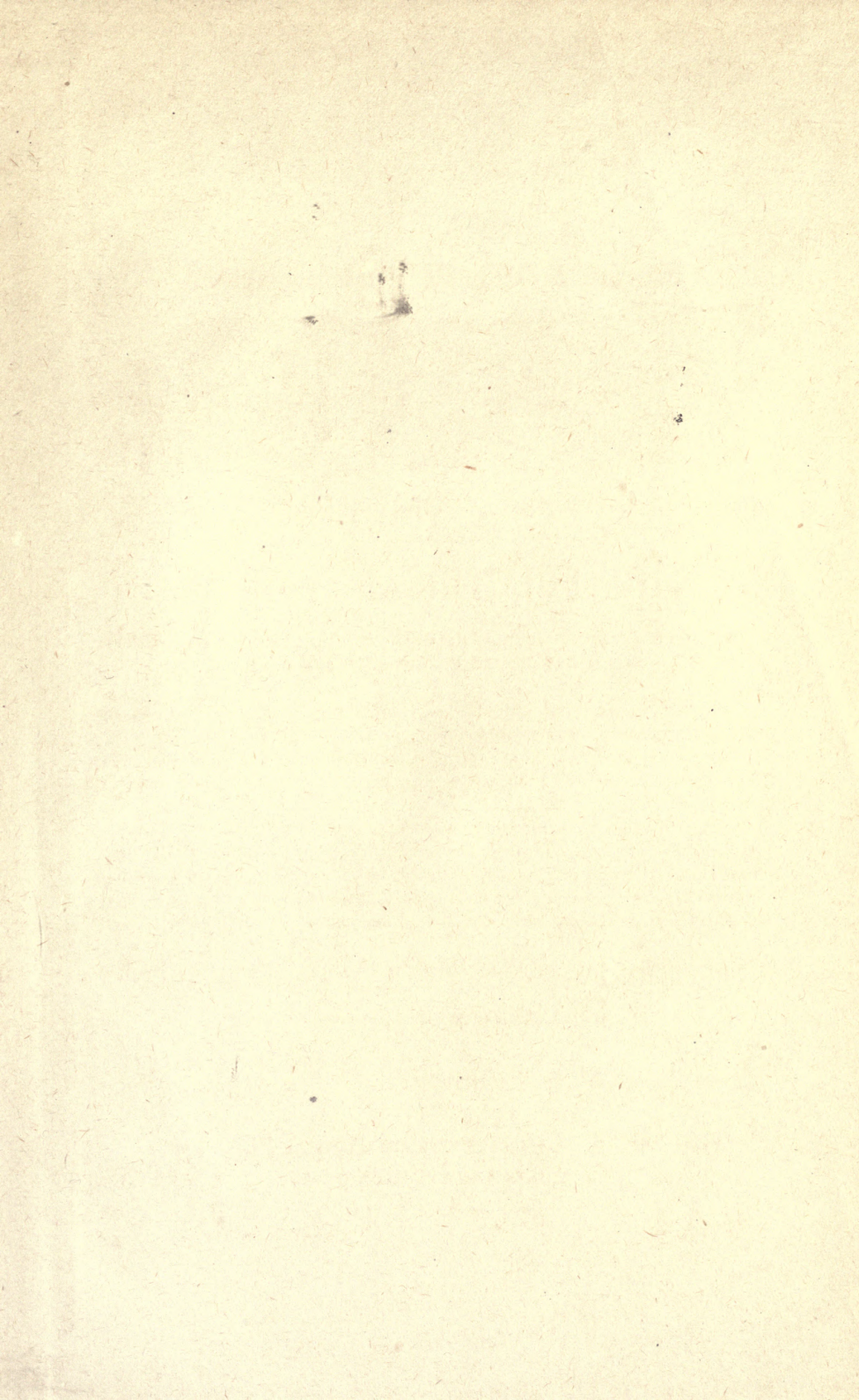
Always abreast of the times, its treatment of everything relating to the practical and scientific development of electrical knowledge is comprehensive and authoritative. Among its many features is a weekly *Digest of Current Technical Electrical Literature*, which gives a complete *résumé* of current original contributions to electrical literature appearing in other journals the world over.

Subscription { including postage in the U. S., } \$3 a Year.
Canada, or Mexico.

May be ordered of any Newsdealer at 10 cents a week.

Cloth Binders for THE ELECTRICAL WORLD postpaid, \$1.00.

The W. J. Johnston Company, Publishers,
253 BROADWAY, NEW YORK.





UNIVERSITY OF CALIFORNIA LIBRARY

This book is DUE on the last date stamped below.

Fine schedule: 25 cents on first day overdue
50 cents on fourth day overdue
One dollar on seventh day overdue.

ENGINEERING LIBRARY

NOV 24 1947

JAN 22 1948
JUL 20 1949

NOV 15 1949

OCT 19 1953

OCT 14 1953

YC 32599

866778

Q C641
S8

Engineering
Library

UNIVERSITY OF CALIFORNIA LIBRARY

